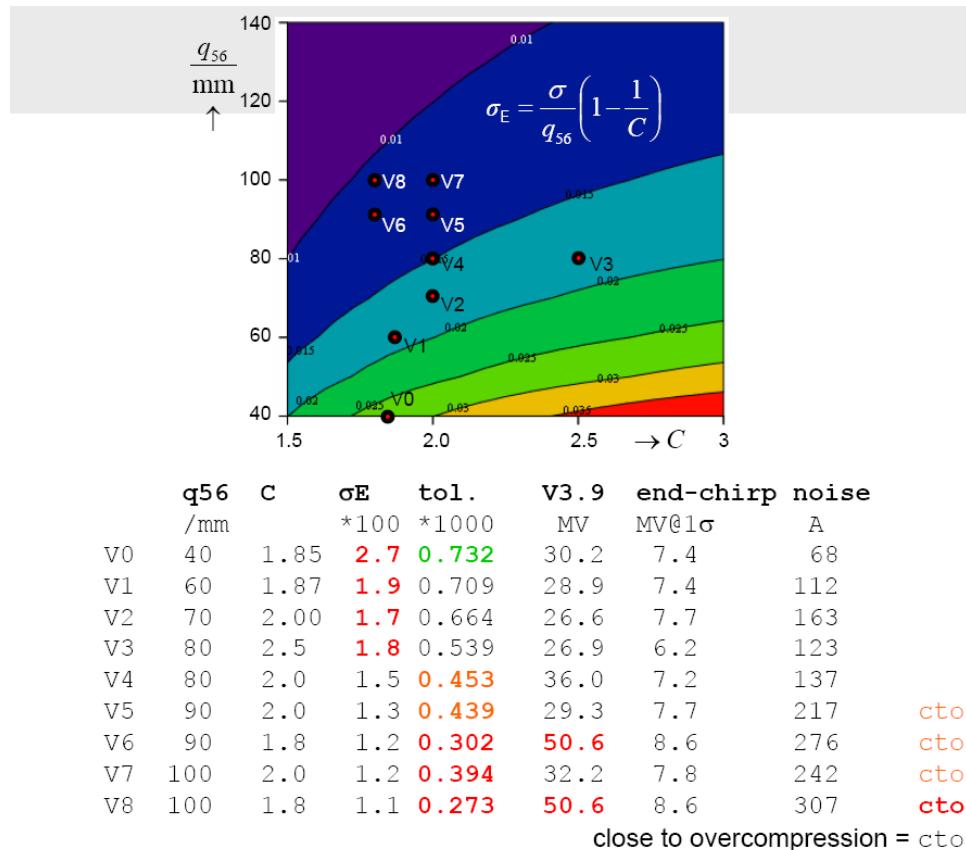


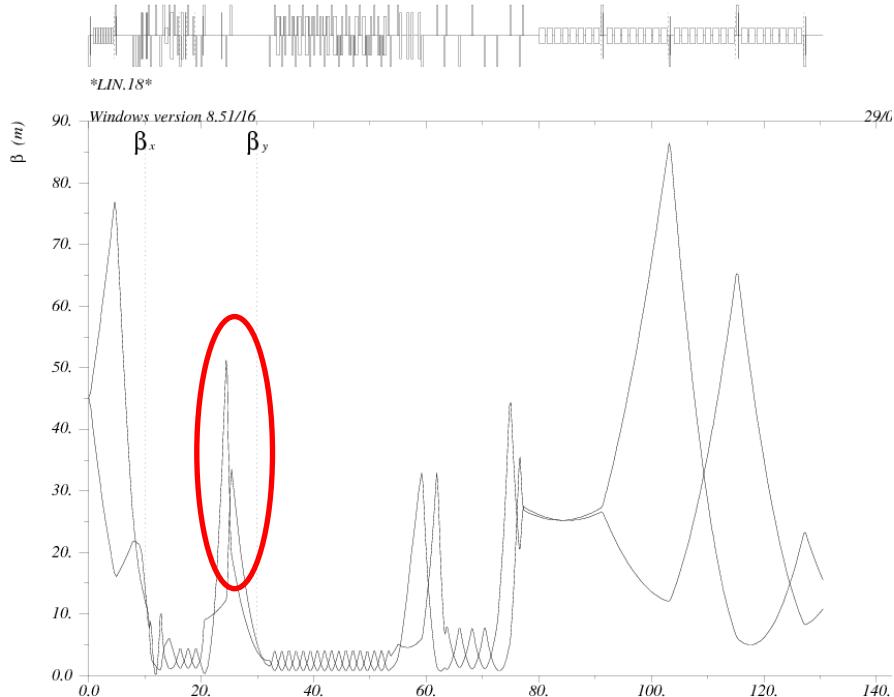
Chromaticity Properties of the Injector Beam Line and Operation at the Laser Heater for Different Working Points of the Three Stage Bunch Compressor System

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08.12.2008

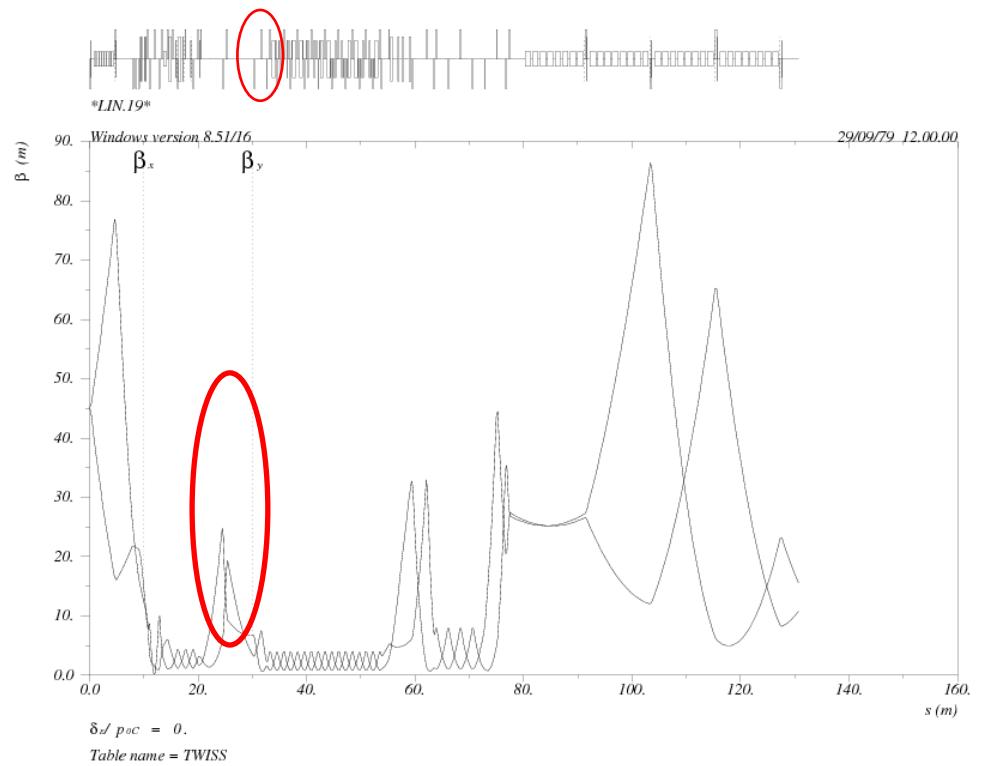
Nine working points have been proposed by M. Dohlus for the operation of the three bunch compressor scheme. Chromaticity properties and operation of the laser heater for these working points will be discussed here



old

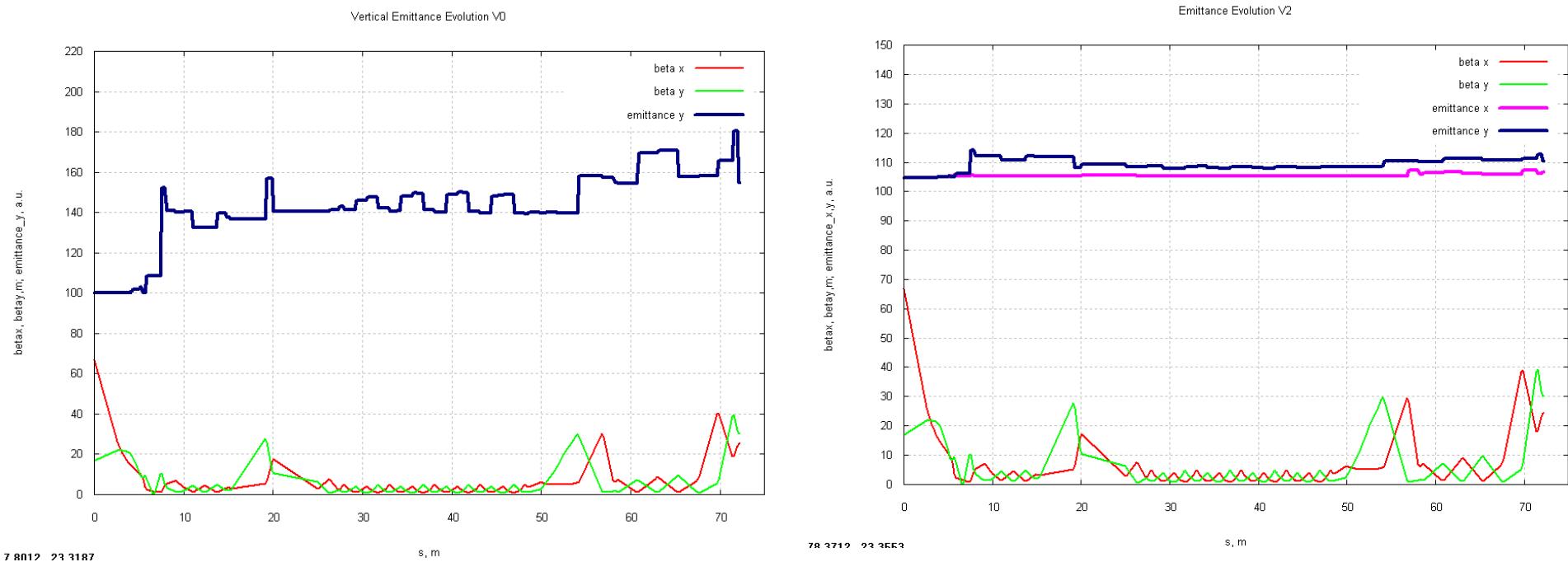


new



- 2 more quadrupoles have been added at the end of shielding
- 1 quadrupole could be spared after the diagnostics
- Whole system requires now 49 instead of 48 quadrupoles
- vertical beta function in the shielding could be reduced by factor of 2 leading to proper chromatics conditions.

Emittance Evolution due to Chromatics



Main sources for emittance blow up:

- Matching to the diagnostics
- Shielding. The Impact of shielding was dominating in the previous optics version
It could be reasonably mitigated by introduction of two quadrupoles at the end of shielding

Chromaticity Properties for Different Working Points

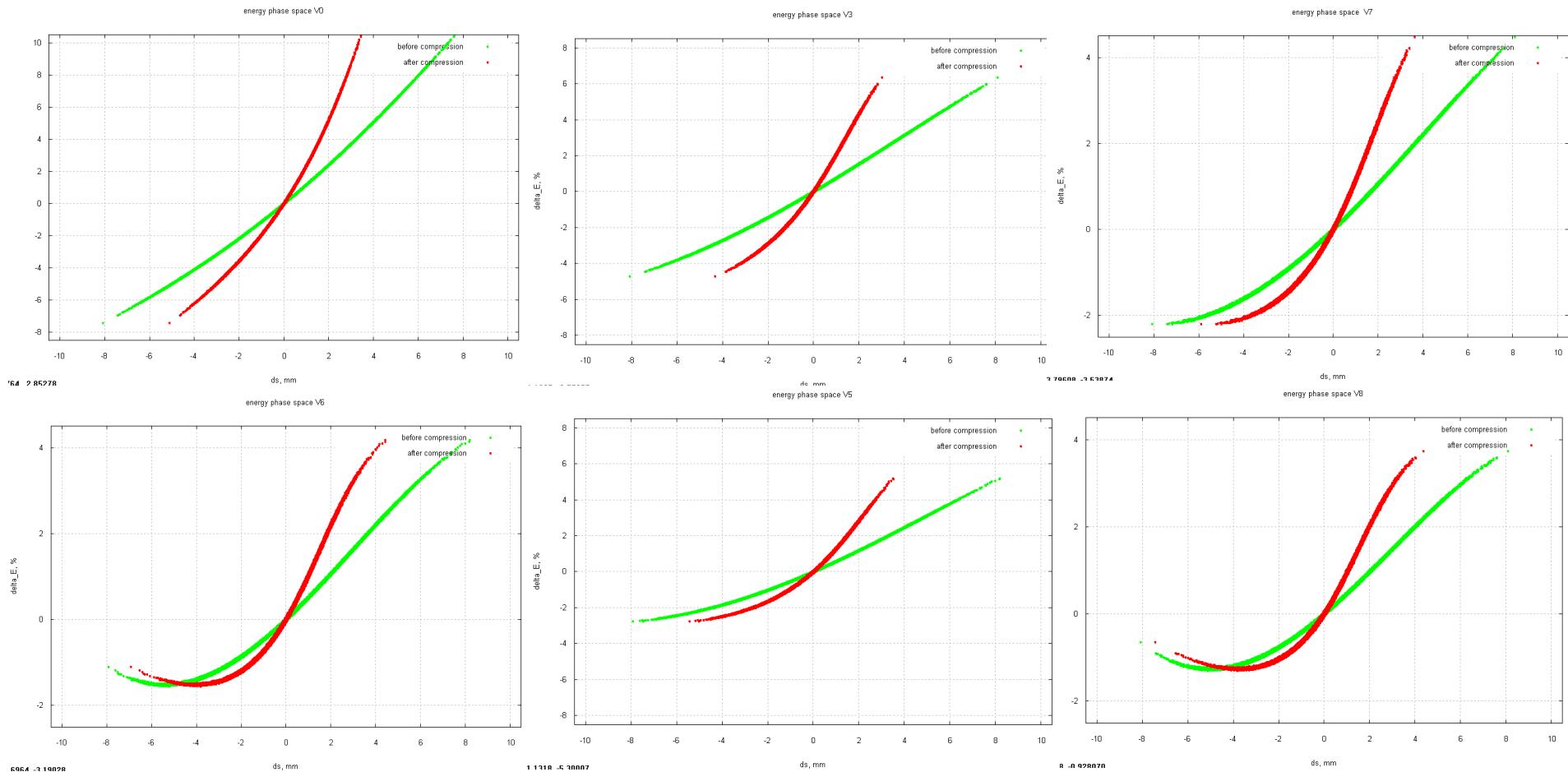
	V0	V1	V2	V3	V4	V5	V6	V7	V8
$\sigma_\delta \%$	2.76 (2.7)	1.84 (1.9)	1.70 (1.7)	1.76 (1.8)	1.44 (1.5)	1.30 (1.3)	1.10 (1.2)	1.16 (1.2)	0.99 (1.1)
C	1.85 (1.85)	1.84 (1.87)	1.97 (2.00)	2.42 (2.5)	1.92 (2.0)	1.93 (2.0)	1.67 (1.8)	1.91 (2.0)	1.67 (1.8)
$\Delta\epsilon_x, \%$	7.84	4.02	3.67	3.72	3.13	2.72	2.27	2.43	2.01
$\Delta\epsilon_y, \%$	54.24	19.5	15.87	17.51	9.80	7.38	4.52	4.97	3.38

Calculated from water bug model for the longitudinal and energy distribution
with $\sigma_s = 2.394\text{mm}$, $\sigma_{\delta(\text{uncorrelated})} = 30\text{keV}$
(...) - „3 BC Working Points“ (M. Dohlus)

Longitudinal Space Phase for some Working Points

The distributions are not always completely linear → discrepancies to

$$\sigma_E = \frac{\sigma}{q_{56}} \left(1 - \frac{1}{C}\right)$$



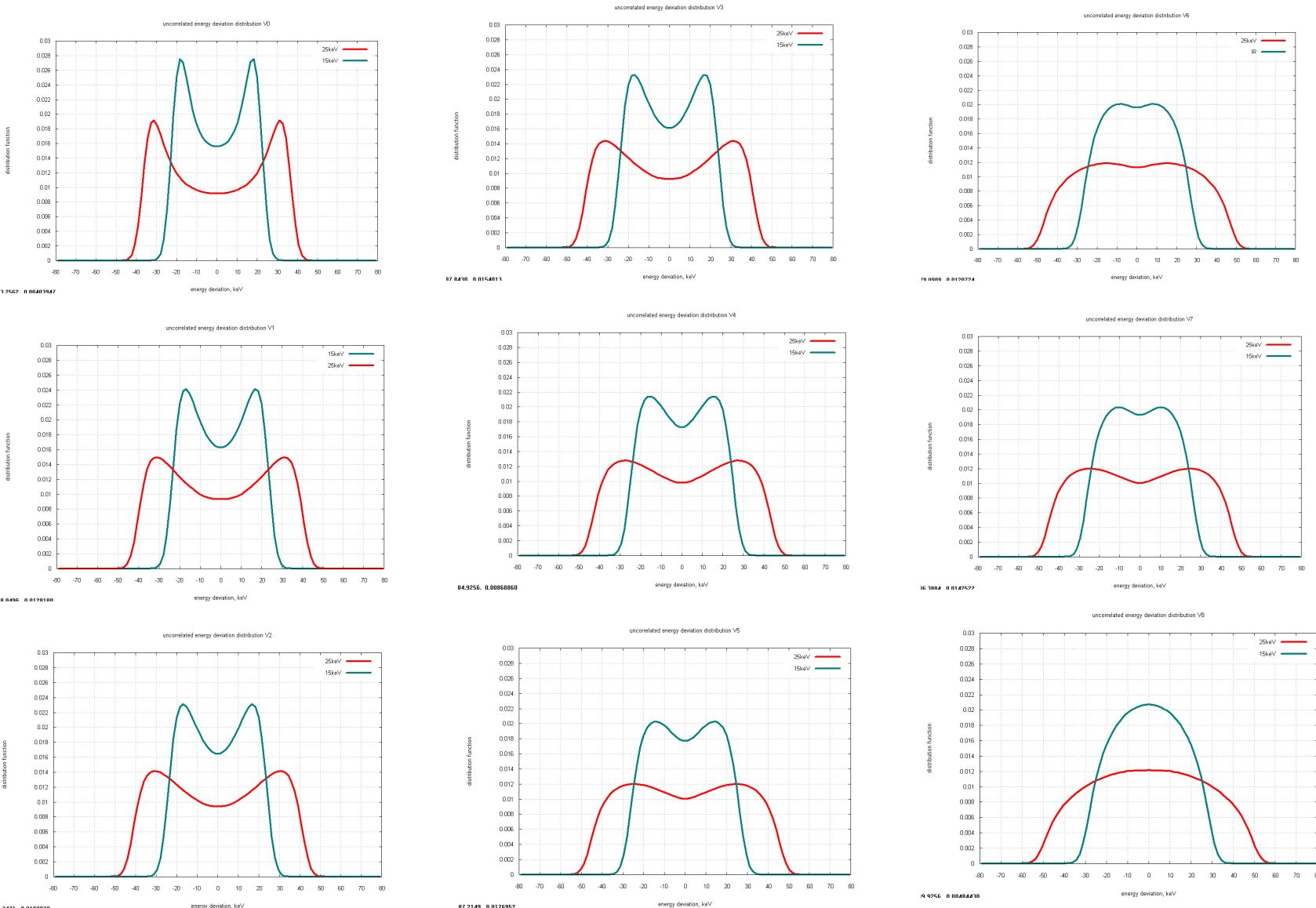
Formulas

$$f_0(z_0, \Delta\gamma_0, r) = \frac{I_0}{ec\sqrt{2\pi}\sigma_{\gamma_0}} \exp\left[-\frac{(\Delta\gamma_0 - \Delta\gamma_L(r)\sin k_L z_0)^2}{2\sigma_{\gamma_0}^2}\right] \times \frac{1}{2\pi\sigma_x^2} \exp\left(-\frac{r^2}{2\sigma_x^2}\right)$$

$$\Delta\gamma_L(r) = \sqrt{\frac{P_L}{P_0}} \frac{KL_u}{\gamma_0\sigma_r} \left[J_0\left(\frac{K^2}{4+2K^2}\right) - J_1\left(\frac{K^2}{4+2K^2}\right) \right] \exp\left(-\frac{r^2}{4\sigma_r^2}\right)$$

$$\begin{aligned} V(\Delta\gamma_0) &= 2\pi \int r dr \int dz_0 f_0(z_0, \Delta\gamma_0, r) \\ &= \frac{1}{\pi\sigma_x^2\sqrt{2\pi}\sigma_{\gamma_0}} \int r dr \exp\left(-\frac{r^2}{2\sigma_x^2}\right) \int \frac{d\xi}{\sqrt{\Delta\gamma_L(r)^2 - (\Delta\gamma_0 - \xi)^2}} \exp\left(-\frac{\xi^2}{2\sigma_{\gamma_0}^2}\right) \end{aligned}$$

Energy Distributions after Interaction with Laser Heater for V0 –V8

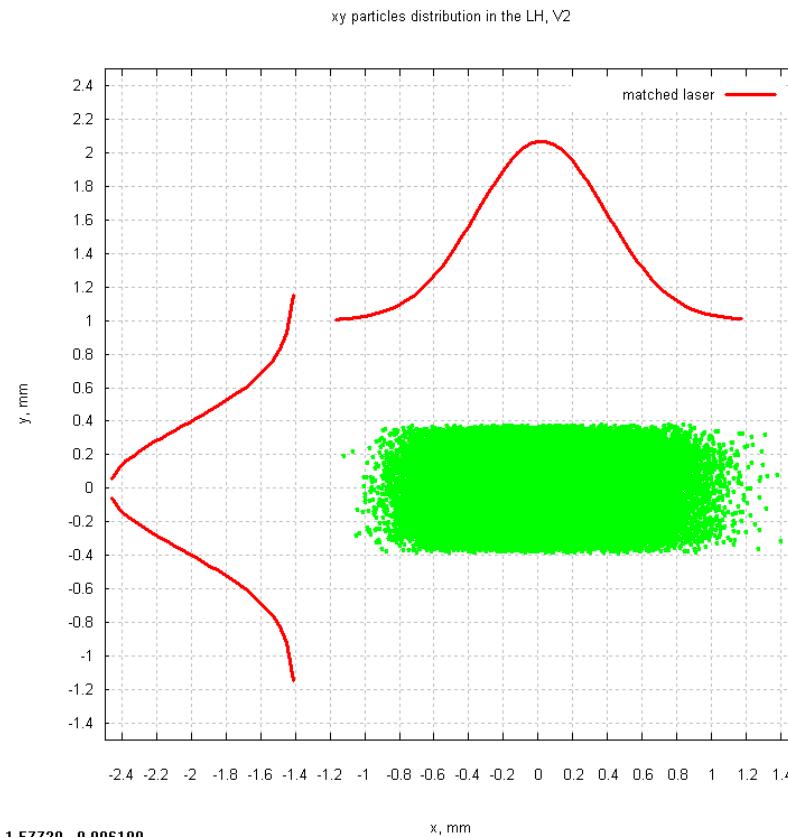


Some Parameters Concerning Laser Heater Operation for Different Working Points

Working point	$\sigma_x, \mu\text{m}$	$\sqrt{\sigma_x \sigma_y}, \mu\text{m}$	Laser peak power, MW, 25keV	Laser peak power, MW, 15keV	$\frac{\sigma_r}{\sigma_y}$	$\frac{\sigma_r}{\sqrt{\sigma_x \sigma_y}}$	$\frac{f_{\max}}{f(0)}$
V0	569	317	2.10	1.29	3.21	1.79	1.75
V1	399	265	1.20	0.74	2.25	1.51	1.48
V2	372	257	1.10	0.68	2.10	1.45	1.40
V3	385	261	1.18	0.73	2.18	1.48	1.45
V4	327	241	0.95	0.58	1.85	1.36	1.26
V5	303	232	0.90	0.55	1.71	1.31	1.16
V6	270	219	0.77	0.47	1.53	1.23	1.02
V7	279	222	0.78	0.48	1.58	1.26	1.06
V8	251	211	0.73	0.45	1.42	1.19	1.00

$$\sigma_y = 177 \mu\text{m}$$

Ideal Case: Laser Matched at Least in One Dimension



Matching shown for the Working Point 2

Formulas (ideal case)

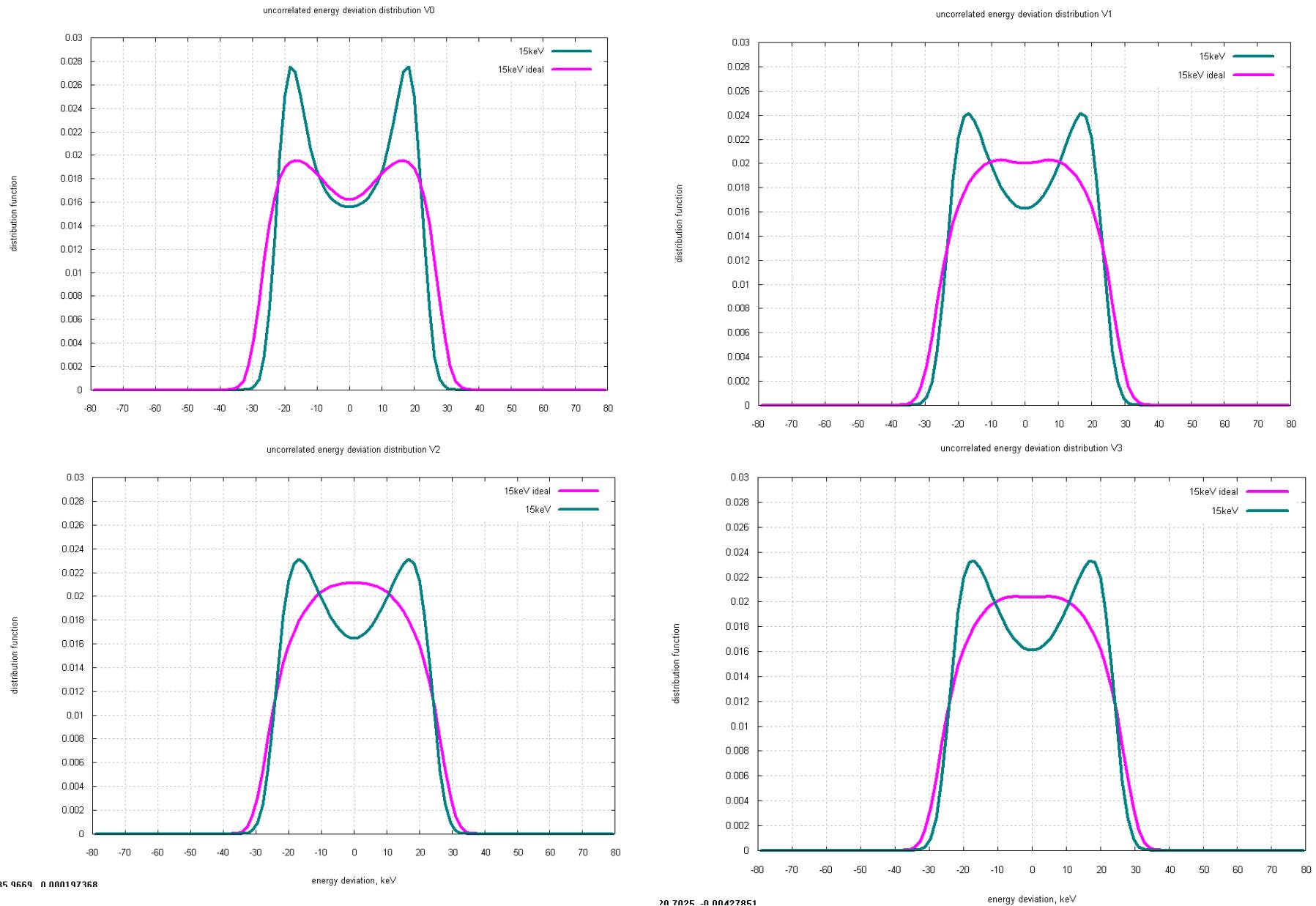
$$f_0(z_0, \Delta\gamma_0, r) = \frac{I_0}{ec\sqrt{2\pi}\sigma_{\gamma_0}} \exp\left[-\frac{(\Delta\gamma_0 - \Delta\gamma_L(r)\sin k_L z_0)^2}{2\sigma_{\gamma_0}^2}\right] \times \frac{1}{2\pi\sigma_x^2} \exp\left(-\frac{r^2}{2\sigma_x^2}\right)$$

replace σ_x by $\sqrt{\sigma_x\sigma_y}$

$$\Delta\gamma_L(r) = \sqrt{\frac{P_L}{P_0}} \frac{KL_u}{\gamma_0\sigma_r} \left[J_0\left(\frac{K^2}{4+2K^2}\right) - J_1\left(\frac{K^2}{4+2K^2}\right) \right] \exp\left(-\frac{r^2}{4\sigma_r^2}\right)$$

$$\begin{aligned} V(\Delta\gamma_0) &= 2\pi \int r dr \int dz_0 f_0(z_0, \Delta\gamma_0, r) \\ &= \frac{1}{\pi\sigma_x^2\sqrt{2\pi}\sigma_{\gamma_0}} \int r dr \exp\left(-\frac{r^2}{2\sigma_x^2}\right) \int \frac{d\xi}{\sqrt{\Delta\gamma_L(r)^2 - (\Delta\gamma_0 - \xi)^2}} \exp\left(-\frac{\xi^2}{2\sigma_{\gamma_0}^2}\right) \end{aligned}$$

Energy Distributions after Interaction with Laser Heater for V0 –V3 (ideal case)



Conclusions, margins and outlook for improvements

- Working points V5-V8 seem to be ok from the point of view chromaticity and laser heater operation. Emittance blow up is well below 10% there and the energy distribution after interaction with the laser heater has still a smooth form.
- The transverse beam form at the laser heater could be changed by change of the beam optics → it could be possible to make β_x twice as large as β_y and thus force the beam to assume more round shape.
- Alternative position for the laser heater (after the dogleg) could be considered