

# Simulating Hysteresis and Remanence in Accelerator Magnets

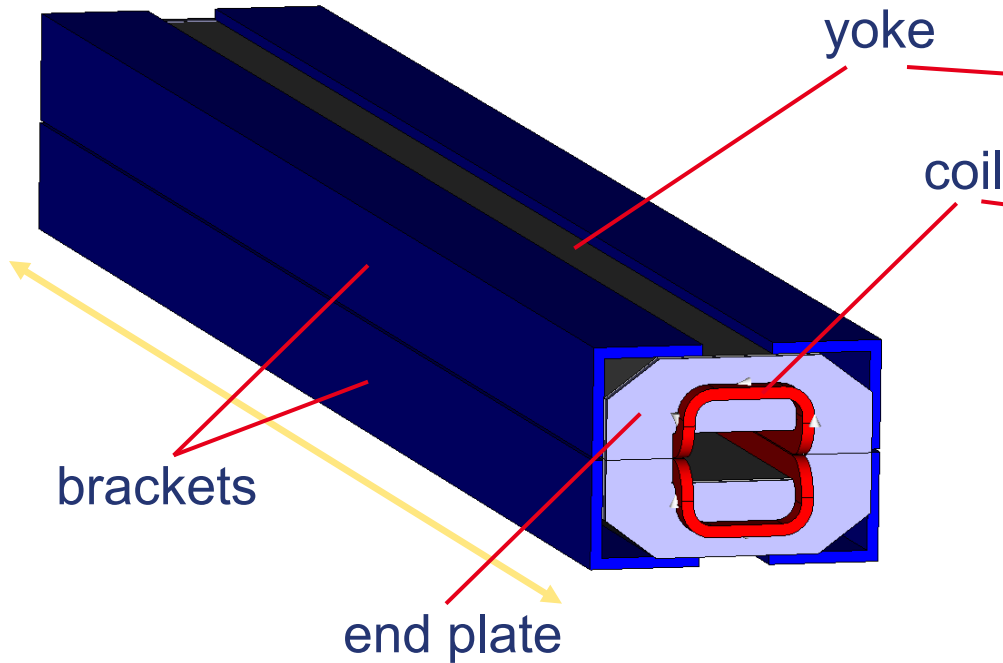


TECHNISCHE  
UNIVERSITÄT  
DARMSTADT

Herbert De Gersem, Stephan Koch, Ulrich Römer, Sebastian Schöps



# Example: GSI-SIS-100 magnet



SIS100 dipole (prototype)

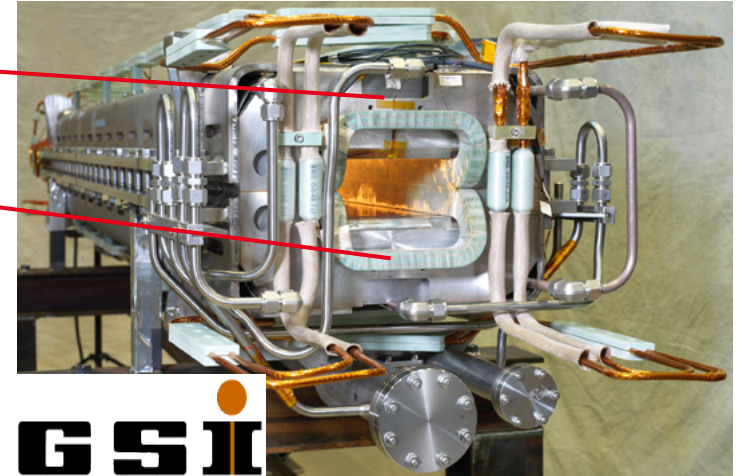
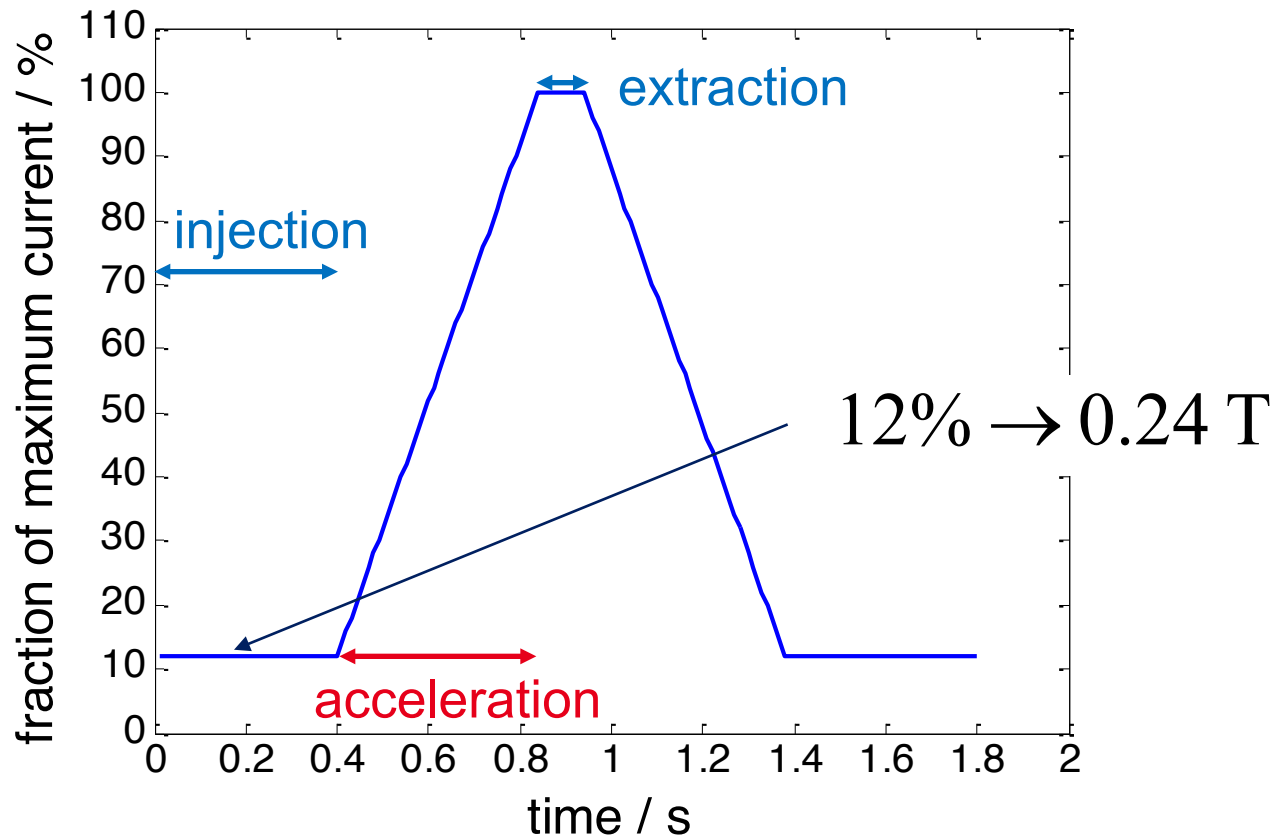


photo: J. Guse, GSI ([www.gsi.de](http://www.gsi.de))

length: 3 m

# Example: GSI-SIS-100 magnet

## excitation profile



# Magnetoquasistatic formulation



differential equation:

$$\nabla \times (\nu \nabla \times \vec{A}) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$$

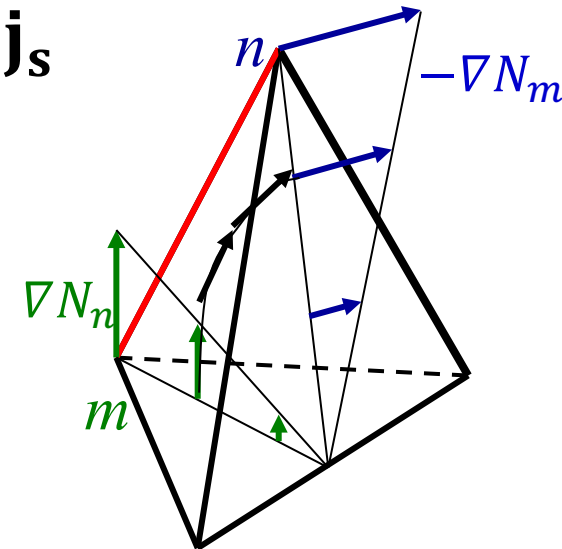
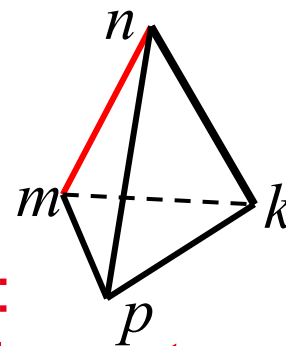
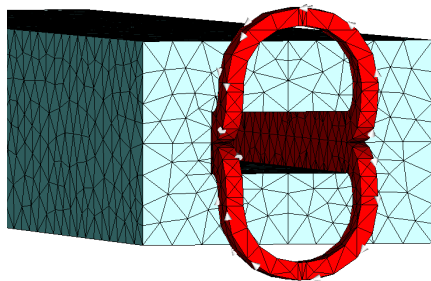
reluctivity  
magnetic vector potential  
conductivity  
applied current density

# Discretisation in space

differential equation:  $\nabla \times (v \nabla \times \vec{A}) + \sigma \frac{\partial \vec{A}}{\partial t} = \vec{J}_s$

spatial discretisation  $\vec{A}(x, y, z) = \sum_j u_j \vec{v}_j(x, y, z)$

semi-discrete system:  $\mathbf{K}_v \mathbf{a} + \mathbf{M}_\sigma \frac{d\mathbf{a}}{dt} = \mathbf{j}_s$



shape functions:  
edge finite elements  
(curl-conforming)  $\vec{v}(\vec{x}) = N_m \nabla N_n - N_n \nabla N_m$

# Discretisation in time

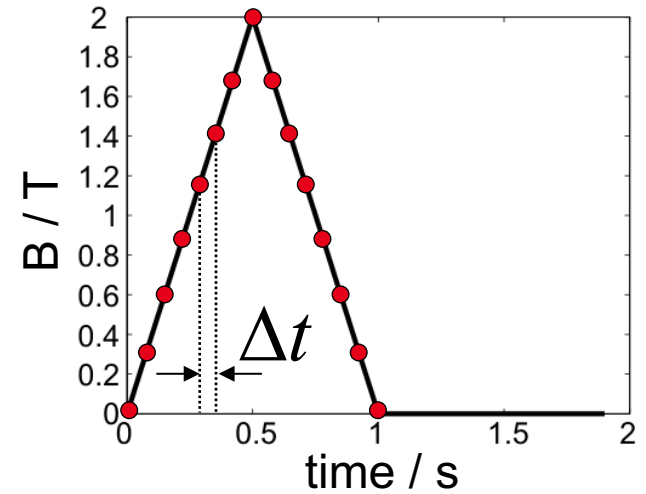
differential equation

spatial discretisation

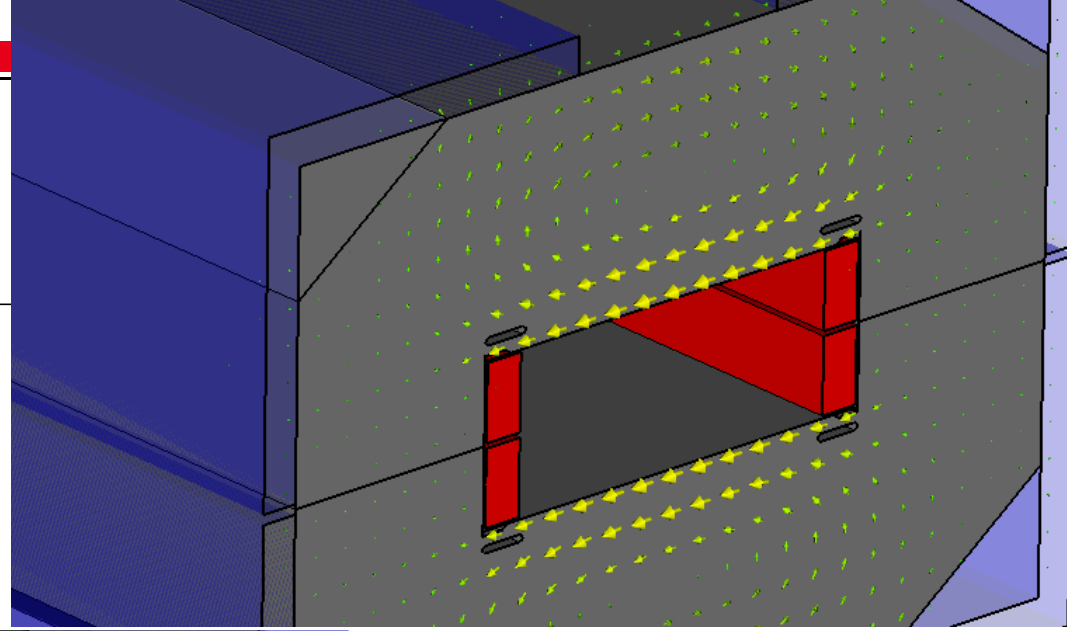
semi-discrete system:  $\mathbf{K}_v \mathbf{a} + \mathbf{M}_\sigma \frac{d\mathbf{a}}{dt} = \mathbf{j}_s$

temporal discretisation

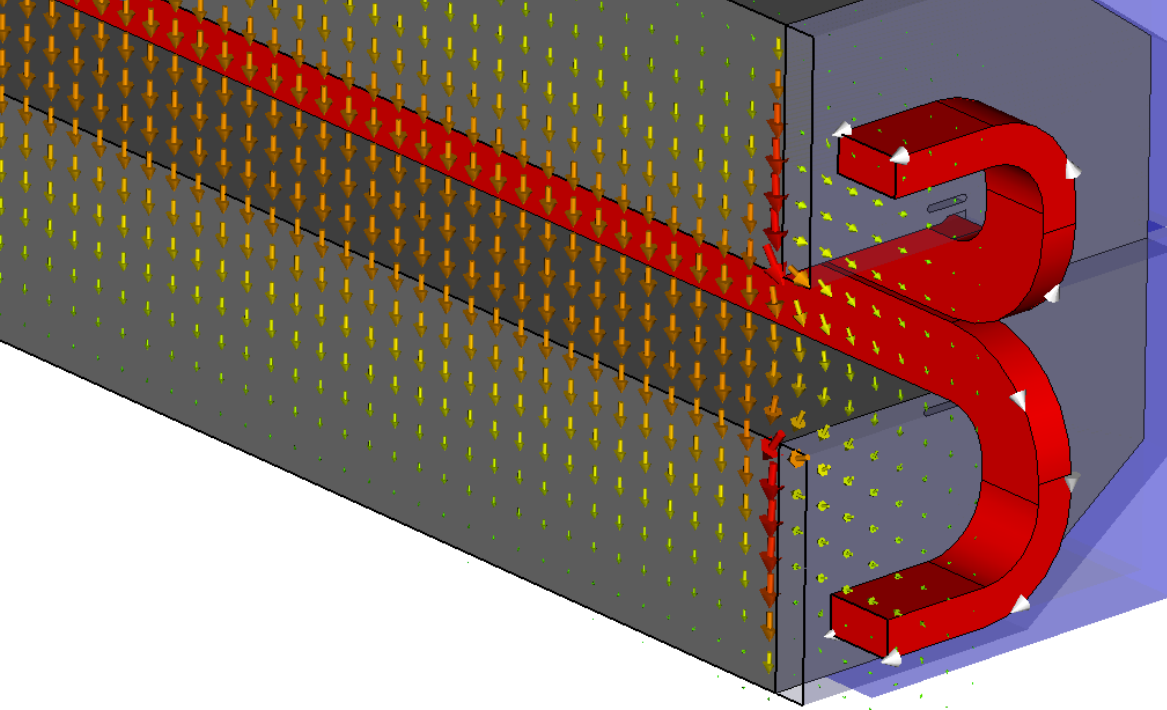
discrete system:  $(\mathbf{K}_v + \alpha \mathbf{M}_\sigma) \mathbf{a} = \mathbf{RHS}$



# Results



magnetic field

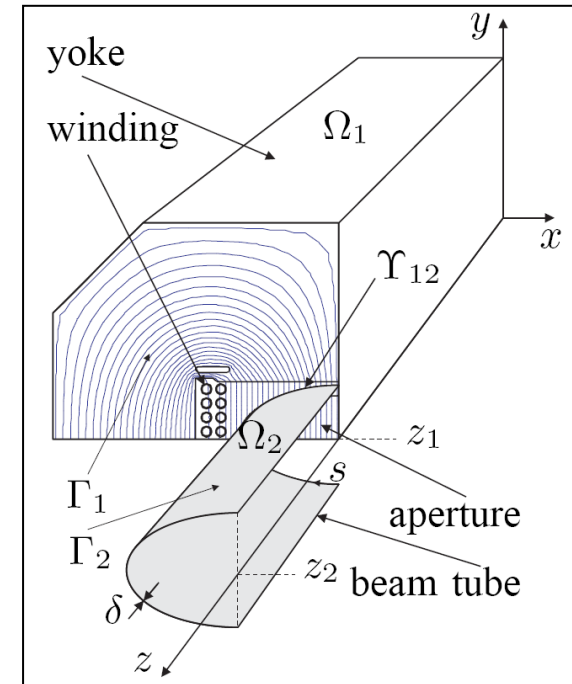
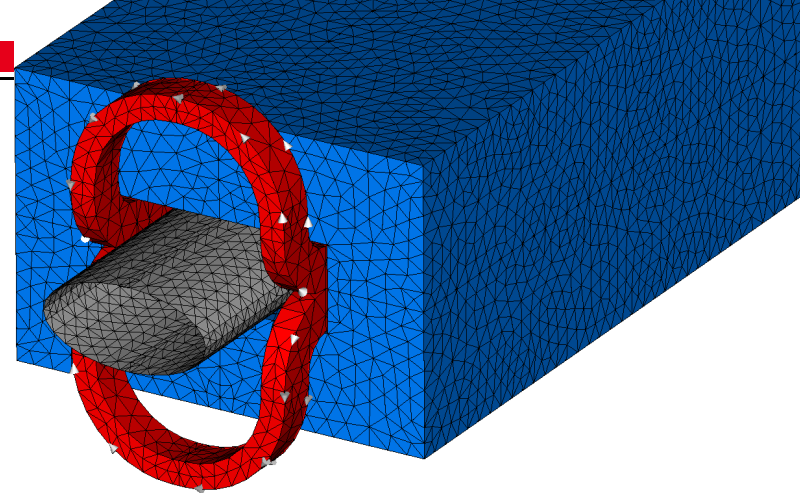


eddy currents  
in the end plane

simulation by  
CST EMStudio®

# Overview

- magnet simulation (standard 3D FE solver)
- challenges
  - geometrical details
  - materials
  - transient effects
  - high accuracy
- magnet simulation (dedicated 3D FE solver)
- hysteresis modelling
- conclusions





# Challenge 1: Detailed geometry

## yoke

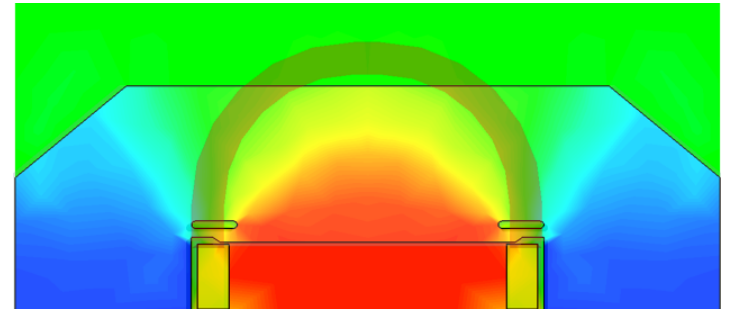
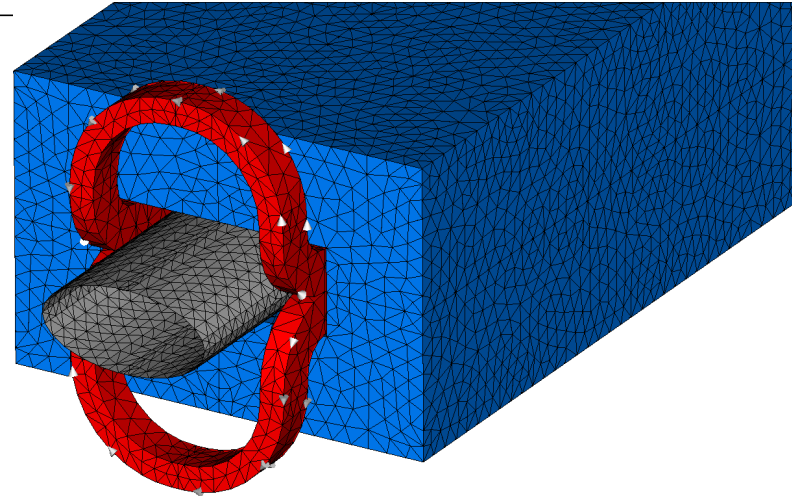
- length (meter)  
vs. lamination thickness (mm)
- shimming, holes

## beam tube

- < 1mm thick

## end-winding parts

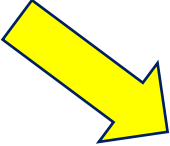
- determine the eddy currents  
in the end plates



# Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)


$$\bar{\underline{v}}^{\mathbf{r}}(B) = R^T \begin{bmatrix} \nu_{\text{rol}} & & \\ & \nu_{\text{trans}} & \\ & & \nu_{\text{trans}} \end{bmatrix} R$$

$\nu_{\text{rol}}$  reluctivity in the rolling direction

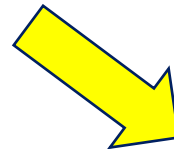
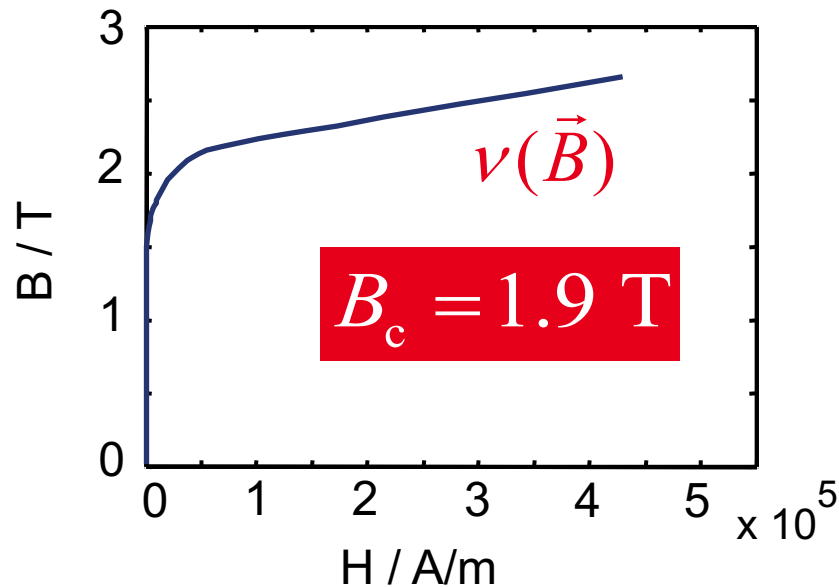
$\nu_{\text{trans}}$  reluctivity in the transversal direction

$R$  local rotation matrix

# Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)

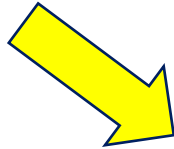


Newton method

# Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)



Jiles-Atherton model

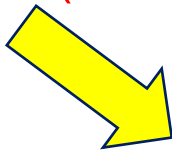
Preisach model

estimation of losses by Steinmetz-Bertotti

# Challenge 2: Materials

## yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- **composite (lamination)**

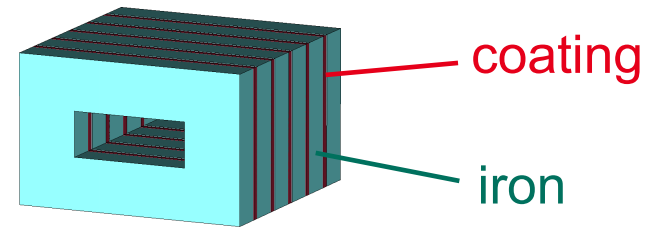


(simple) homogenisation  
along lamination direction

perpendicular to laminates

stacking factor

$$\gamma_{st} \approx 0.95 \leq \sim 1$$



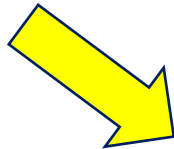
$$\frac{1}{\nu_{xy}} = \frac{\gamma_{st}}{\nu_{Fe}} + \frac{1 - \gamma_{st}}{\nu_0}$$

$$\nu_z = \gamma_{st} \nu_{Fe} + (1 - \gamma_{st}) \nu_0$$

# Challenge 2: Materials

yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- composite (lamination)
- **variability**



stochastics, sensitivity

(see recent research  
of Ulrich Römer and Sebastian Schöps, TU Darmstadt)

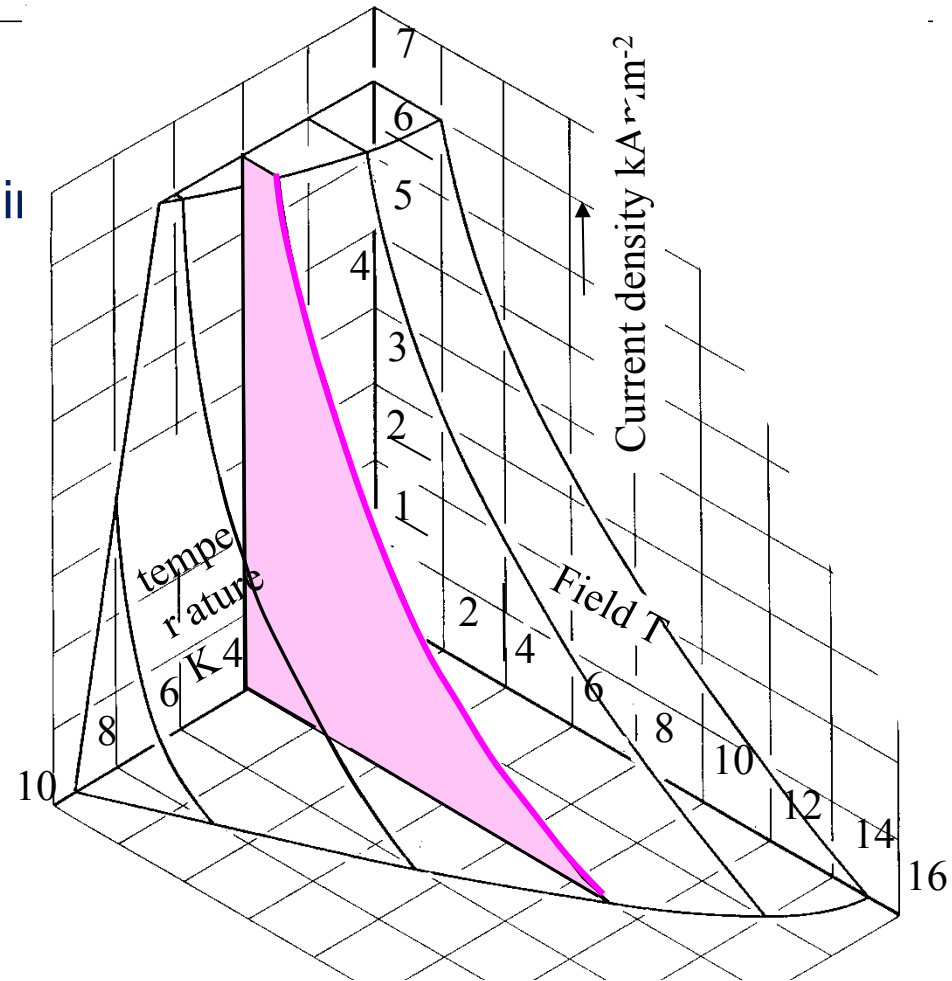
# Challenge 2: Materials

## yoke iron:

- anisotropic (rolling & transverse direction)
- nonlinear (saturation)
- hysteretic (remanent field)
- composite (lamination)
- variability

## superconductor:

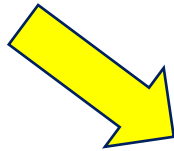
- critical current
- temperature
- magnetic field



# Challenge 3: Transient phenomena

## lamination

- hysteresis + remanence



Jiles-Atherton model

Preisach model

estimation of the remanence

(based on data from material vendor)

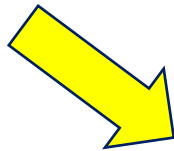


# Challenge 3: Transient phenomena

## lamination

- hysteresis + remanence
- eddy currents

$$\nabla \times \left( \nu \nabla \times \overset{r}{A} \right) + \sigma \frac{\partial \overset{r}{A}}{\partial t} = \overset{r}{J}_S$$

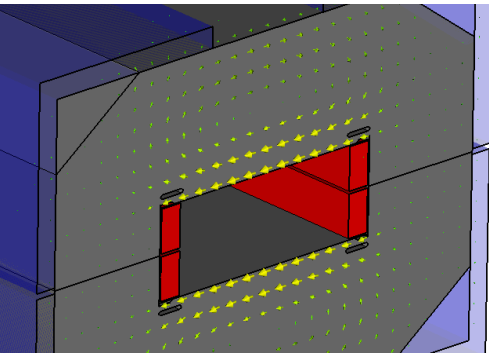


eddy current term

+ (simple) homogenisation  $\sigma_{xy} = \gamma_{st} \sigma_{Fe}$

$$\sigma_z = 0$$

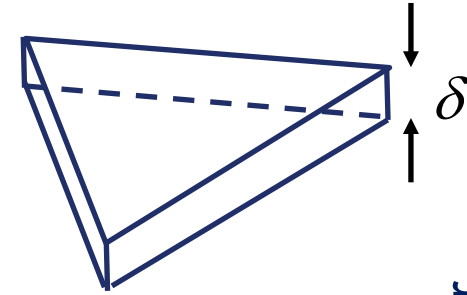
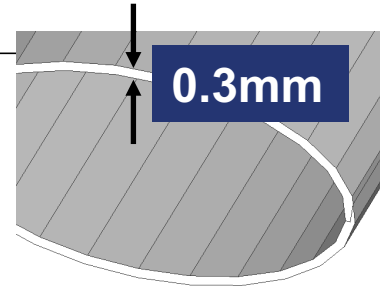
or + multi-scale model (hand-shaking)



# Challenge 3: Transient phenomena

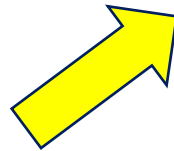
## lamination

- hysteresis + remanence
- eddy currents



## beam tube

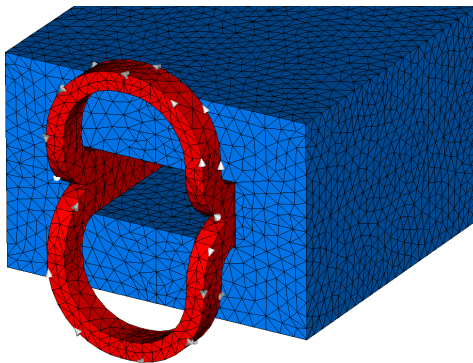
- eddy currents



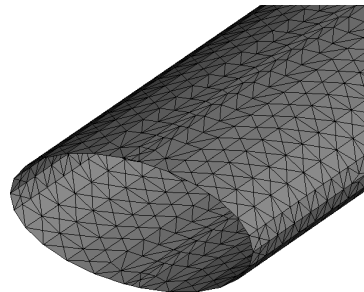
shell elements

additional matrix contributions  $\mathbf{K}_\delta$  and  $\mathbf{M}_\delta$   
assembling into system matrix by  $\mathbf{Q}$

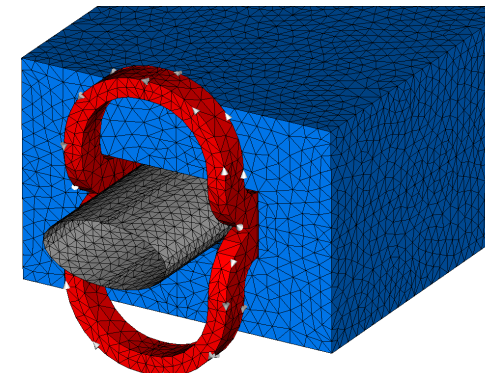
$$\mathbf{K}_V + \sigma \mathbf{M}_\sigma + \mathbf{Q}^T (\mathbf{K}_\delta + \alpha \mathbf{M}_\delta) \mathbf{Q} = \mathbf{K}_{\text{full}} + \alpha \mathbf{M}_{\text{full}}$$



+



=



# Challenge 3: Transient phenomena

## lamination

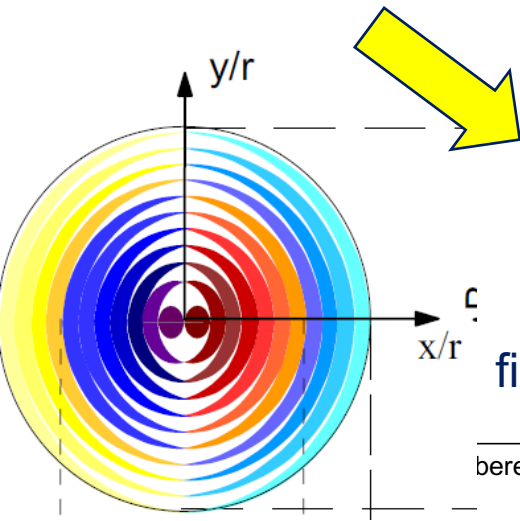
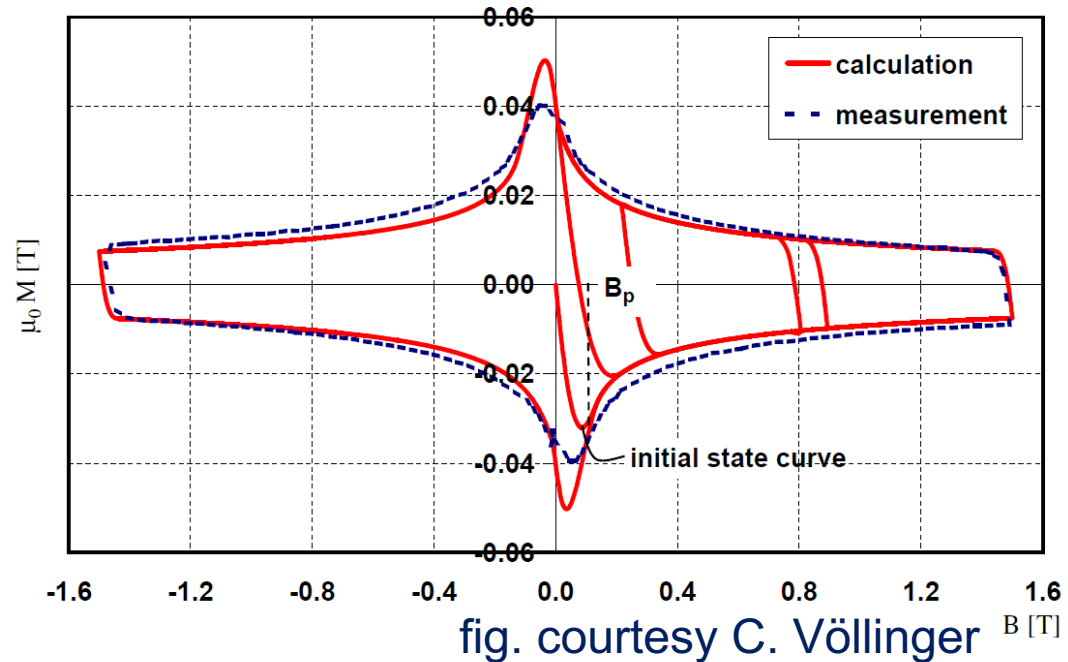
- hysteresis + remanence
- eddy currents

## beam tube

- eddy currents

## superconductor

- persistent currents



Bean model → magnetisation (Christine Völlinger)  
implemented in ROXIE

fig. courtesy C. Völlinger

# Challenge 3: Transient phenomena

## lamination

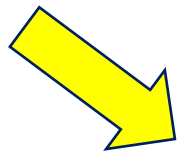
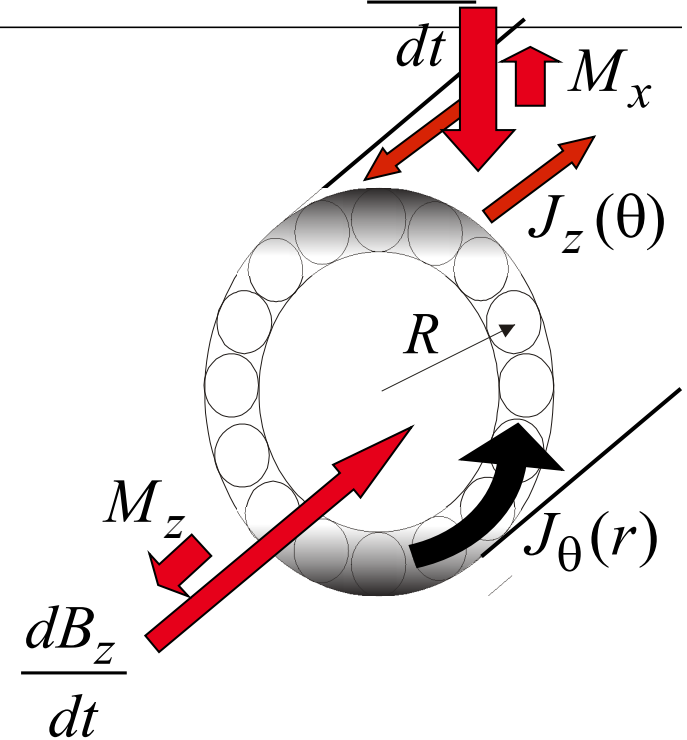
- hysteresis + remanence
- eddy currents

## beam tube

- eddy currents

## superconductor

- persistent currents
- coupling currents
- cable eddy currents



$$\nabla \times (\nu \nabla \times \overset{r}{A}) + \sigma \frac{\partial A}{\partial t} + \nabla \times \left( \nu_0 \bar{\tau}_{cb} \nabla \times \frac{\partial A}{\partial t} \right) = \overset{r}{J}_s$$

additional magnetisation

# Challenge 4: High accuracy requirements

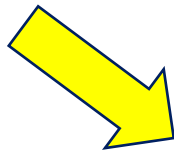


## losses

- dimensioning of the cooling system
- hot spots
- quench

## aperture field

- multipoles during injection, ramping and extraction
- + influence of eddy currents

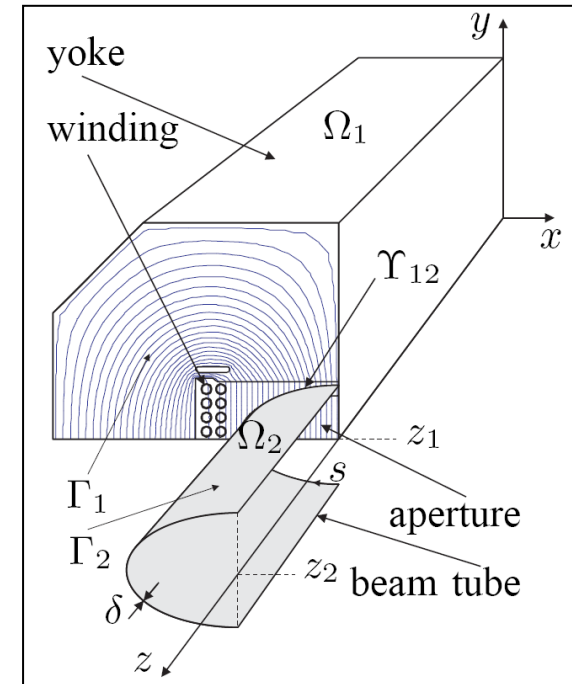
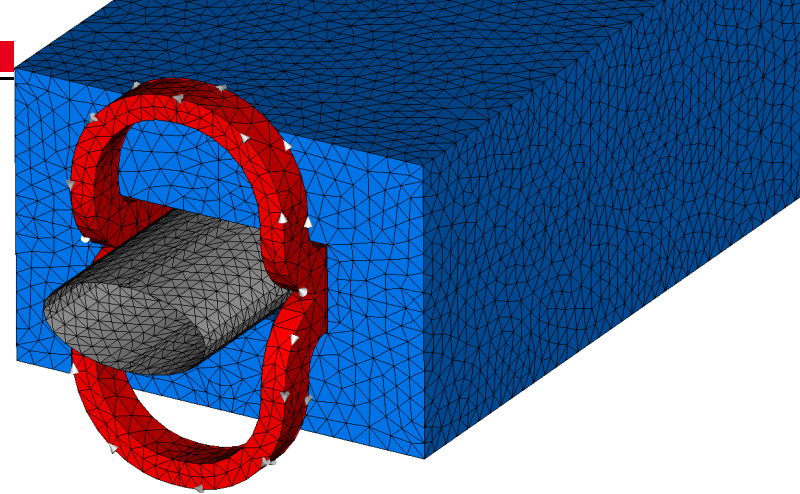


huge models

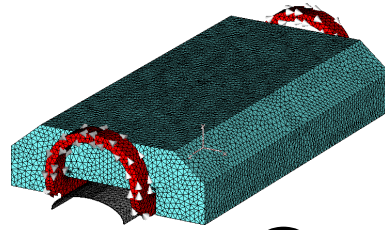
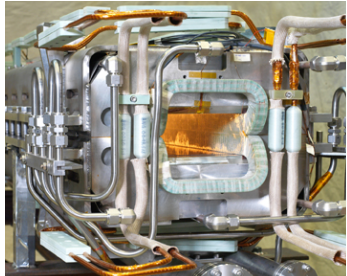
parallelisation, multi-core computers

# Overview

- magnet simulation (standard 3D FE solver)
- challenges
  - geometrical details
  - materials
  - transient effects
  - high accuracy
- magnet simulation (dedicated 3D FE solver)
- hysteresis modelling
- conclusions

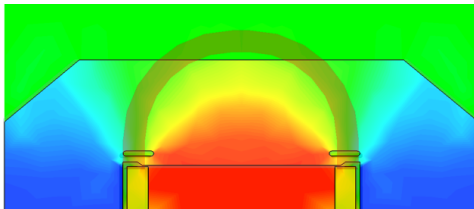


# Dedicated Simulation Tool

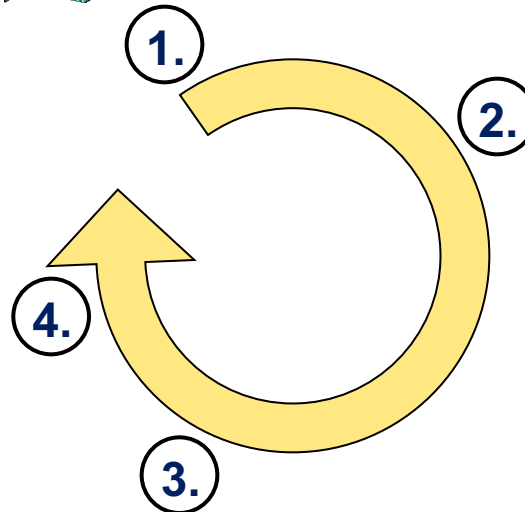


CST Studio Suite®

- CAD modelling
- meshing
- visualisation



+ Stephan Koch, Jens Trommler



Matlab

- postprocessing
- visualisation

FEMSTER,  
LLNL

TRILINOS,  
Sandia Labs

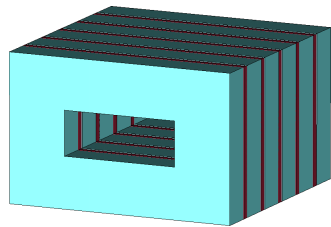
own software

- FE assembly  
(higher order FEs)
- transient solver
- nonlinear materials
- system solver

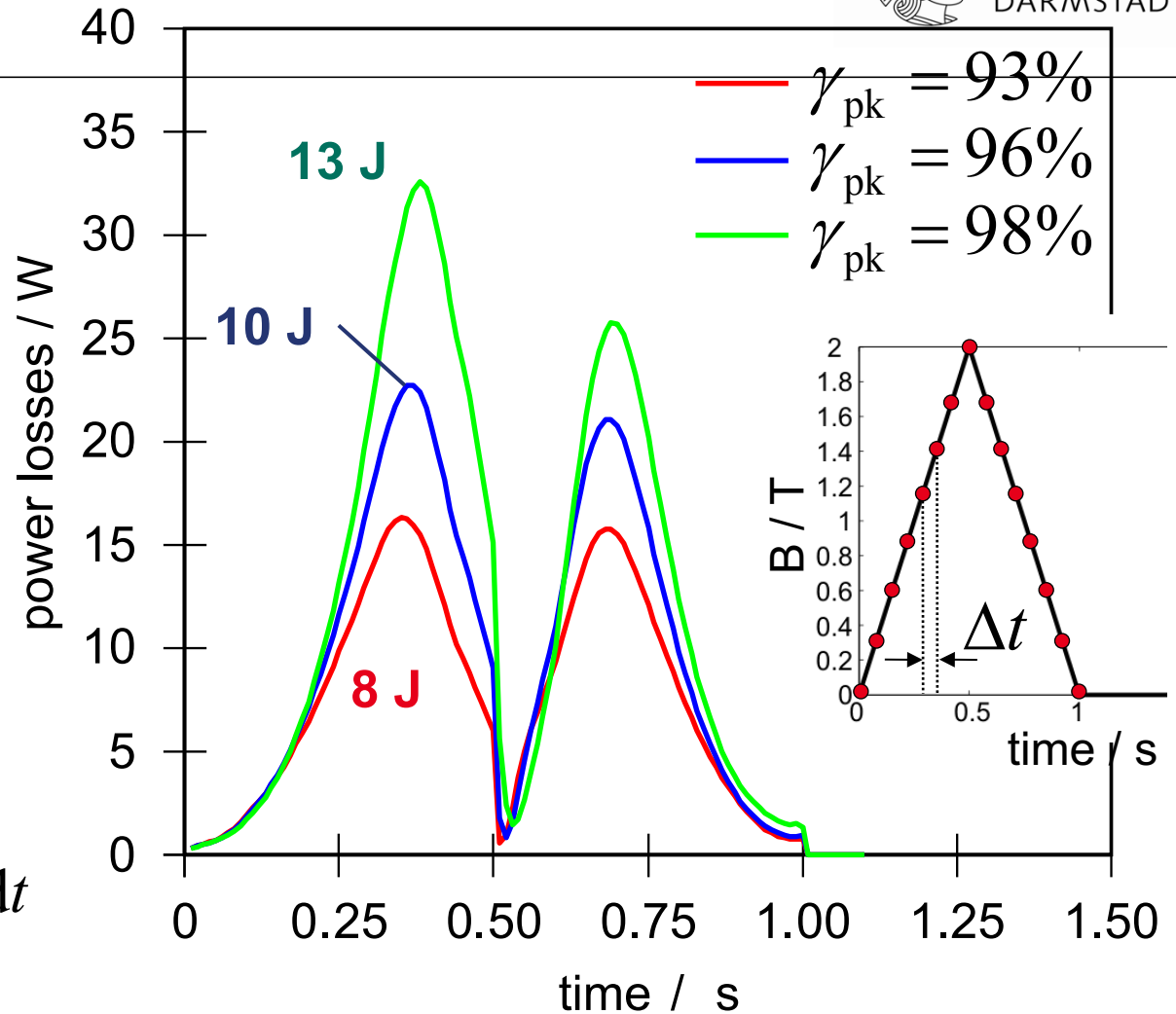
**parallelisation**

# Results: Eddy-Current Losses

eddy-current  
losses over one  
cycle  
for different  
stacking factors  $\gamma_{pk}$



loss energy:  $W = \int_0^T P dt$



+ Stephan Koch, Jens Trommler



# Results: Loss Energy

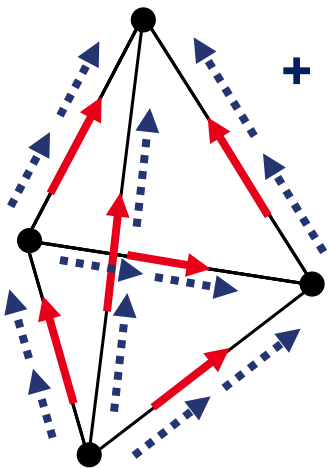
## discretization:

- increase number of elements
- increase order of approximation

$$\vec{A} \approx \vec{A}_{\text{FE}} = \sum_j a_j \vec{w}_j^{\text{tv}}$$

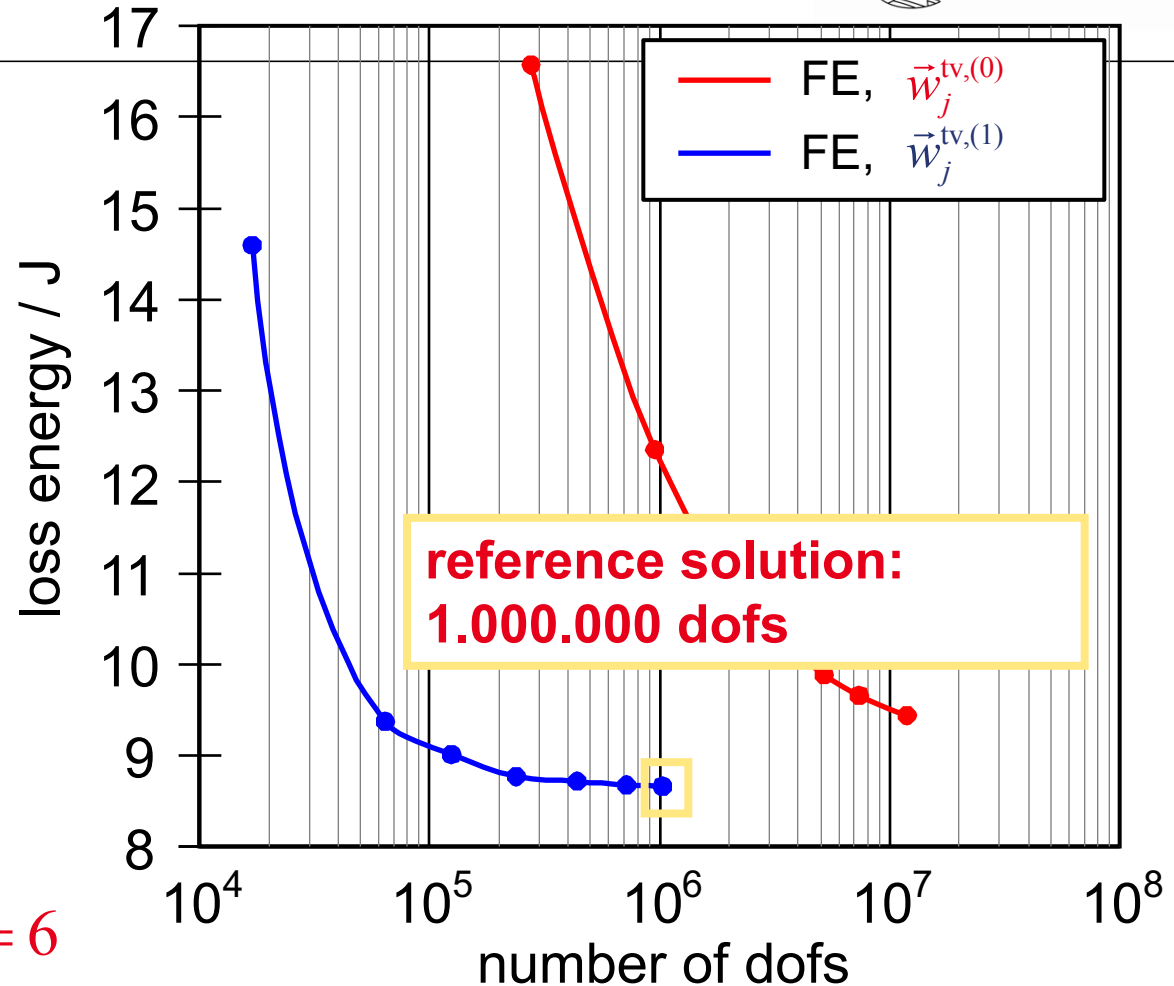
degrees of freedom:

+ 2 per face



$$\vec{w}_j^{\text{tv},(0)} \quad n_{\text{dof}} = 6$$

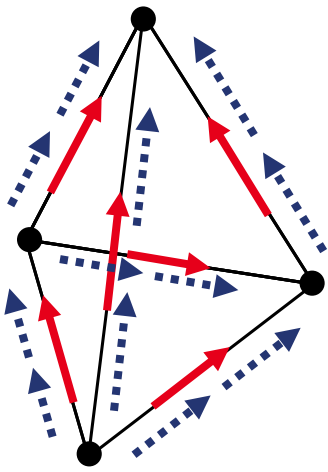
$$\vec{w}_j^{\text{tv},(1)} \quad n_{\text{dof}} = 20 \quad + \text{S. Koch, J. Trommler}$$



# Convergence: Loss Energy

- relative error with respect to reference solution

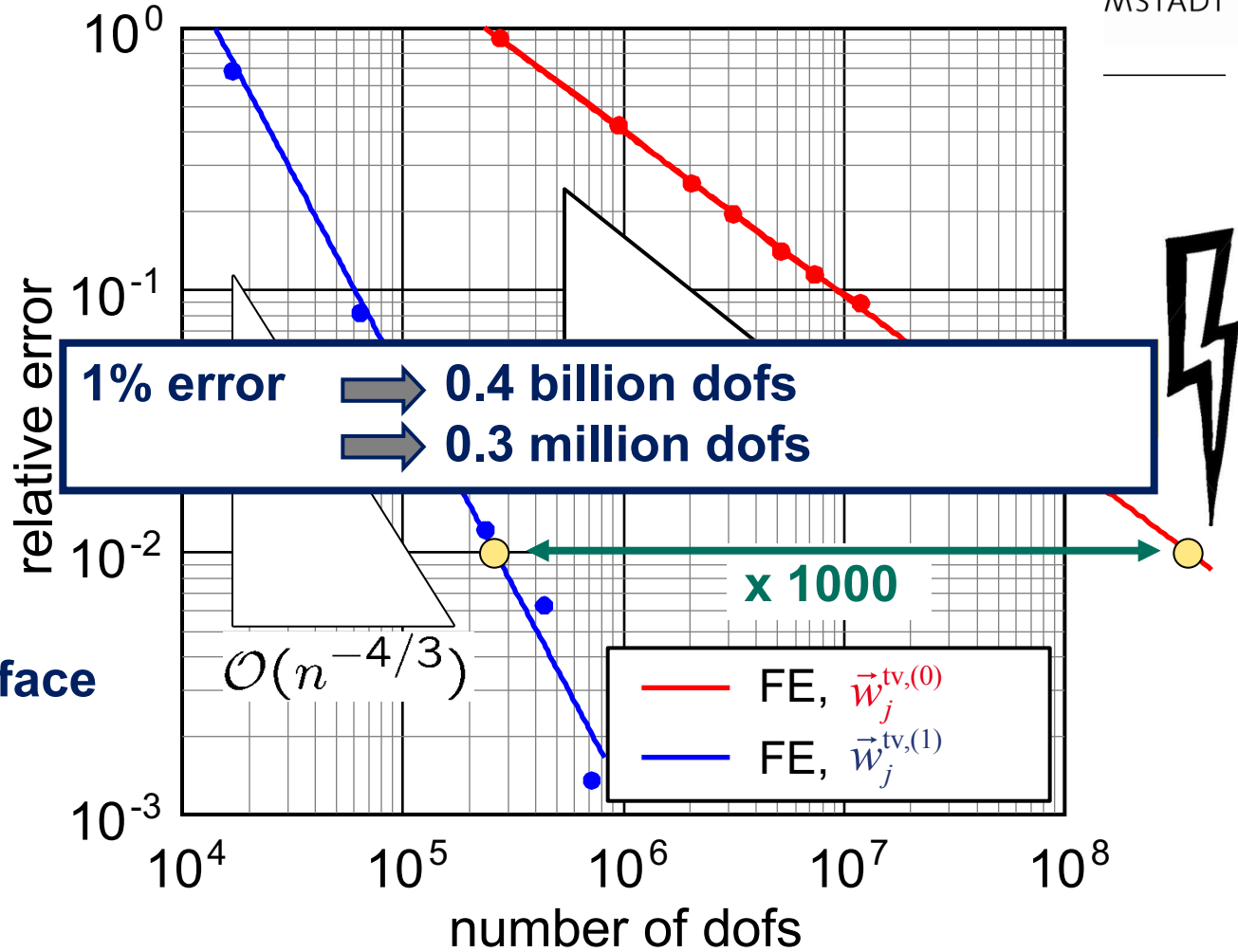
degrees of freedom:



+ 2 per face

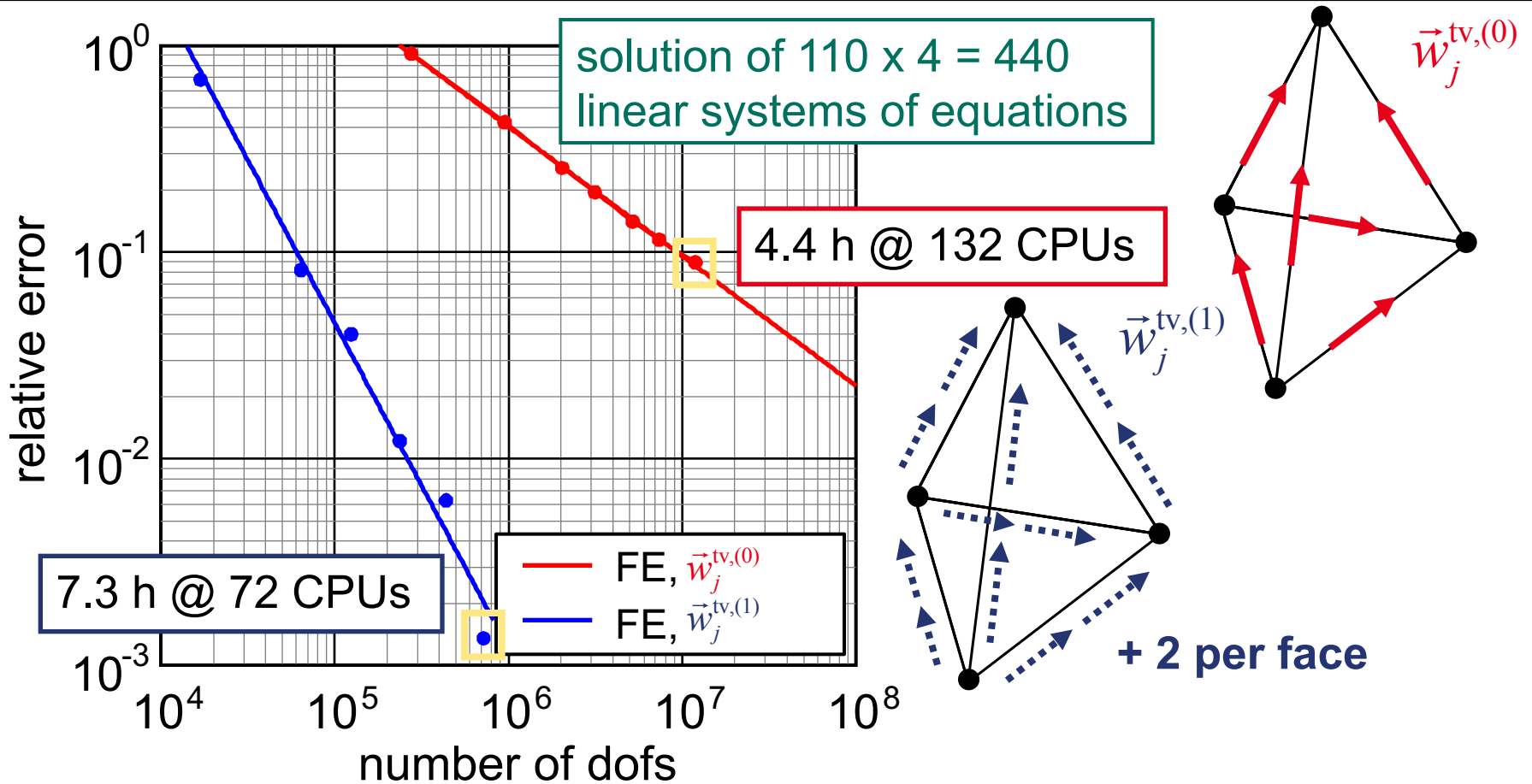
$$\vec{w}_j^{tv,(0)}$$

$$\vec{w}_j^{tv,(1)}$$



+ S. Koch, J. Trommler

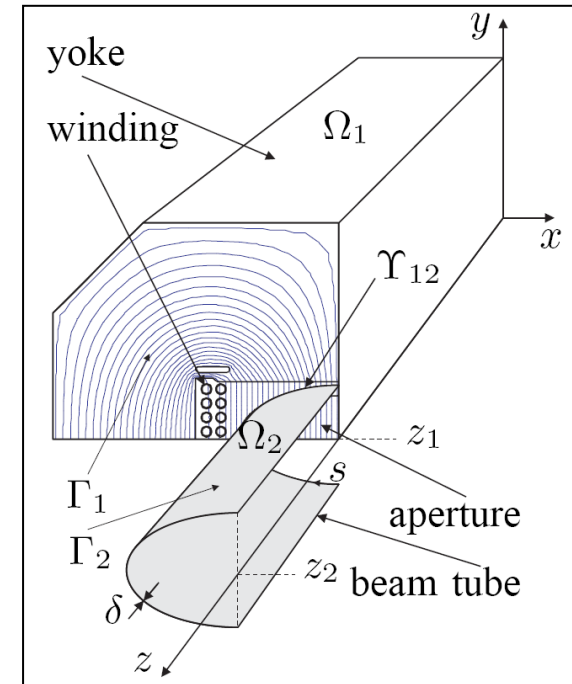
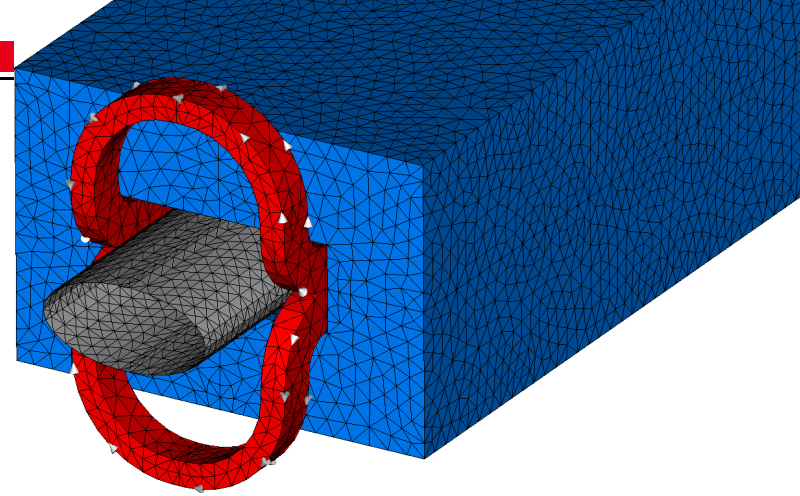
# Comparison: Shape Functions



+ S. Koch, J. Trommler

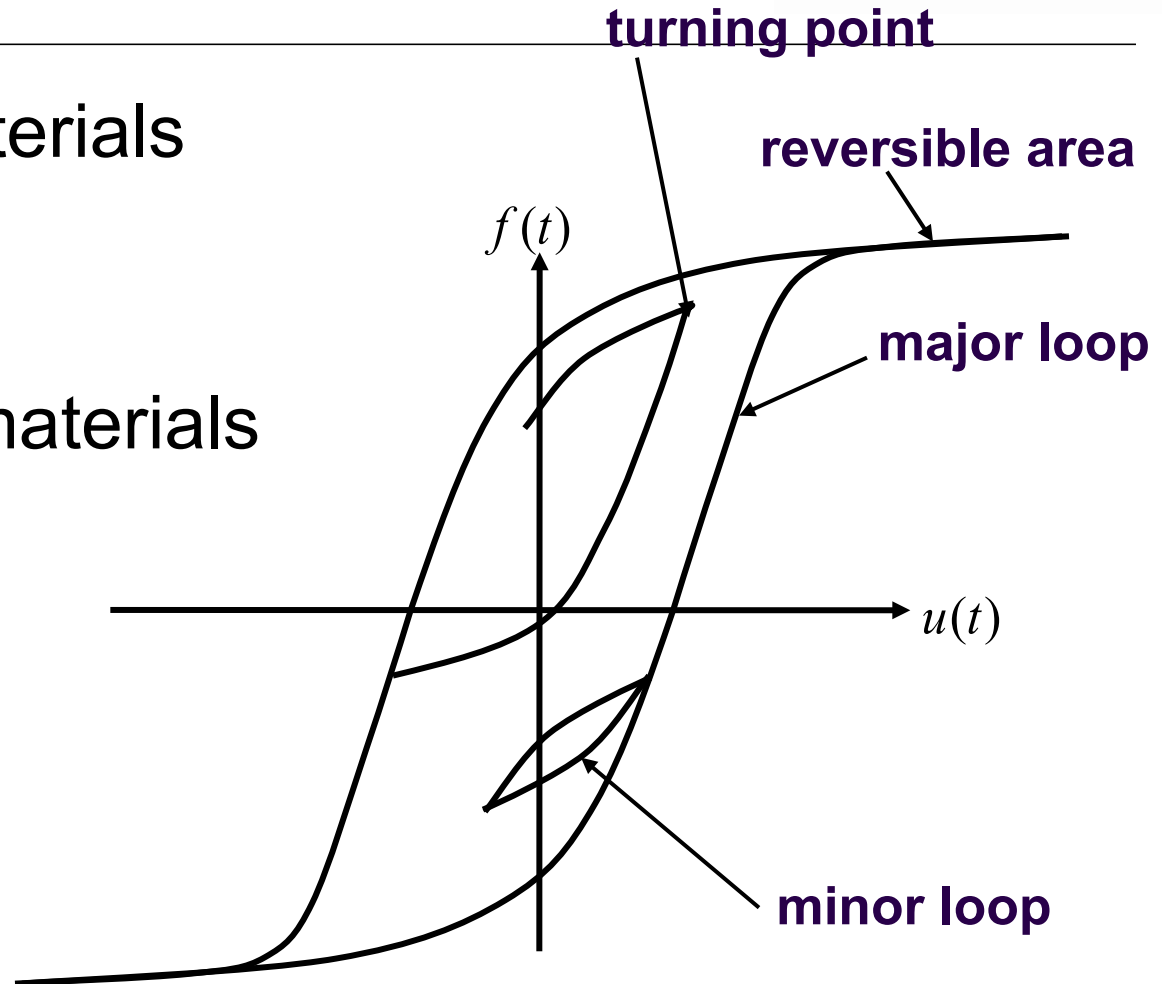
# Overview

- magnet simulation (standard 3D FE solver)
- challenges
  - geometrical details
  - materials
  - transient effects
  - high accuracy
- magnet simulation (dedicated 3D FE solver)
- **hysteresis modelling**
- conclusions



# Hysteresis

- Ferromagnetic materials
  - remanence
  - hysteresis losses
- Superconductive materials
- Friction



# Hysteresis and Field Modelling

- transient field simulation + hysteresis model
- transient field simulation + simple hysteresis model  
e.g. hysteresis losses: complex permeability

$$\left. \begin{array}{l} B(t) = \hat{B} \cos(\omega t) \\ H(t) = \hat{H} \cos(\omega t - \varphi) \end{array} \right\} \Rightarrow \underline{\mu} = \frac{\hat{B}}{\hat{H}} e^{j\varphi}$$

- post-processing step + simple hysteresis model  
e.g. hysteresis losses: Steinmetz formula

$$p_{\text{hyst}} = \sigma_{\text{hyst}} k_{\text{hyst}} \frac{f}{50 \text{ Hz}} \left( \frac{|B|}{1 \text{ T}} \right)^2$$

- post-processing step + simple remanence model  
e.g. remanence: look-up table

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# Hysteresis Models

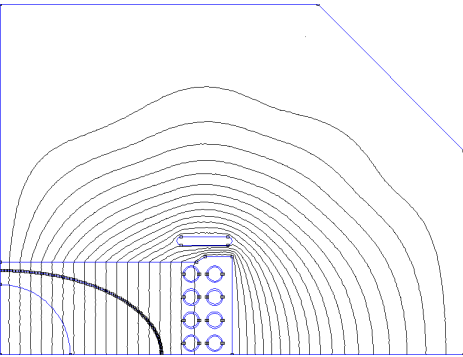
- Preisach model
- Jiles-Atherton model
- Stone-Wolfarth model
- ...

## Preisach model

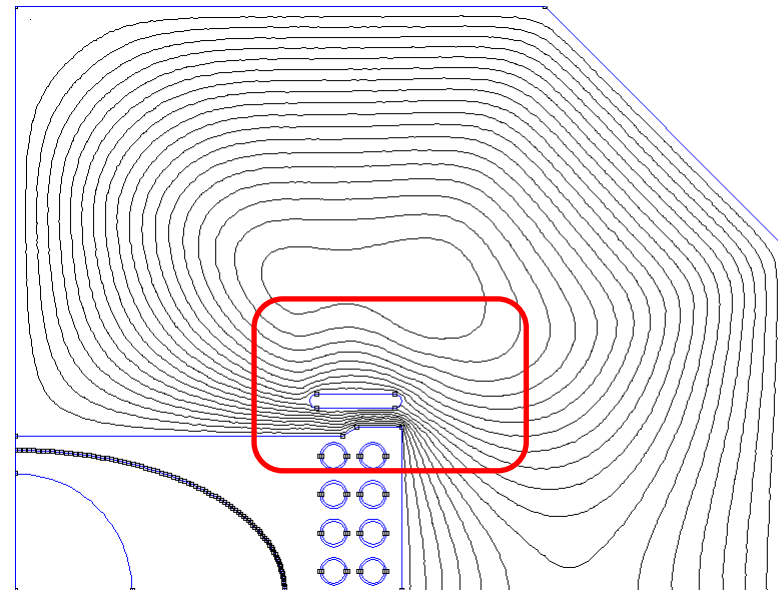
I.D. Mayergoyz, „Mathematical Models of Hysteresis“,  
Springer-Verlag, New York, 1991, pp. 1-44.

# SIS100: Remanence at Injection

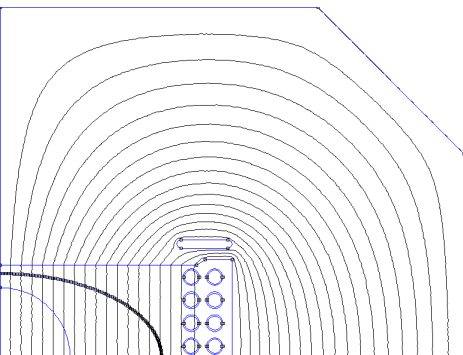
injection field  
(with remanence)



remanent field



injection field  
(without remanence)

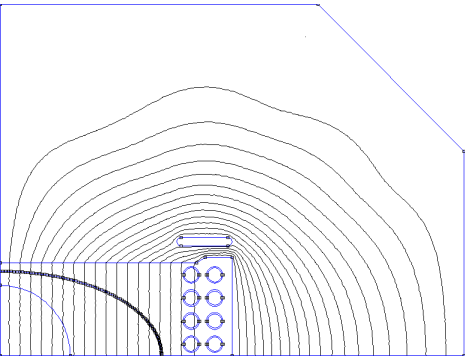


region with heavy saturation  
acts as „source“ of  
magnetisation

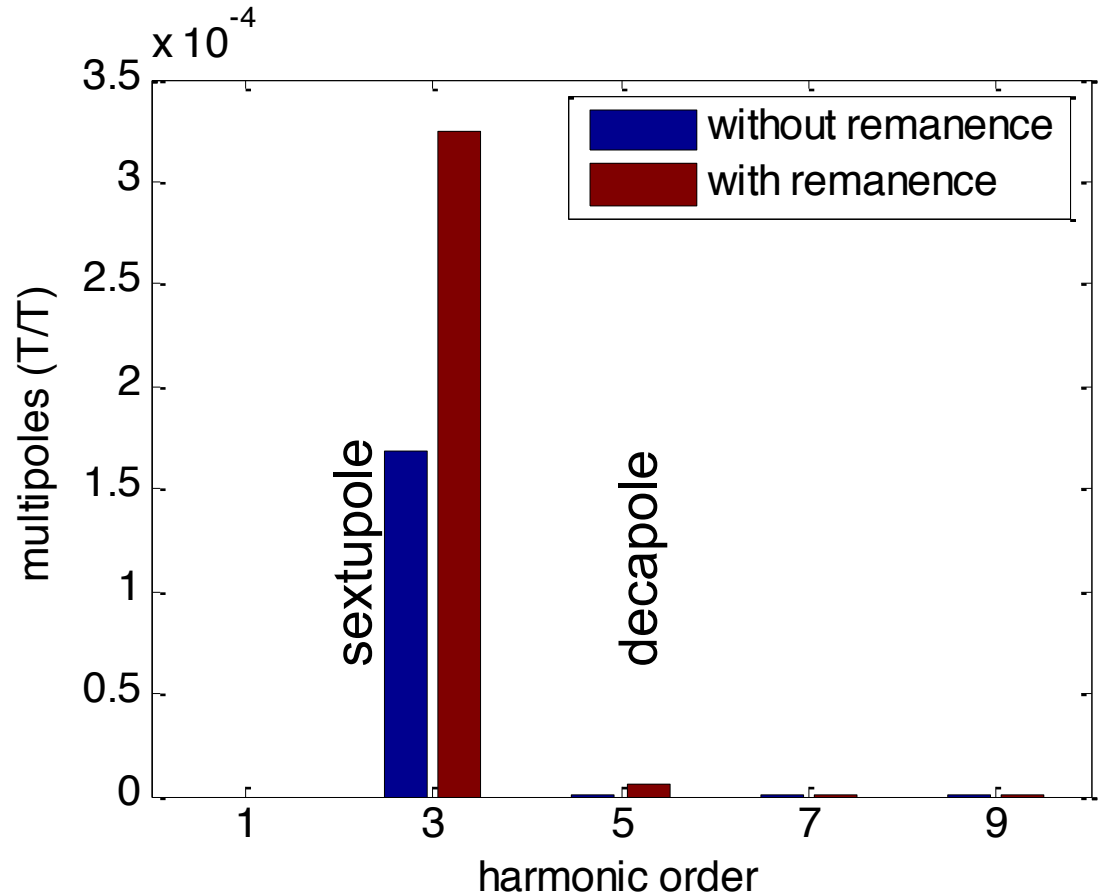
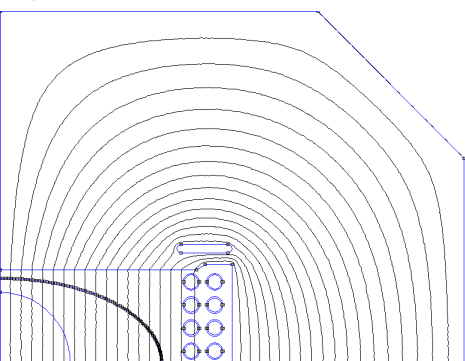


# SIS100: Remanence at Injection

injection field  
(with remanence)



injection field  
(without remanence)



# Conclusions

- nonlinear 3D transient magnetic simulation feasible with of-the-shell software
- challenges remain and are problem specific
  - geometrical details
  - materials
  - transient effects
  - high accuracy
- hysteresis modelling (Preisach)

**necessity of accurate material models and measurement data**

