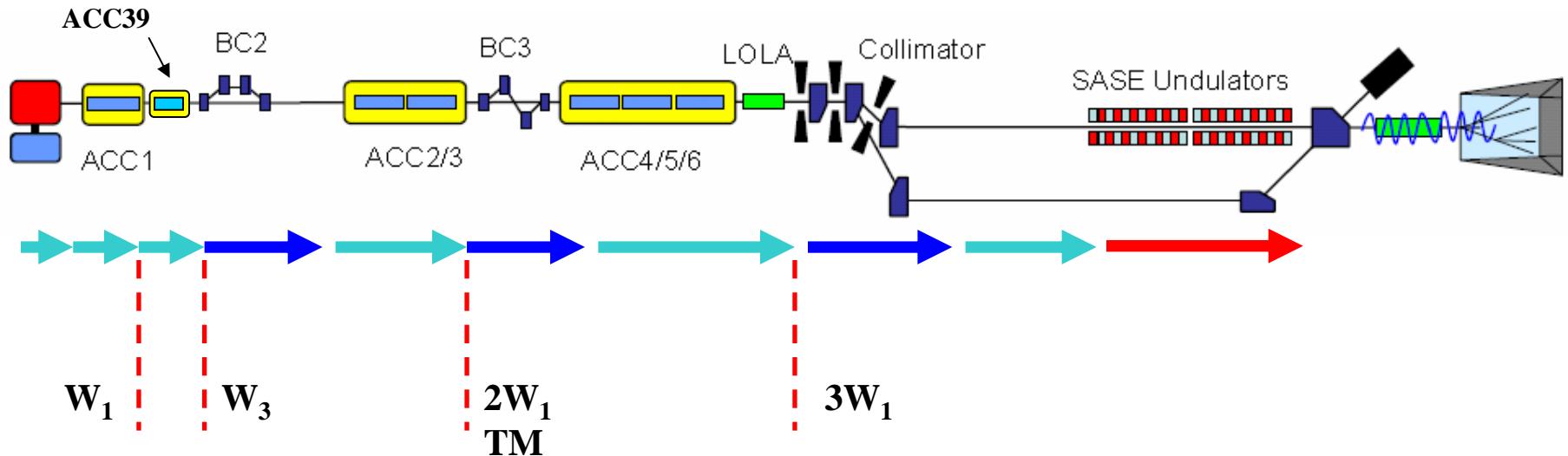


1. Example 1 (Cavity Wakes, Flash)
2. About Wakes
3. ASTRA Input
4. Some Wake Files
5. Example 2 (Resistive Wakes {per length}, Undulator)
6. More ?!



1. Example 1 (Cavity Wakes, Flash)



→ **ASTRA** (tracking with space charge, DESY)

→ **CSRtrack** (tracking through dipoles, DESY)

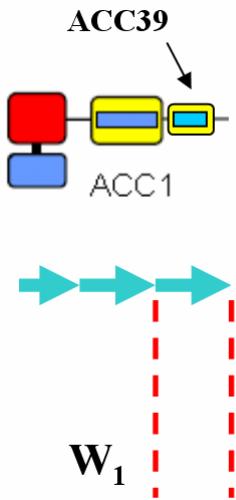
→ **ALICE** (3D FEL code, DESY)

W1 -TESLA cryomodule wake (TESLA Report 2003-19, DESY, 2003)

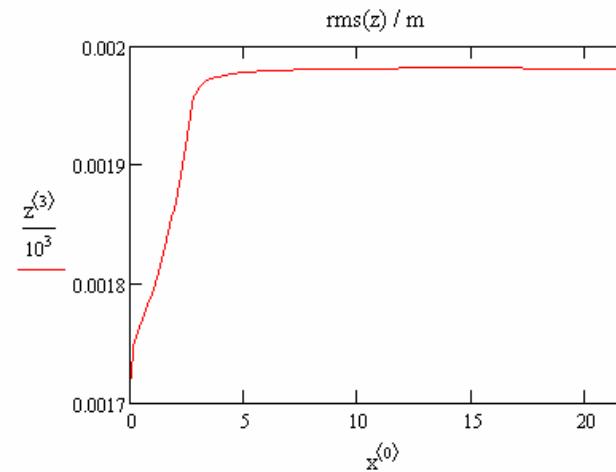
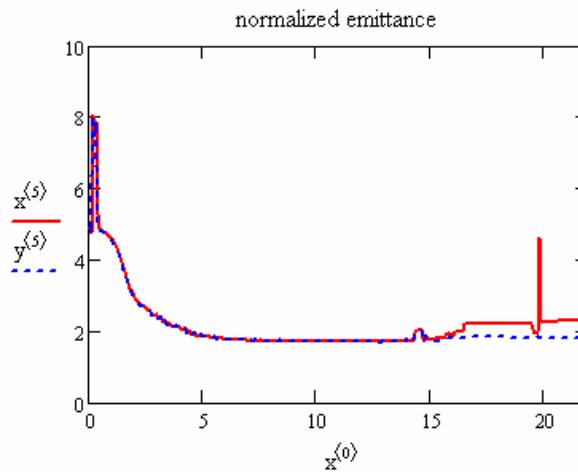
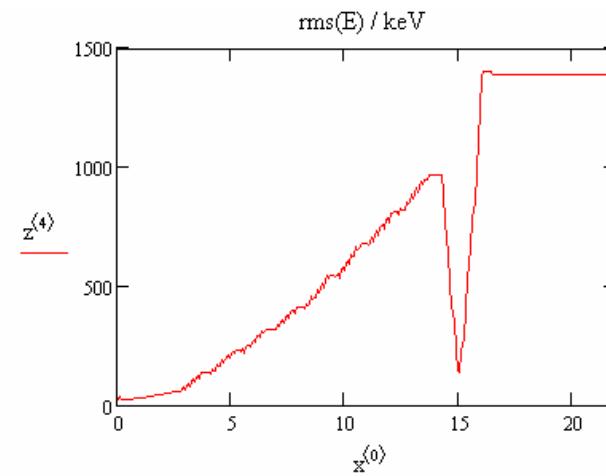
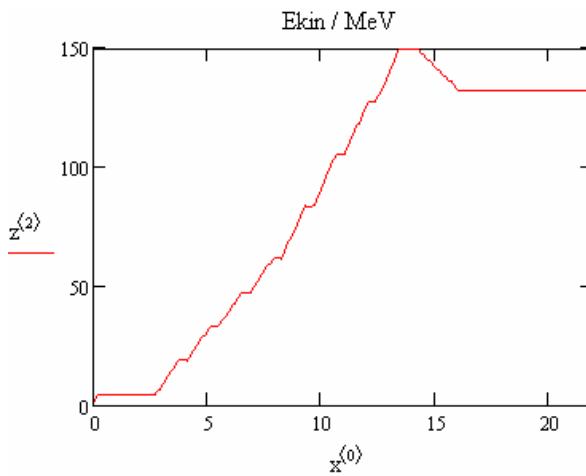
W3 - ACC39 wake (TESLA Report 2004-01, DESY, 2004)



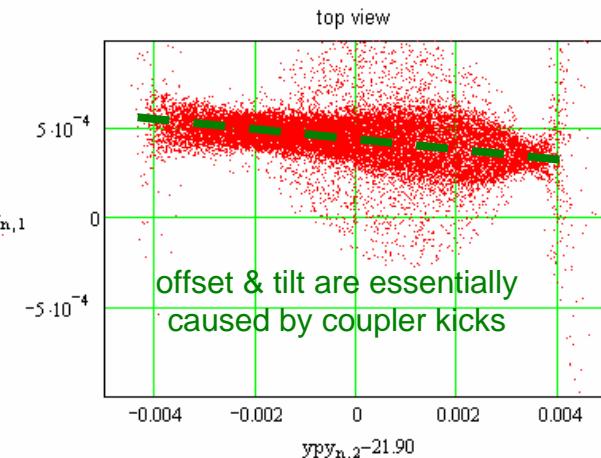
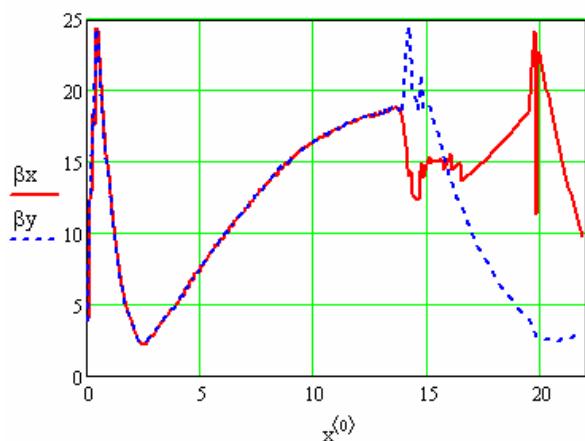
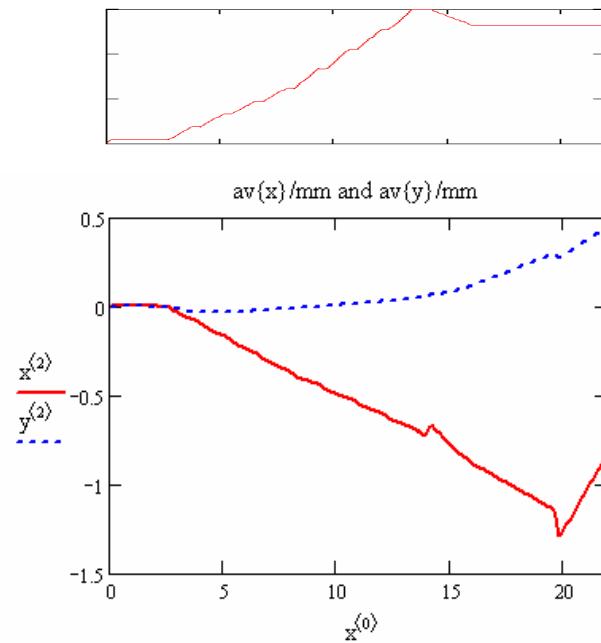
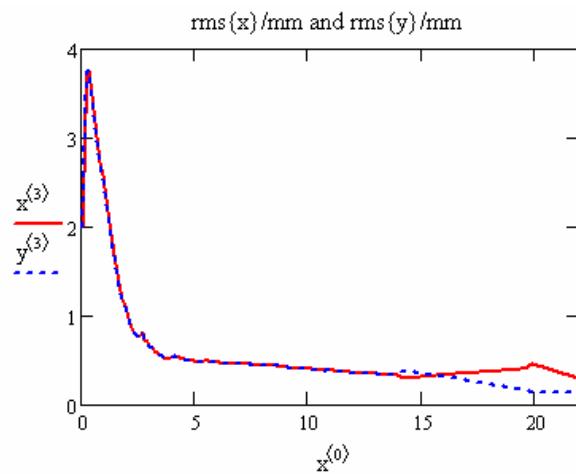
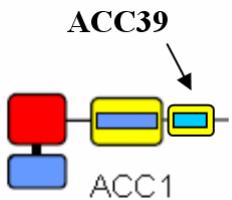
1. Example 1 (Cavity Wakes, Flash)



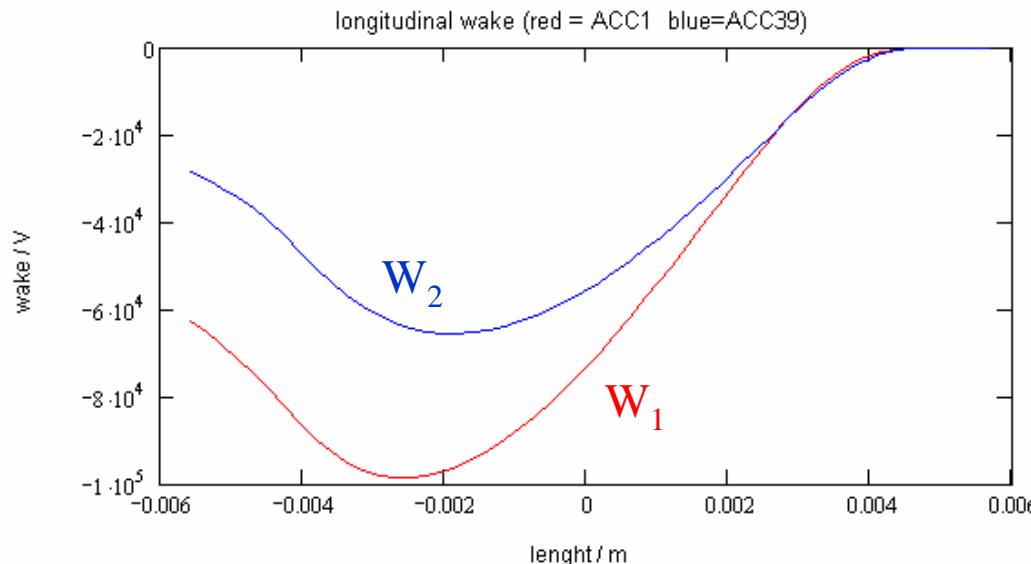
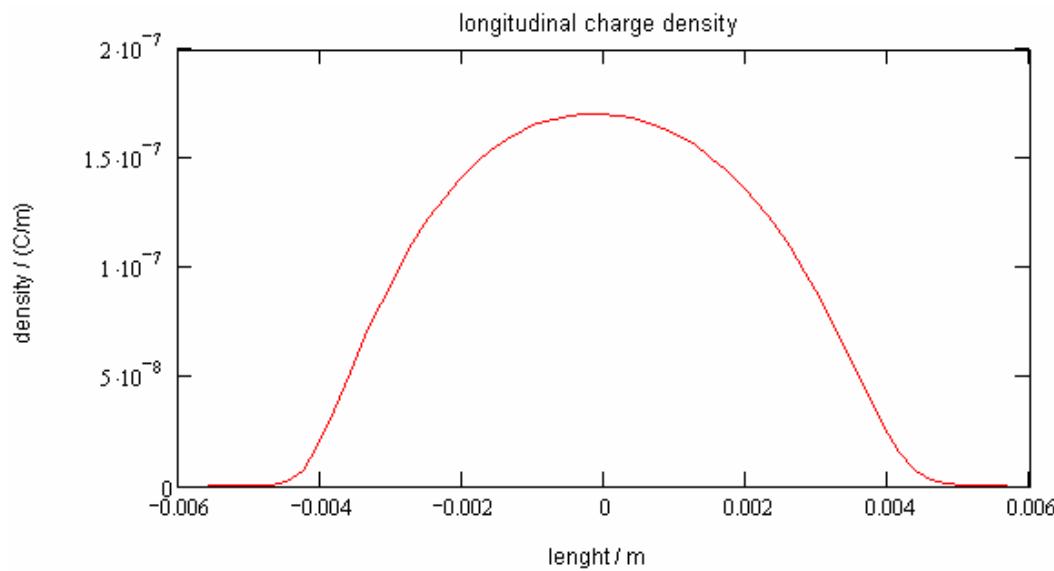
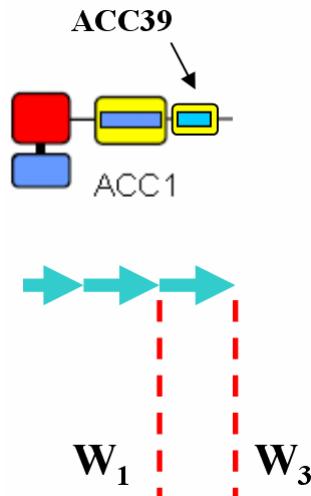
calculation with monopole- und dipole wakes
with 3D cavity fields (including coupler assymmetries)



1. Example 1 (Cavity Wakes, Flash)



1. Example 1 (Cavity Wakes, Flash)

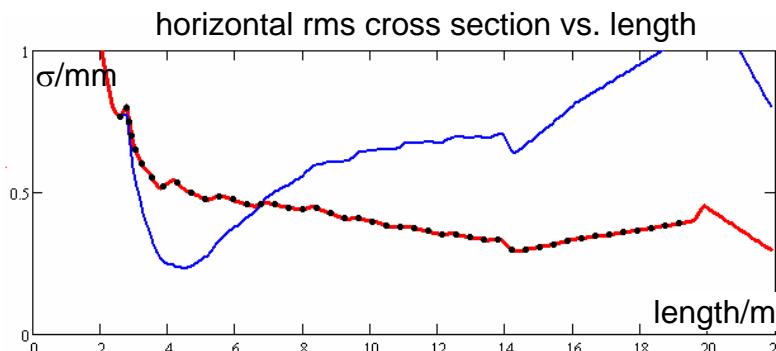


1. Example 1 (Cavity Wakes, Flash)

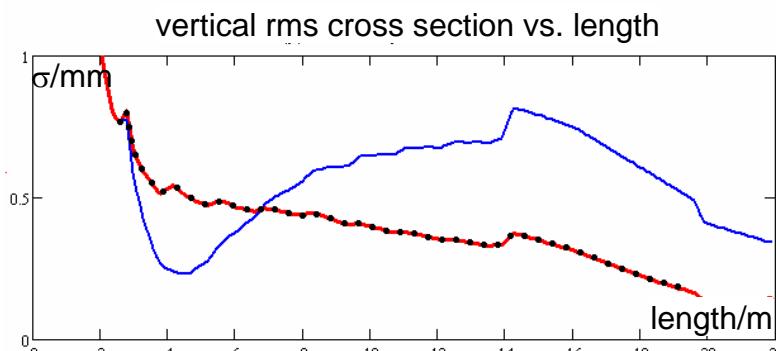
... but:

- 3d effects need 3d simulation
- more particles needed
- mirror charges in rz implemented

to be investigated:



rz run
... rz run restarted at $z=2.6\text{m}$
xyz run started at $z=2.6\text{m}$

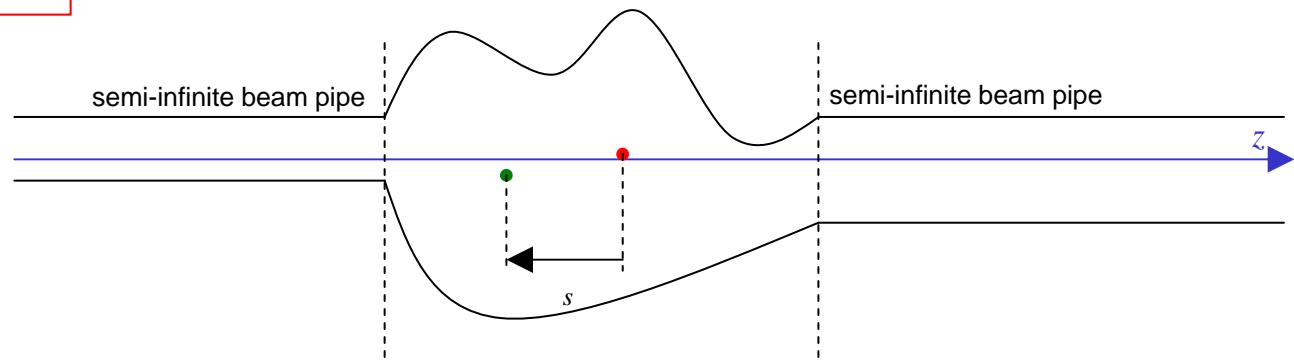


2. About Wakes

definition of wake function: 2 point particles, “C7 convention”

$$\mathbf{w}_f(u_s, v_s, u_t, v_t, s) = -\frac{c}{q_t q_s} \Delta \mathbf{p}(u_t, v_t, -s) \leftarrow \int_{-\infty}^{\infty} dz (\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

!!!



change of momentum: many particles, in principle

$$\Delta \mathbf{p}(u_t, v_t, w_t) = -\frac{q_t}{c} \sum_n q^{(n)} \mathbf{w}_f(u_n, v_n, u_n, v_t, w_s - w_t)$$

change of momentum – continuous distribution

$$\Delta \mathbf{p}(u_t, v_t, w_t) = -\frac{q_t}{c} \int \rho(u, v, r) \mathbf{w}_f(u, v, u_t, v_t, w_t - r) du dv dr$$



2. About Wakes

representation of wake function:

monopole

$$\mathbf{w}_f(u, v, u_t, v_t, s) = \mathbf{e}_w w_{m,w}(s)$$

dipole

$$\mathbf{w}_f(u, v, u_t, v_t, s) = (u\mathbf{e}_u + v\mathbf{e}_v)w_i(s) + (uu_t + vv_t)\mathbf{e}_w w_{d,w}(s)$$

$$\text{with } w_i(s) = - \int_{-\infty}^s w_{d,w}(x) dx$$

Taylor expansion

$$\mathbf{w}_f(u, v, u_t, v_t, s) = \dots + \mathbf{e}_w w_{t,w}(u, v, u_t, v_t, s)$$

with

$$w_{t,w}(u, v, u_t, v_t, s) \approx w_0(s) + \begin{bmatrix} w_1(s) \\ w_2(s) \\ w_3(s) \\ w_4(s) \end{bmatrix}^t \begin{bmatrix} u \\ v \\ u_t \\ v_t \end{bmatrix} + \begin{bmatrix} u \\ v \\ u_t \\ v_t \end{bmatrix}^t \begin{bmatrix} w_{11}(s) & w_{12}(s) & w_{13}(s) & w_{14}(s) \\ w_{12}(s) & w_{22}(s) & w_{23}(s) & w_{24}(s) \\ w_{13}(s) & w_{23}(s) & w_{33}(s) & w_{34}(s) \\ w_{14}(s) & w_{24}(s) & w_{34}(s) & -w_{33}(s) \end{bmatrix} \begin{bmatrix} u \\ v \\ u_t \\ v_t \end{bmatrix}$$

fulfills longitudinal theorem, transverse components follow from Panofsky Wenzel theorem

special case (monopole + dipole wake): $w_0(s) = w_{m,w}(s)$

$$w_{13}(s) = w_{24}(s) = 0.5w_{d,w}(s)$$

all other components vanish



2. About Wakes

transverse theorem (Panofsky Wenzel):

$$\frac{\partial}{\partial s} w_u(u, v, x_t, v_t, s) = - \frac{\partial}{\partial u_t} w_w(u, v, u_t, v_t, s)$$

$$\frac{\partial}{\partial s} w_v(u, v, u_t, v_t, s) = - \frac{\partial}{\partial v_t} w_w(u, v, u_t, v_t, s)$$

longitudinal theorem:

$$\left(\frac{\partial^2}{\partial u_t^2} + \frac{\partial^2}{\partial v_t^2} \right) w_w(u, v, u_t, v_t, s) = 0$$



2. About Wakes

$$\Delta \mathbf{p}(u_t, v_t, w_t) = -\frac{q_t}{c} \int \rho(u, v, r) \mathbf{w}_f(u, v, u_t, v_t, w_t - r) du dv dr$$

change of momentum - Taylor expansion

$$\Delta p_x(x_t, y_t, z_t) = -\frac{q_t}{c} \begin{bmatrix} w_{3i} \otimes \lambda + 2w_{13i} \otimes \lambda_x + 2w_{23i} \otimes \lambda_y \\ 2w_{33i} \otimes \lambda \\ 2w_{34i} \otimes \lambda \end{bmatrix}^t \begin{bmatrix} 1 \\ x_t \\ y_t \end{bmatrix} \quad \Delta p_y(x_t, y_t, z_t) = \dots$$

$$\Delta p_z(x_t, y_t, z_t) = -\frac{q_t}{c} \begin{bmatrix} w_0 \otimes \lambda + w_1 \otimes \lambda_x + w_2 \otimes \lambda_y + w_{11} \otimes \lambda_{xx} + 2w_{12} \otimes \lambda_{xy} + w_{22} \otimes \lambda_{yy} \\ w_3 \otimes \lambda + 2w_{13} \otimes \lambda_x + 2w_{23} \otimes \lambda_y \\ w_4 \otimes \lambda + 2w_{14} \otimes \lambda_x + 2w_{24} \otimes \lambda_y \\ 2w_{34} \otimes \lambda \\ w_{33} \otimes \lambda \end{bmatrix}^t \begin{bmatrix} 1 \\ x_t \\ y_t \\ x_t y_t \\ x_t x_t - y_t y_t \end{bmatrix}$$

with $a \otimes b = \int a(z_t) b(r + z_t) dr$

Taylor coefficients $w_0(s), w_1, w_2, w_3, w_4, w_{11}, w_{12}, w_{22}, w_{13}, w_{14}, w_{23}, w_{24}, w_{33}, w_{34}$

and 1D distribution functions:

$$\lambda(w) = \sum_n q^{(n)} \delta(w - w_n)$$

$$\lambda_u(w) = \sum_n u_n q^{(n)} \delta(w - w_n)$$

...

in continuous representation:

$$\lambda(w) = \int \rho(u, v, w) du dv$$

$$\lambda_u(w) = \int u \rho(u, v, w) du dv$$

...

→ binning & smoothing



3. ASTRA Input

logical & control

LCSR	[F]	F/T = use_not/use discrete wake kick
wk_screen()	[F]	F/T = write_not/write particle file (after kick)

location and directions

wk_x()	[0]	pointer to origin of wake unit = meter
wk_y()	[0]	
wk_z()	[1]	
wk_ex()	[0]	vector of longitudinal direction
wk_ey()	[0]	(will be normalized internally)
wk_ez()	[1]	
wk_hx()	[1]	vector of horizontal direction
wk_ty()	[0]	(will be normalized internally)
wk_tz()	[0]	

binning and smoothing

wk_equi_grid()	[T]	T/F = binning to equi grid/charge
wk_N_bin()	[10]	number of bins
wk_ip_method()	[2]	interpolation method 0/1/2 = rectangular/triangular/gaussian
wk_smooth()	[0.5]	smoothing parameter (for gaussian interpolation)

wake functions and scaling

wk_type()	['undefined']	type or method of wake calculation (character)
wk_filename()	['undefined']	file name with required information
wk_testfile()	['undefined']	file name for test output; writes test output if filename is defined
wk_scaling()	[1]	scaling factor for wake kick



3. ASTRA Input

logical & control

LCSR	[F]
wk_screen()	[F]

location and directions

wk_x()	[0]
wk_y()	[0]
wk_z()	[1]
wk_ex()	[0]
wk_ey()	[0]
wk_ez()	[1]
wk_hx()	[1]
wk_hy()	[0]
wk_hz()	[0]

defines plane of where discrete wake kick is applied and coordinate transformation

$$(\mathbf{e}_x \quad \mathbf{e}_y \quad \mathbf{e}_z) \begin{pmatrix} x_n \\ y_n \\ z_n \end{pmatrix} = \mathbf{r}_p + (\mathbf{e}_u \quad \mathbf{e}_v \quad \mathbf{e}_w) \begin{pmatrix} u_n \\ v_n \\ w_n \end{pmatrix}$$

$$(\mathbf{e}_x \quad \mathbf{e}_y \quad \mathbf{e}_z) \begin{pmatrix} p_{x,n} \\ p_{y,n} \\ p_{z,n} \end{pmatrix} = (\mathbf{e}_u \quad \mathbf{e}_v \quad \mathbf{e}_w) \begin{pmatrix} p_{u,n} \\ p_{v,n} \\ p_{w,n} \end{pmatrix}$$

(wake is calculated with respect to uvw origin)

binning and smoothing

wk_equi_grid()	[T]
wk_N_bin()	[10]
wk_ip_method()	[2]
wk_smooth()	[0.5]

binning and smoothing parameters

wake functions and scaling

wk_type()	['undefined']
wk_filename()	['undefined']
wk_testfile()	['undefined']
wk_scaling()	[1]

type or method of wake calculation (monopole/dipole/taylor) and file with wake coefficient functions



3. ASTRA Input

coefficient functions:

only longitudinal coefficients (w-component) have to be specified,
transverse coefficients follow from Panofsky Wenzel theorem

We follow the proposal of Igor Zagorodnov to describe each coefficient function by an expression of the following type:

$$w_i(s) = w_i^{(0)}(s) + \frac{\Phi(s)}{C_i} + R_i c \delta(s) - c \frac{\partial}{\partial s} [L_i c \delta(s) + w_i^{(-1)}(s)]$$

or:

$$w_{ij}(s) = w_{ij}^{(0)}(s) + \dots$$

Each coefficient function is defined by three network parameters R , L , C and by two functions $w^{(0)}(s)$ and $w^{(-1)}(s)$ that are all together described in a single table:

table _i or table _{ij} =	<table border="0"><tr><td>N_0</td><td>N_1</td></tr><tr><td>R</td><td>L</td></tr><tr><td>\tilde{C}</td><td>i or $i+10j$</td></tr><tr><td>$s_1^{(0)}$</td><td>$w^{(0)}(s_1^{(0)})$</td></tr><tr><td>$s_2^{(0)}$</td><td>$w^{(0)}(s_2^{(0)})$</td></tr><tr><td>\vdots</td><td>\vdots</td></tr><tr><td>$s_{N_0}^{(0)}$</td><td>$w^{(0)}(s_{N_0}^{(0)})$</td></tr><tr><td>$s_1^{(-1)}$</td><td>$w^{(-1)}(s_1^{(-1)})$</td></tr><tr><td>$s_2^{(-1)}$</td><td>$w^{(-1)}(s_2^{(-1)})$</td></tr><tr><td>\vdots</td><td>\vdots</td></tr><tr><td>$s_{N_1}^{(-1)}$</td><td>$w^{(-1)}(s_{N_1}^{(-1)})$</td></tr></table>	N_0	N_1	R	L	\tilde{C}	i or $i+10j$	$s_1^{(0)}$	$w^{(0)}(s_1^{(0)})$	$s_2^{(0)}$	$w^{(0)}(s_2^{(0)})$	\vdots	\vdots	$s_{N_0}^{(0)}$	$w^{(0)}(s_{N_0}^{(0)})$	$s_1^{(-1)}$	$w^{(-1)}(s_1^{(-1)})$	$s_2^{(-1)}$	$w^{(-1)}(s_2^{(-1)})$	\vdots	\vdots	$s_{N_1}^{(-1)}$	$w^{(-1)}(s_{N_1}^{(-1)})$	N_0 or N_1 or both may be zero
N_0	N_1																							
R	L																							
\tilde{C}	i or $i+10j$																							
$s_1^{(0)}$	$w^{(0)}(s_1^{(0)})$																							
$s_2^{(0)}$	$w^{(0)}(s_2^{(0)})$																							
\vdots	\vdots																							
$s_{N_0}^{(0)}$	$w^{(0)}(s_{N_0}^{(0)})$																							
$s_1^{(-1)}$	$w^{(-1)}(s_1^{(-1)})$																							
$s_2^{(-1)}$	$w^{(-1)}(s_2^{(-1)})$																							
\vdots	\vdots																							
$s_{N_1}^{(-1)}$	$w^{(-1)}(s_{N_1}^{(-1)})$																							

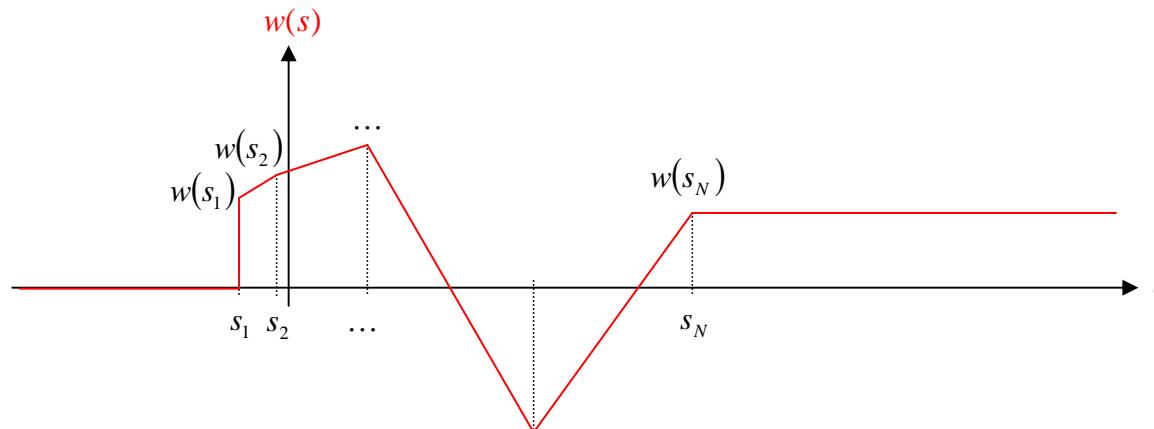


3. ASTRA Input

description of wake functions, “C7 convention”

capacitive coefficient $\frac{1}{C} = \begin{cases} 1/\tilde{C} & \text{if } \tilde{C} > 0 \\ 0 & \text{otherwise} \end{cases}$

table description of $w^{(0)}(s)$ and $w^{(-1)}(s)$:



with $s_1 < s_2 < \dots < s_N$

monopole wake function

$$\mathbf{w}_f(u, v, u_t, v_t, s) = \mathbf{e}_w w_{m,w}(s)$$

```
wk_type()      = monopole_method_f  
wk_filename() = filename
```



3. ASTRA Input

dipole wake function

$$w_f(u, v, u_t, v_t, s) = (u\mathbf{e}_u + v\mathbf{e}_v)w_i(s) + (uu_t + vv_t)\mathbf{e}_w w_{d,w}(s)$$

`wk_type() = dipole_method_f`
`wk_filename() = filename`

filename describes $w_{d,w}(s)$

the transverse wake is calculated with the Panofsky-Wenzel theorem

Taylor expansion of wake function

`wk_type() = taylor_method_f`
`wk_filename() = filename`

file describes a “multi-table” with up to 14 coefficient functions:

w_0, w_1, w_2, w_3, w_4
 $w_{11}, w_{12}, w_{22}, w_{13}, w_{14}, w_{23}, w_{24}, w_{33}, w_{34}$

format:

K	0
table 1	
table 2	
...	
table K	

K is the number of non vanishing coefficient functions
(vanishing coefficients need no sub-tables)
the order of sub-tables is arbitrary



3. ASTRA Input

other formats:

monopole wake potential

```
wk_type()      = monopole_method_p  
wk_filename() = filename
```

dipole wake potential

```
wk_type()      = dipole_method_p  
wk_filename() = filename
```



4. Some Wake Files

(A) Cavities

TESLA 2004-01 (659KB)

Wake Fields Generated by the LOLA-IV Structure and the 3rd Harmonic Section in TTF-II

Igor Zagorodnov, Thomas Weiland - TU Darmstadt;
Martin Dohlus - DESY

TESLA 2003-19 (374KB)

The Short-Range Transverse Wake Function for TESLA Accelerating Structure

Thomas Weiland, I. Zagorodnov - TEMF, TU Darmstadt

The TESLA cavity is a main element of the LINAC and it is reasonable to compare the obtained wakes to ones of the TESLA cryomodule [8]: $L_a = 8.288[m/module]$

$$w_{\parallel}^{Cryo}(s) = -\theta(s) \cdot 41.5 e^{-\sqrt{\frac{s}{1.7 \cdot 10^{-3}}}} \left[\frac{V}{pC \cdot m} \right],$$

$$w_{\perp}^{Cryo}(s) = \theta(s) \left[121 \left(1 - \left(1 + \sqrt{\frac{s}{0.92 \cdot 10^{-3}}} \right) e^{-\sqrt{\frac{s}{0.92 \cdot 10^{-3}}}} \right) \right] \left[\frac{V}{pC \cdot m \cdot m} \right].$$

The active length of the LOLA structure is $L_{total} = 3.64 m$. And the normalized short range wake functions of the LOLA read

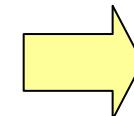
$$w_{\parallel}^{LOLA}(s) = -\theta(s) \left[70.8 e^{-\sqrt{\frac{s}{3.96 \cdot 10^{-3}}}} + 0.32 \frac{\cos(1760s^{0.72})}{\sqrt{s} + 1600s^{1.23}} \right] \left[\frac{V}{pC \cdot m} \right],$$

$$w_{\perp}^{LOLA}(s) = \theta(s) \left[2804 \left(1 - \left(1 + \sqrt{\frac{s}{11.7 \cdot 10^{-3}}} \right) e^{-\sqrt{\frac{s}{11.7 \cdot 10^{-3}}}} \right) + 2530\sqrt{s} \right] \left[\frac{V}{pC \cdot m \cdot m} \right].$$

The active length of the 3rd harmonic section is $L_{total} = 36 \cdot 0.03844 = 1.3838 m$. And the normalized short range wake functions of the section read

$$w_{\parallel}^{3rd}(s) = -\theta(s) \left[230 e^{-\sqrt{\frac{s}{8.4 \cdot 10^{-4}}}} + 0.65 \frac{\cos(5830s^{0.83})}{\sqrt{s} + 195s} + 0.026\delta(s) \right] \left[\frac{V}{pC \cdot m} \right],$$

$$w_{\perp}^{3rd}(s) = \theta(s) \left[1612 \left(1 - \left(1 + \sqrt{\frac{s}{0.56 \cdot 10^{-3}}} \right) e^{-\sqrt{\frac{s}{0.56 \cdot 10^{-3}}}} \right) + 3932\sqrt{s} + 64 \right] \left[\frac{V}{pC \cdot m \cdot m} \right].$$



Name	Size
LOLA_CAVITY_WAKE_DIPOLE.dat	821 KB
LOLA_CAVITY_WAKE_MONO.dat	1.641 KB
LOLA_CAVITY_WAKE_TAYLOR.dat	3.282 KB
TESLA_MODULE_WAKE_DIPOLE.dat	821 KB
TESLA_MODULE_WAKE_MONO.dat	821 KB
TESLA_MODULE_WAKE_TAYLOR.dat	2.462 KB
THIRD_HARMONIC_SECTION_WAKE_DIPOLE.dat	821 KB
THIRD_HARMONIC_SECTION_WAKE_MONO.dat	1.641 KB
THIRD_HARMONIC_SECTION_WAKE_TAYLOR.dat	3.282 KB

..._MONO = monopole wake

..._DIPOLE = dipole wake

..._TAYLOR = monopole & dipole wake
(together)



4. Some Wake Files

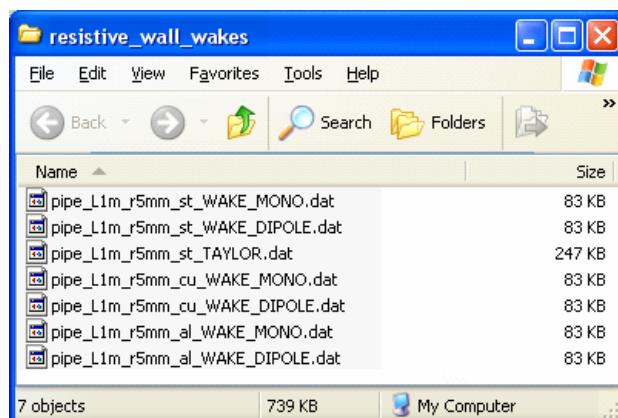
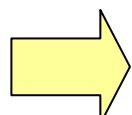
(B) resistive walls (round pipes)

monopole- and dipole impedance functions (**per length**)

$$\mathbf{Z}^{(m)}(x, y, x_t, y_t, \omega) = \frac{Z_s}{2\pi R} \frac{1}{1 + jk \frac{R}{2} \frac{Z_s}{Z_0}} \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

$$\mathbf{Z}^{(d)}(x, y, x_t, y_t, \omega) \approx \frac{Z_s}{2\pi R} \frac{2}{R^2} \frac{1}{1 + jk \frac{R}{2} \frac{Z_s}{Z_0}} \begin{pmatrix} jx/k \\ jy/k \\ xx_t + yy_t \end{pmatrix}$$

for usual beam parameters (not ultra-long bunches)



and wakes (**per length**)

$$\mathbf{w}^{(m)}(x, y, x_t, y_t, s) = \begin{pmatrix} 0 \\ 0 \\ w_r(s) \end{pmatrix}$$

$$\mathbf{w}^{(d)}(x, y, x_t, y_t, s) \approx \begin{pmatrix} \dots \\ \dots \\ \frac{2w_r(s)}{R^2}(xx_t + yy_t) \end{pmatrix}$$

wakes for 1m beam pipe with 5mm radius
for Al, Cu and steel (for frequency dependant conductivity)

use [wk_scaling\(\)](#) for different length



5. Example 2 (Resistive Wakes {per length}, Undulator)

emittance growth in a FLASH-like undulator due to resistive wall wakes:

Holger's DA:
Resistive Wall Wake Fields

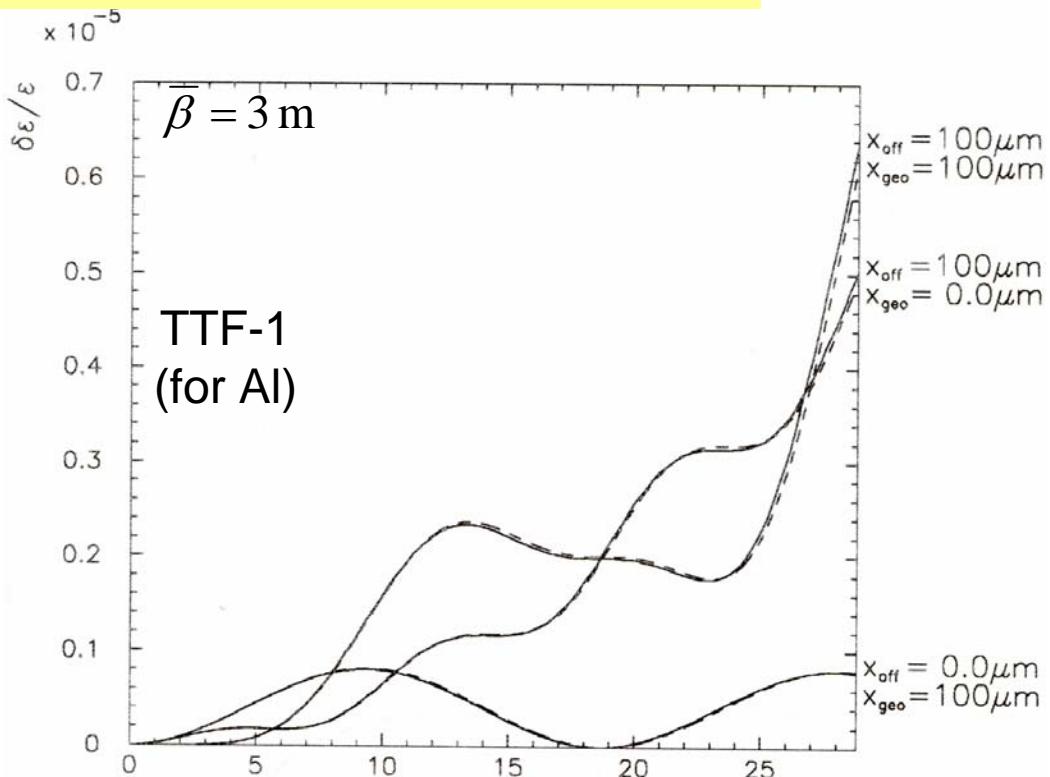
Diplomarbeit
 zur Erlangung des Grades
 eines Diplomphysikers

vorgelegt dem Fachbereich Physik
 der Universität Hamburg
 von Holger Schlarb

Hamburg
 August 1997

analytic estimation:

$$\frac{\delta\epsilon_x(s)}{\epsilon_x} \approx \frac{1}{2\epsilon_x} \cdot \left(\frac{Ne^2}{E_0} \right)^2 \cdot \left(\langle W_{\perp}^{\lambda^2} \rangle_{\lambda} - k_{\perp}^2 \right) \times \left\{ \left(\frac{x_{off}\sqrt{\beta}}{2} s \sin(k_{\beta}s) - x_{geo} \beta^{3/2} [1 - \cos(k_{\beta}s)] \right)^2 + \left(\frac{x_{off}\sqrt{\beta}}{2} [s \cos(k_{\beta}s) + \beta \sin(k_{\beta}s)] - x_{geo} \beta^{3/2} \sin(k_{\beta}s) \right)^2 \right\} . \quad (3.5)$$



5. Example 2 (Resistive Wakes {per length}, Undulator)

ASTRA input:

&NEWRUN

Version=2

Head='FODO LP=0.96m beta_av=3m'

Distribution=particles.ini

...

/

&OUTPUT

ZSTART = 0.000

ZSTOP = 30.000

...

/



30 m undulator

&SCAN

/

&MODULES

/

&ERROR

/

&CHARGE

LSPCH =F

...

/



no space charge forces



5. Example 2 (Resistive Wakes {per length}, Undulator)

ASTRA input:

```
&CSR
LCSR=T
WK_X          (1)=0.001
WK_Z          (1)=0.47
WK_EQUI_GRID(1)=T
WK_N_BIN      (1)=50
WK_TYPE       (1)='taylor_method_f'
WK_IP_METHOD(1)=2
WK_SMOOTH     (1)=1.0
WK_FILENAME   (1)='pipe_L1m_r5mm_st_TAYLOR.dat'
WK_SCALING    (1)=0.48
WK_SCREEN     (1)=T
• • •

WK_X          (62)=0.001
WK_Z          (62)=29.75
WK_EQUI_GRID(62)=T
WK_N_BIN      (62)=50
WK_TYPE       (62)='taylor_method_f'
WK_IP_METHOD(62)=2
WK_SMOOTH     (62)=1.0
WK_FILENAME   (62)='pipe_L1m_r5mm_st_TAYLOR.dat'
WK_SCALING    (62)=0.48
/
```

name list “CSR” for wakes!

62 x wake elements in
half-fodo cells

1 mm offset

R = 5 mm beam pipe
from steel



5. Example 2 (Resistive Wakes {per length}, Undulator)

ASTRA input:

```
&APERTURE  
/  
  
&CAVITY  
/  
  
&SOLENOID  
/  
  
&QUADRUPOLE  
LQUAD           =T  
  
Q_length(1)=0.1365  
Q_K(1)      =5.625472  
! Q_Bore(1)  =0.0000001  
Q_pos(1)    =0.24  
  
Q_length(2)=0.1365  
Q_K(2)      =-5.625472  
! Q_Bore(2)  =0.0000001  
Q_pos(2)    =0.72  
  
• • •  
  
/  
  
&DIPOLE  
/
```

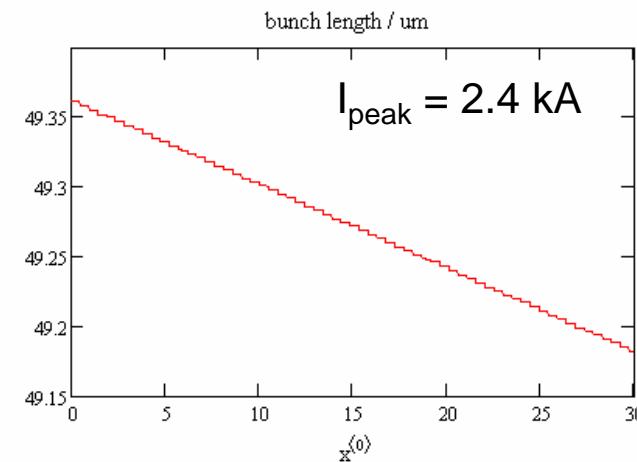
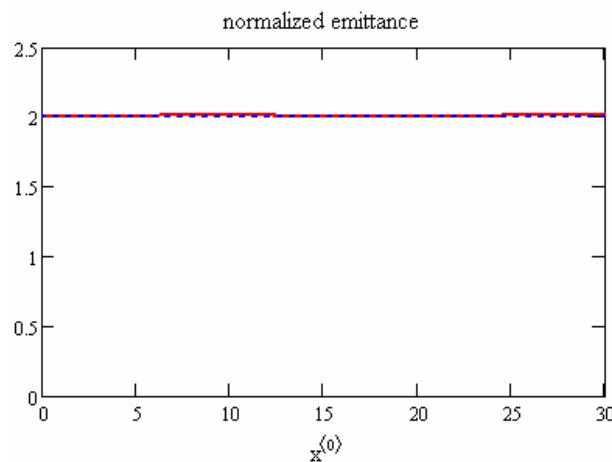
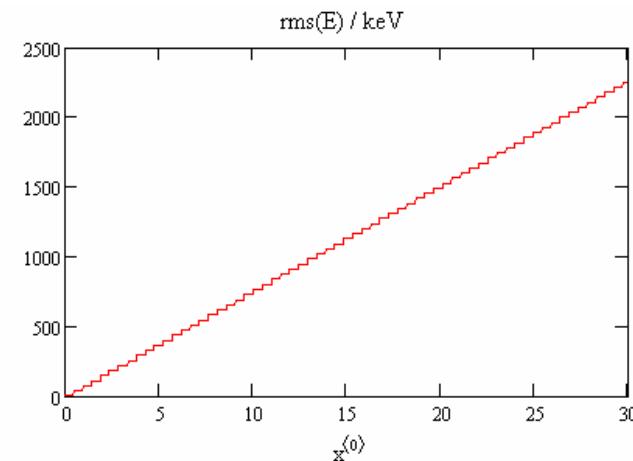
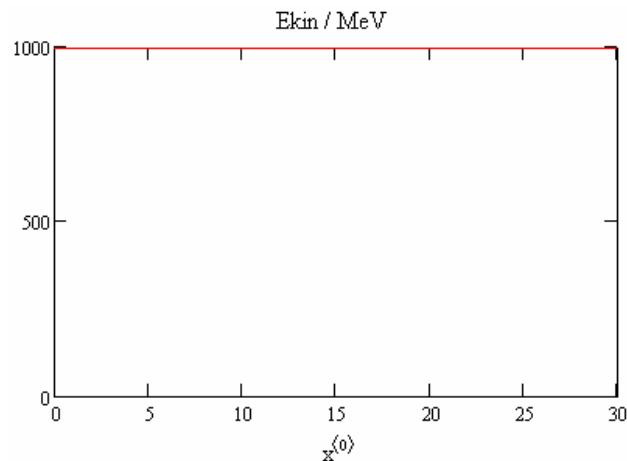


fodo lattice with
 $L_p=0.9600\text{m}$, $L_q=0.1365\text{m}$, $k_q=5.625472\text{m}^{-2}$
(av. beta function is $\approx 3.0\text{m}$)



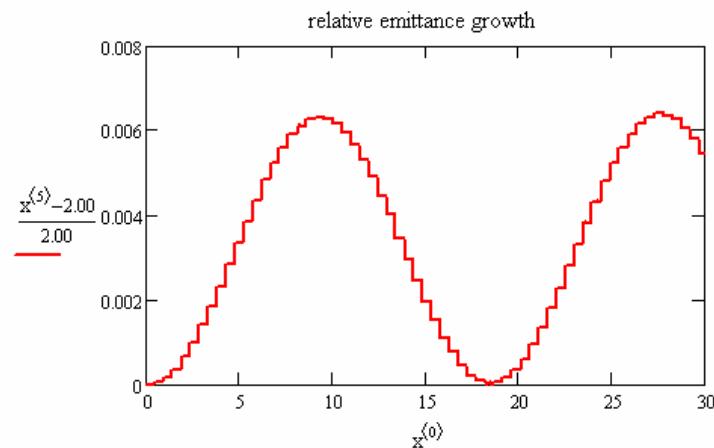
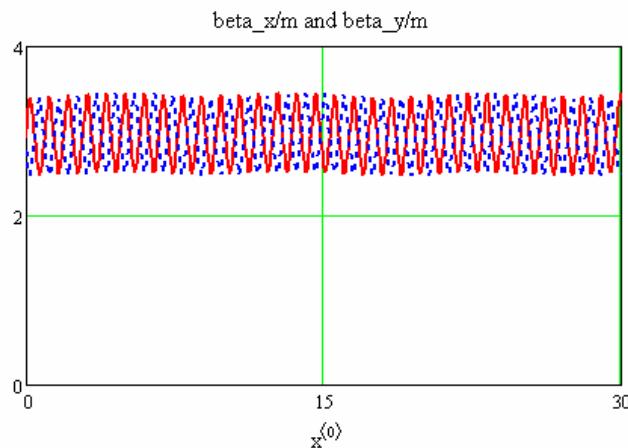
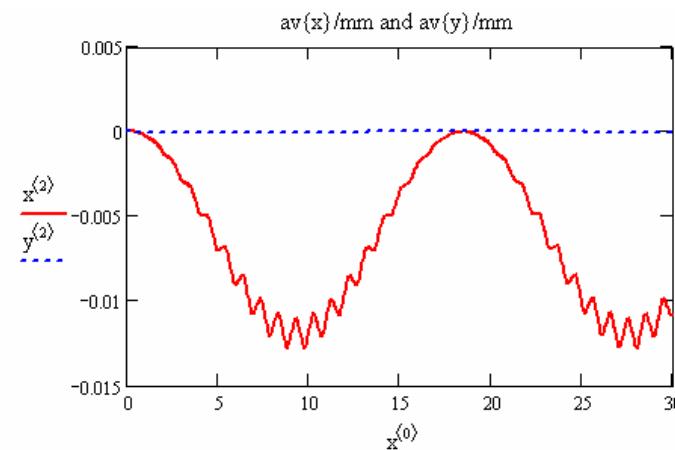
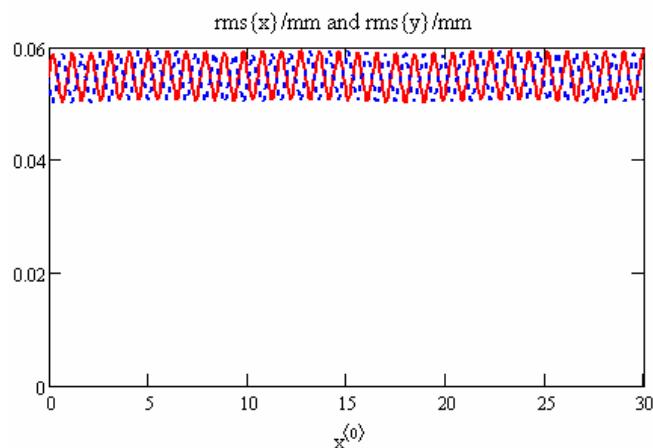
5. Example 2 (Resistive Wakes {per length}, Undulator)

some results:



5. Example 2 (Resistive Wakes {per length}, Undulator)

some results:



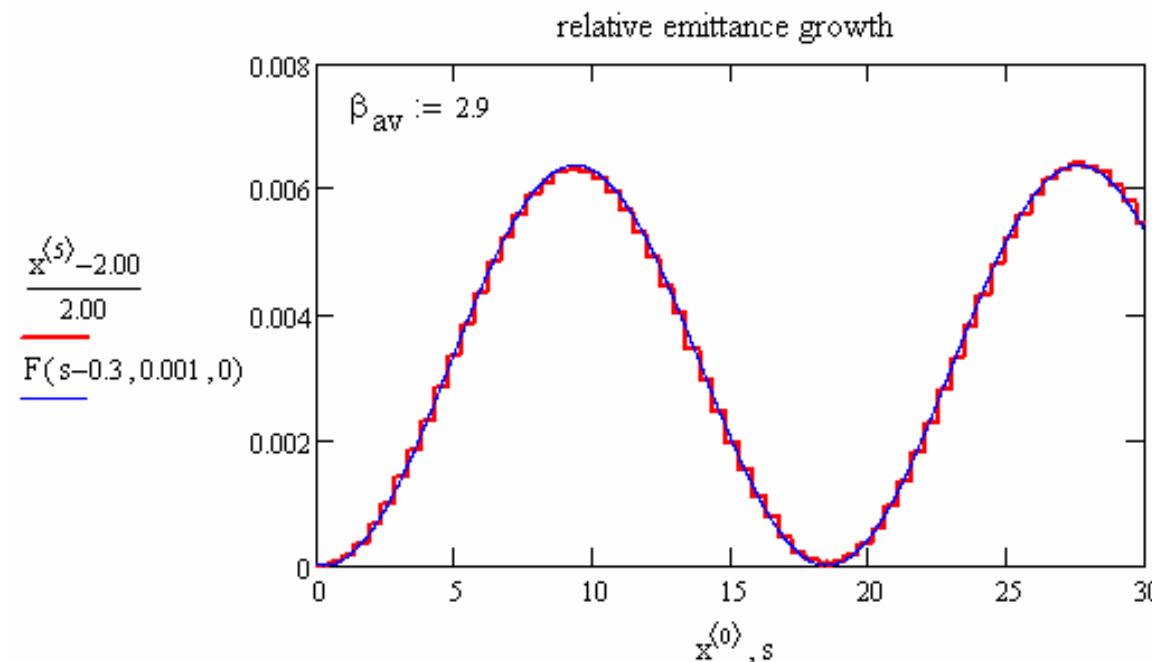
5. Example 2 (Resistive Wakes {per length}, Undulator)

comparison with analytic estimation for averaged beta function:

$$\text{fact} := \frac{1}{2 \cdot \epsilon_x} \left(\frac{q_b}{E_0} \right)^2 \cdot \left(\frac{1}{q} \cdot \text{rms}(s, \lambda, \text{TWake_st_tr}) \right)^2$$

fact = 65.371

$$F(s, x_{\text{geo}}, x_{\text{off}}) := \text{fact} \cdot \left[\left[\frac{x_{\text{off}} \sqrt{\beta_{\text{av}}}}{2} \cdot s \cdot \sin\left(\frac{s}{\beta_{\text{av}}}\right) - x_{\text{geo}} \cdot \beta_{\text{av}}^{\frac{3}{2}} \cdot \left(1 - \cos\left(\frac{s}{\beta_{\text{av}}}\right)\right) \right]^2 + \left[\frac{x_{\text{off}} \sqrt{\beta_{\text{av}}}}{2} \cdot \left(s \cdot \cos\left(\frac{s}{\beta_{\text{av}}}\right) + \beta_{\text{av}} \cdot \sin\left(\frac{s}{\beta_{\text{av}}}\right)\right) - x_{\text{geo}} \cdot \beta_{\text{av}}^{\frac{3}{2}} \cdot \sin\left(\frac{s}{\beta_{\text{av}}}\right) \right]^2 \right]$$



6. More ?!

to be done: wakes per length

projected CSR in ASTRA – a second attempt?

MATLAB tool in preparation:

test binning and smoothing

use (and test) wake files without ASTRA

