

DISPERSION MEASUREMENT AND CORRECTION IN THE VUV-FEL (FLASH)

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- Introduction

- Dispersion Measurement
 - Procedure
 - Measurements

- Dispersion Correction
 - Procedure
 - Response matrix measurements
 - Dispersion correction simulations
 - 1st dispersion correction measurements

- Summary and next steps

$$\eta_x = \frac{\Delta x}{\Delta p / p}$$

$$\sigma = \sqrt{\varepsilon \cdot \beta(s) + \eta(s)^2 \cdot \left(\frac{\Delta p}{p}\right)^2}$$

Goal: dispersion in the undulator of **1 cm**

VUV-FEL (FLASH)



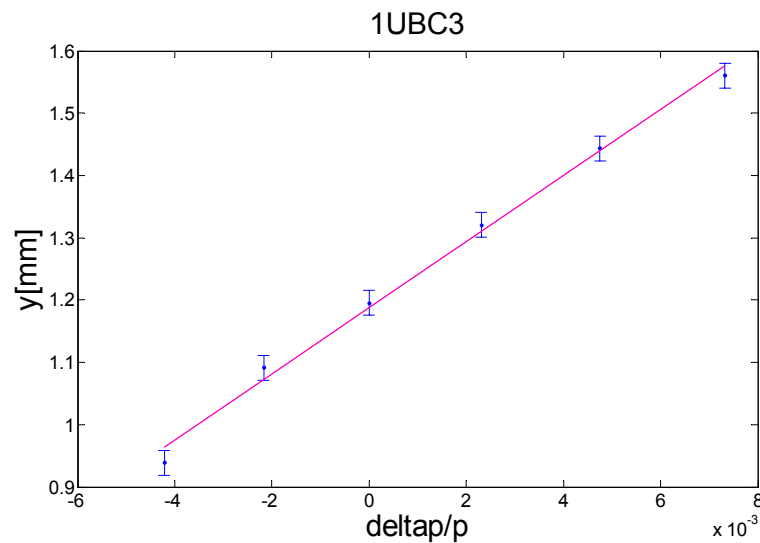
Generation mechanisms

Source	Error (in all the lattice)	Error (only in the dog-leg)	Dispersion (after the dog-leg)
<i>Quad misalign</i>	17 μm	50 μm	~ 1cm
<i>Dipole field error</i>	0.25 %	5 %	
<i>Quad field error</i>	0.75 %	0.75 %	

- Quad misalignment seems to be the most important dispersion source
- Dog-leg is a critical zone for dispersion generation

- Measure the orbit for different energies
 1. Change RF gradient of the module
 2. Apply orbit correction to restore launch conditions after the module
 3. Read BPM positions downstream last correction BPM

- Derive the dispersion

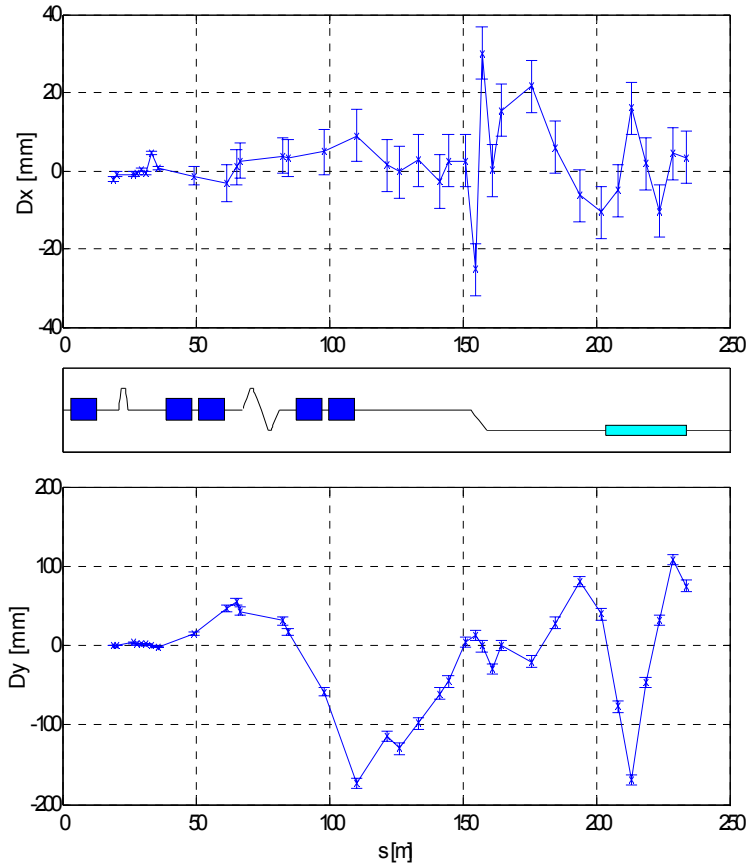


$$x = x_0 + D_0 \frac{\Delta p}{p} + D_1 \left(\frac{\Delta p}{p} \right)^2 + \dots$$

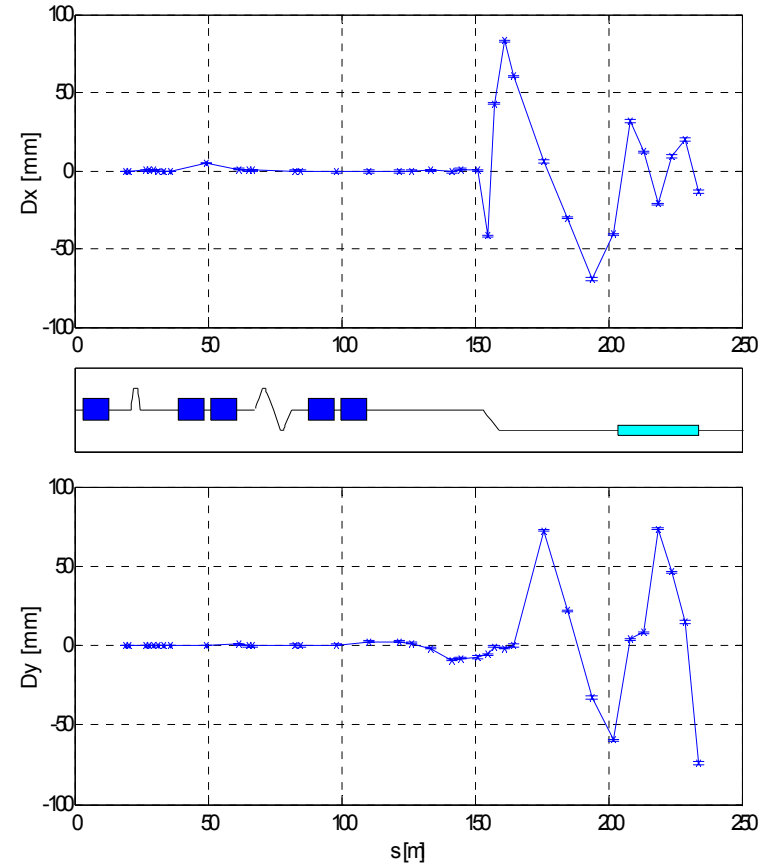
↑
Dispersion

Dispersion Measurements (Nov. 05)

From DBC2



From ACC4-5



Dispersion Correction Algorithm

It corrects both **orbit** and **dispersion**, using the orbit and dispersion response matrices

➤ Orbit response term $O_{i,j} = \frac{\Delta x_i}{\Delta \theta_j}$

 ➤ Dispersion response term $D_{i,j} = \frac{\Delta D_i}{\Delta \theta_j}$

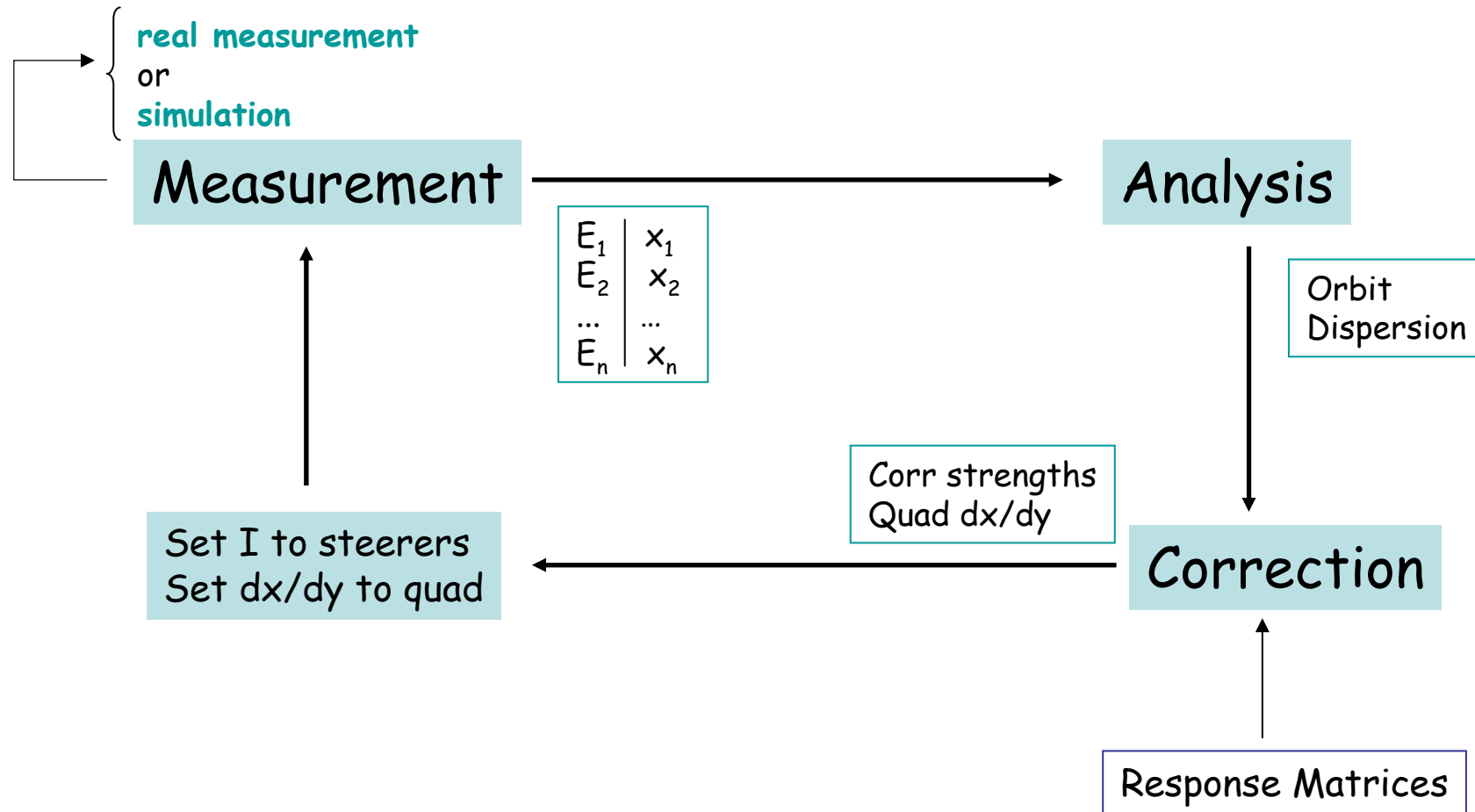
$\frac{\Delta x_i}{\Delta \theta_j}$ -----> change of the orbit / dispersion at the BPM i
 $\Delta \theta_j$ -----> change of the kick angle of the steerer j

$$\begin{pmatrix} \underline{O} \cdot (1-w) \\ \underline{D} \cdot w \end{pmatrix} \cdot \underline{\Delta \theta} = \begin{pmatrix} \underline{x} \cdot (1-w) \\ \underline{d} \cdot w \end{pmatrix}$$

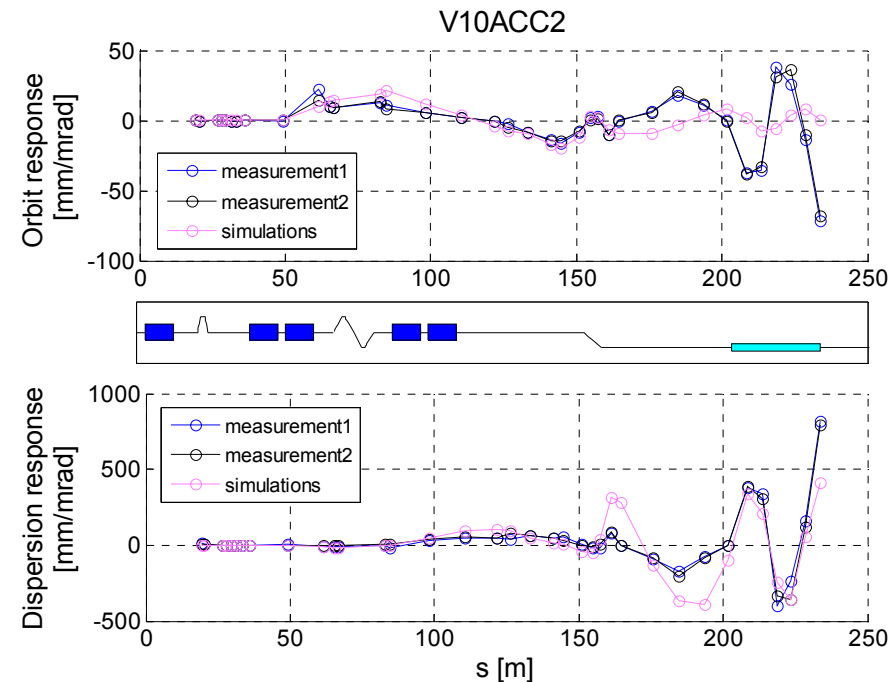
Response matrices \underline{O} and \underline{D} lead to $\underline{O} \cdot (1-w)$ and $\underline{D} \cdot w$ respectively.
 The vector $\underline{\Delta \theta}$ is multiplied by the combined matrix.
 The result is split into $\underline{x} \cdot (1-w)$ (Orbit) and $\underline{d} \cdot w$ (Dispersion).
 The parameter w is the Weighting factor.
 The final result is used to determine the Corrector strengths.

$$\sum \left[\begin{pmatrix} \underline{x}_{meas} \\ \underline{d}_{meas} \end{pmatrix} - \begin{pmatrix} \underline{x} \\ \underline{d} \end{pmatrix} \right]^2 = \min \Rightarrow \underline{\Delta \theta}$$

Dispersion Correction Procedure

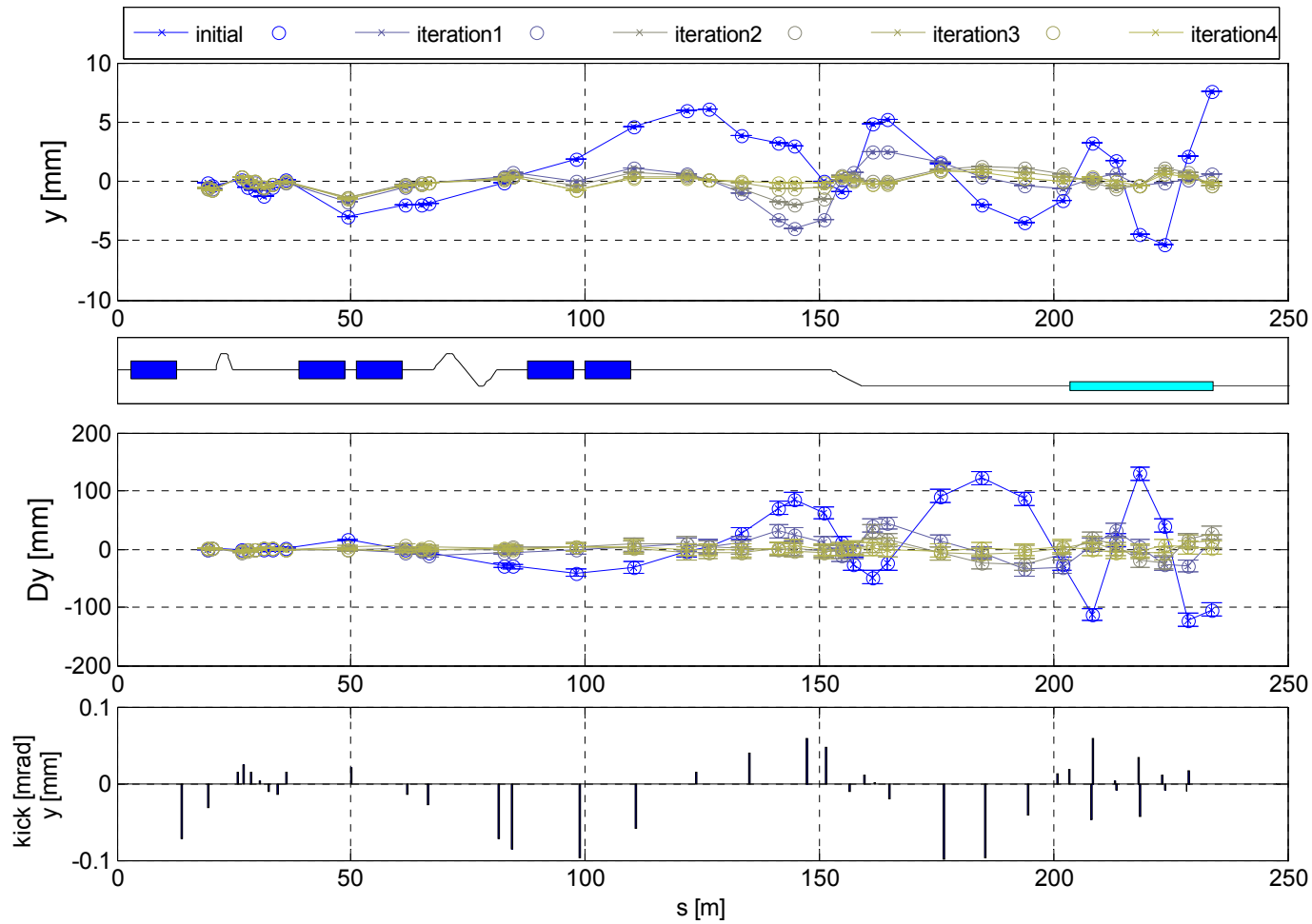


- For dispersion correction, optics of the machine have to be close to the design optics or one has to use the measured response matrices
- Comparing the measured and simulated orbit and dispersion response will let to fix possible optic errors
- We have measured the complete response for the machine and the data is presently being analyzed



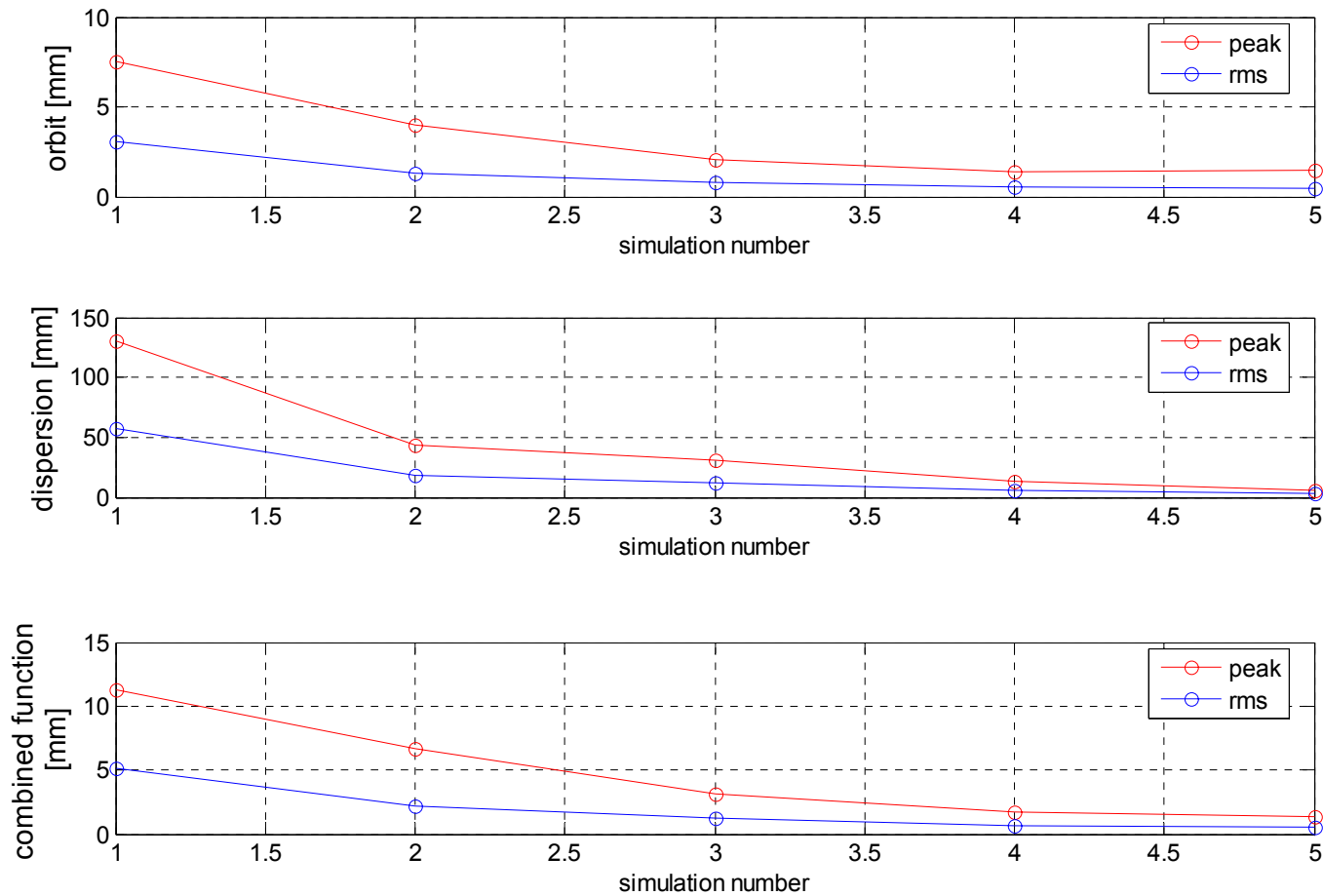
Dispersion correction simulations

vertical plane, $w = 0.1$; quad malign = 200 μm , dipole field error = 1%;
quad field error = 1%; bpm noise = 20 μm ; bpm off-set = 100 μm ; all bpm's ; all steerers

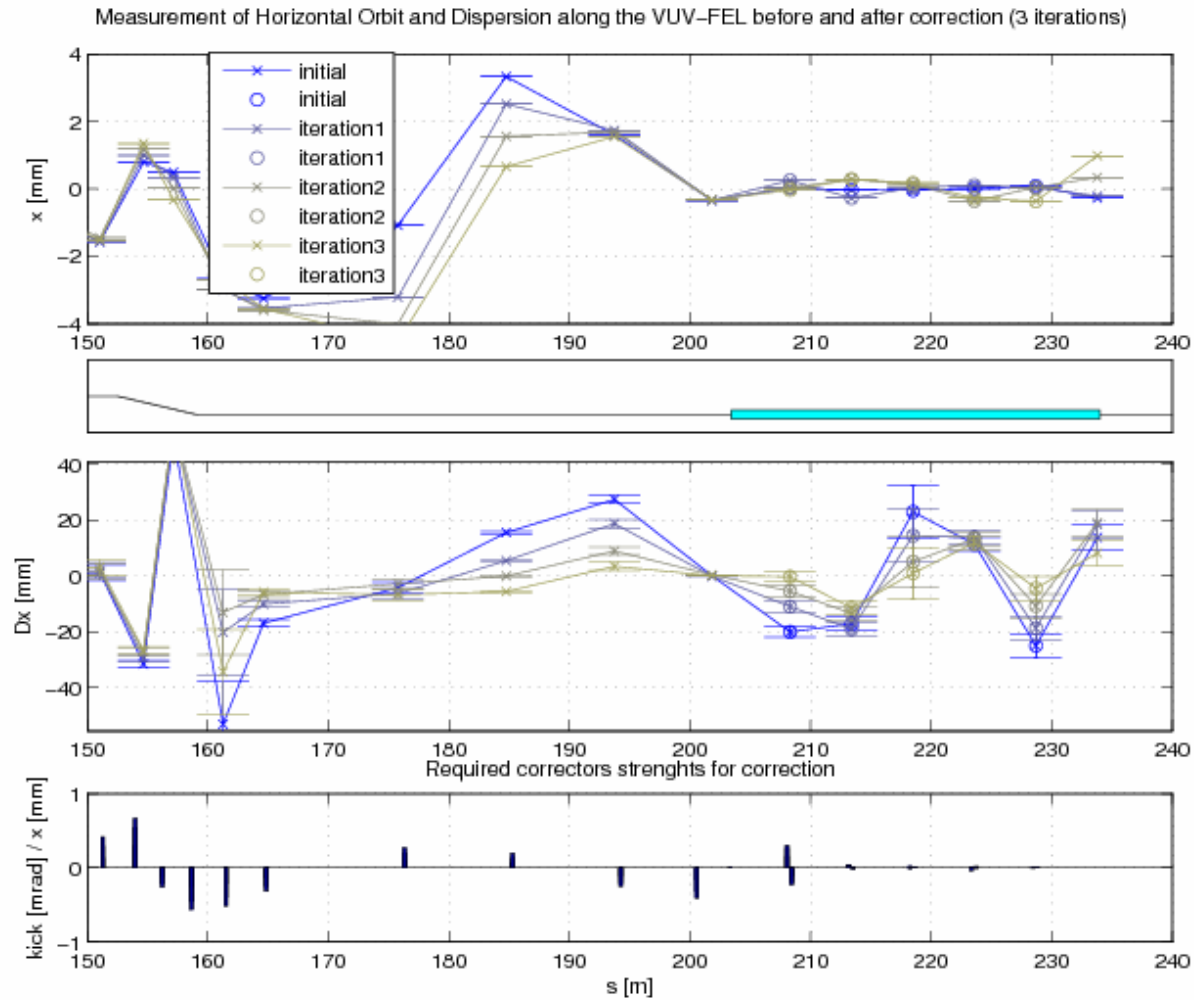


Dispersion correction simulations

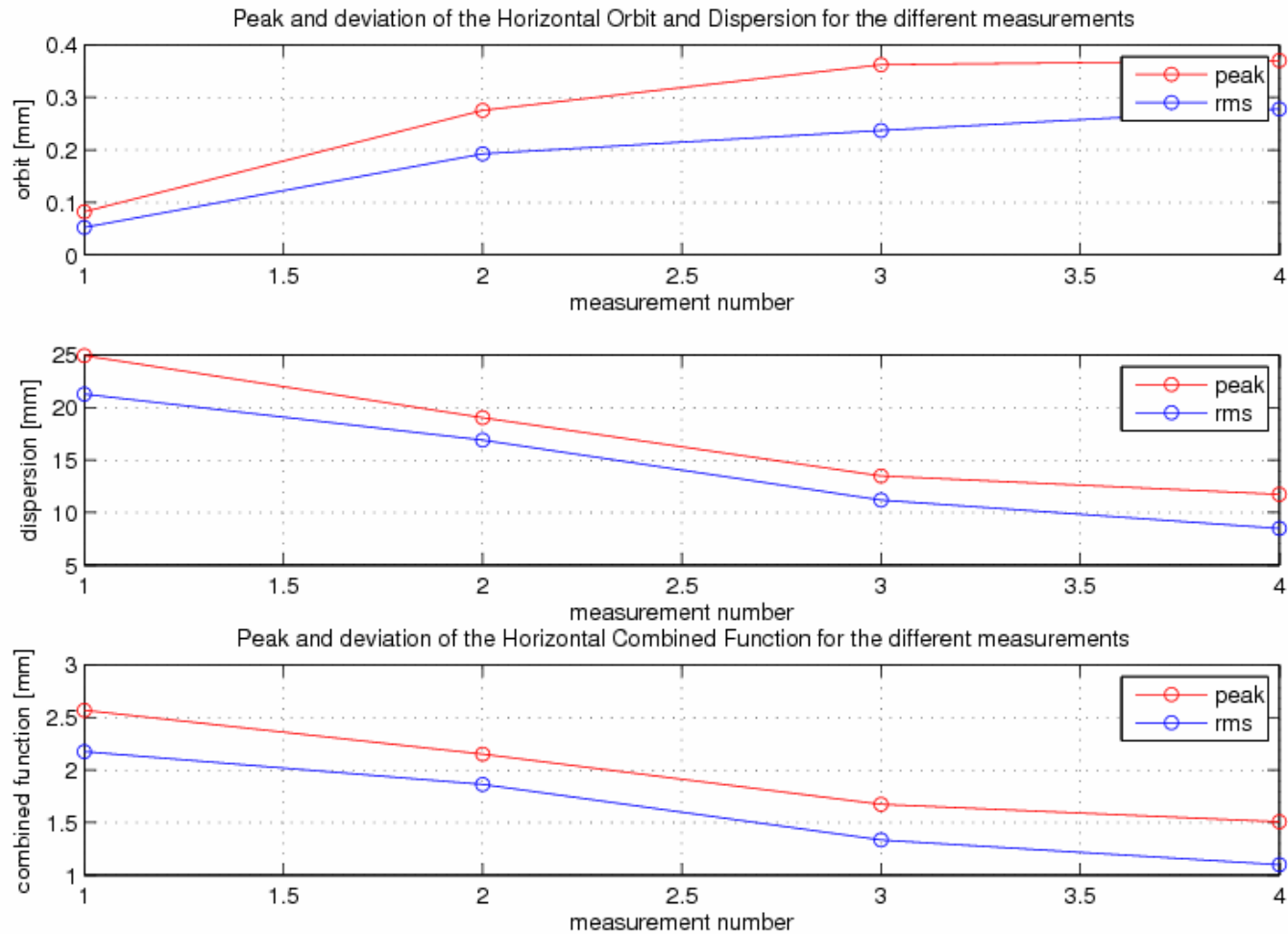
Peak and deviation of the orbit and dispersion for the different simulations



1st Dispersion correction measurements (April 06)



1st Dispersion correction measurements (April 06)



Summary and next steps

Summary:

- A tool for measuring and correcting orbit and dispersion has been developed
- Several dispersion measurements done on November 05
- Complete response matrix measurement has been done
- Simulations of dispersion correction have been performed
- Dispersion correction in the undulator in the horizontal plane done

Next steps:

- Analyze data from orbit and dispersion response measurements
- Make dispersion correction program more user friendly
- Correct dispersion in vertical plane