

# XFEL - INJ 1/2 Dumps

## Remarks / Requirements

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**A. Dump Layout**

**B. Beam Size Requirements**

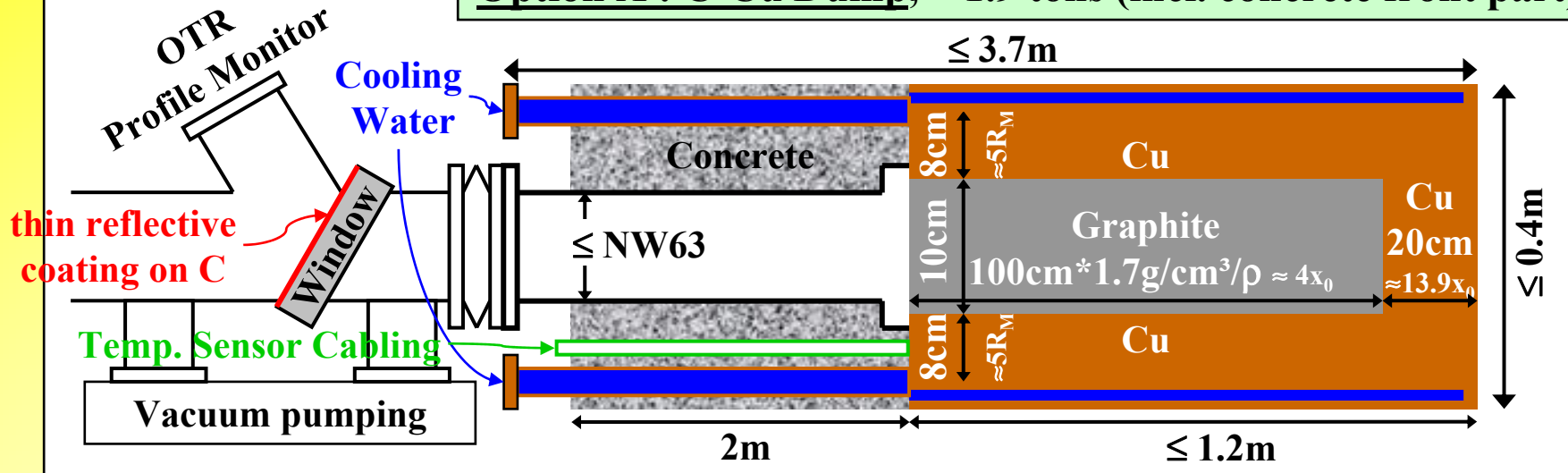
**C. Fast Sweeper Space Requirements**

**D. Summary / Questions**

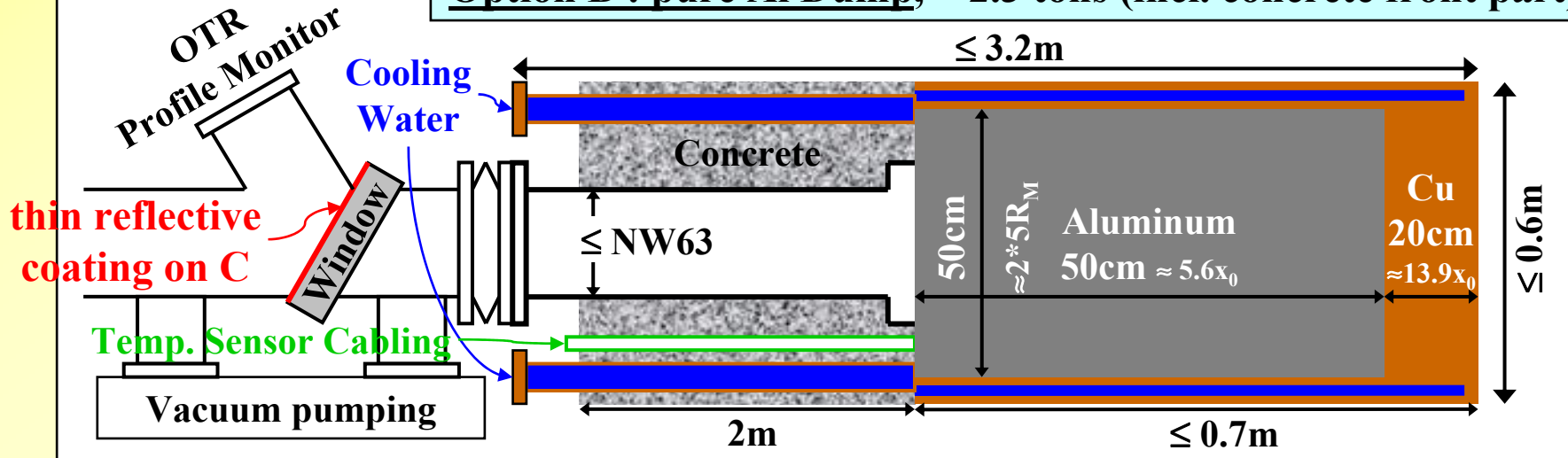
# Dump Layout: 2 possible options

Required capability:  $E_0 \leq 300 \text{ MeV}$ ,  $N_t \leq 2.5 \cdot 10^{13} \text{ e}^- = 4 \mu\text{C}$ ,  $I_{\text{ave}} \leq 40 \mu\text{A}$ ,  $P_{\text{ave}} \leq 12 \text{ kW}$

## Option A : C-Cu Dump, $\approx 1.9 \text{ tons}$ (incl. concrete front part)

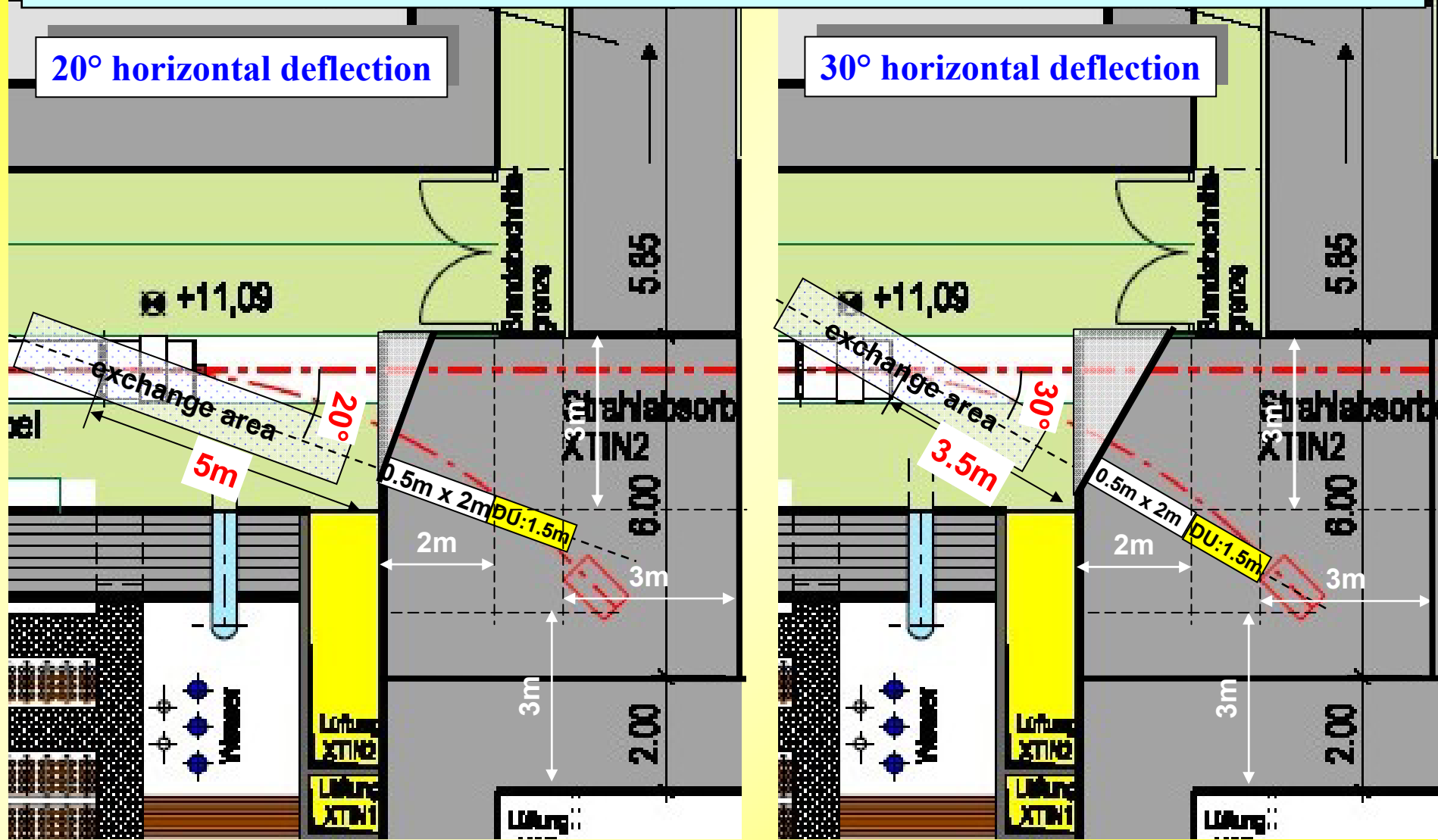


## Option B : pure Al Dump, $\approx 2.3 \text{ tons}$ (incl. concrete front part)



# Dump Layout: integration in XSE

Top view sketch of horizontal bend into dump arm, showing available beam line length vs bend angle and required space in case of exchange

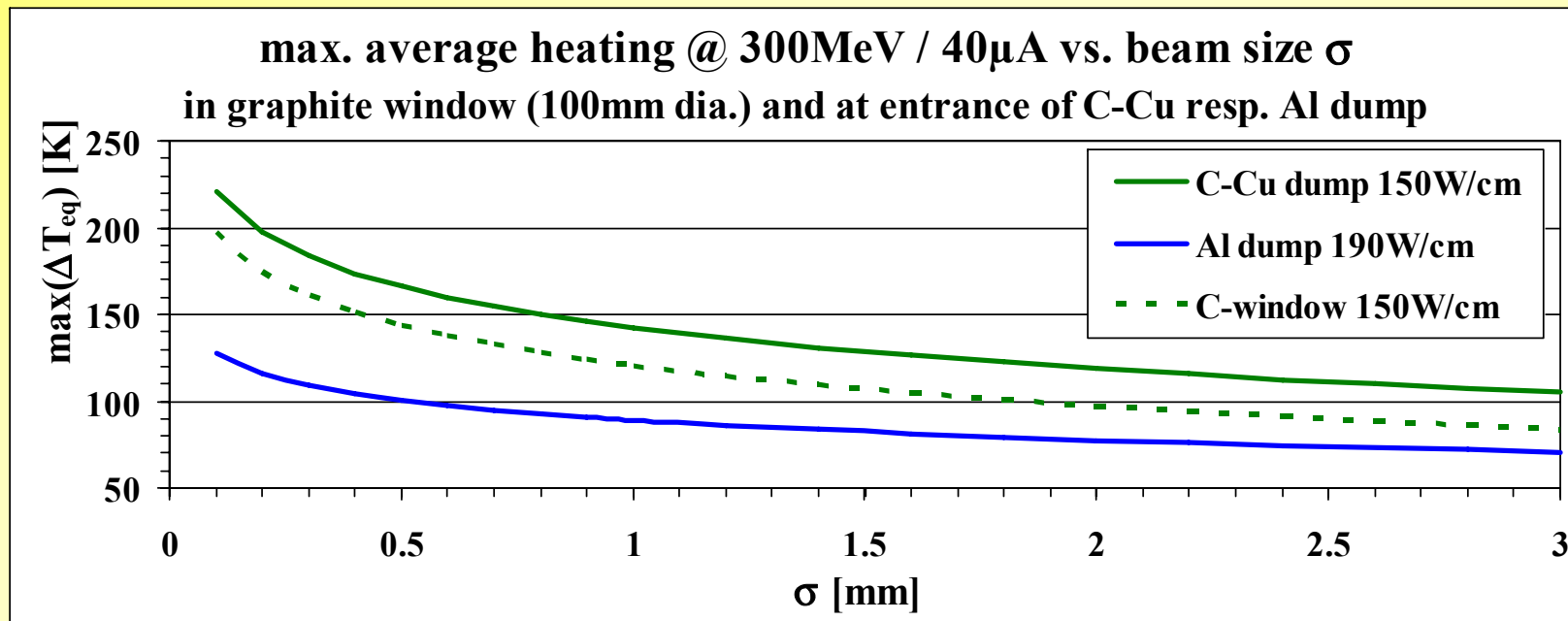


# Beam Size Requirements: properties of materials

Material Properties	normal C	Al
density, $\rho$ [g/cm <sup>3</sup> ]	1.7 – 1.9	2.7
specific heat capacity, $c$ [J/g/K]	~ 1 @ 150°C	0.9
thermal conductivity, $\lambda$ [W/cm/K]	0.7	2.0
Temperature Limits		
$T_{\text{melt}}$	$\geq 3000^\circ\text{C}$	660°C
cyclic heating, $\max(\Delta T_{\text{inst}})$	~ 150-200 K derived from tensile strength	~ 50 K plasticity limit
$\max(T_{\text{operation}})$	~ 500-600°C, oxidation limit	~ 250°C
average heating $T_{\text{heat sink}} \sim 60^\circ\text{C} \Rightarrow \max(\Delta T_{\text{eq}})$	~ 350 K	~ 150 K

## Beam Size Requirements: average heating

	C-Cu dump		Al dump	
max(dP/dz) [W/cm] @ 300MeV / 40μA	@ entrance	@ shower max.	@ entrance	@ shower max.
	150	190	210	380



- **considering the beam as a dc heat source, i.e if no pulsed stress is involved**  
⇒  $\sigma \approx 0.1\text{mm}$  to tolerate average heating by 300MeV / 40μA beam
- **also o.k. for average heating @ shower max. (dP/dz higher, but r-profile wider)**

# Beam Size Requirements: instantaneous heating

- our cases here ( $\sigma \leq 2\text{mm}$ ,  $E_0 \leq 500\text{MeV}$  on C and Al) allow analytical estimation:

$$\max(\Delta T_{\text{inst}}) = \frac{1}{c} \cdot \max\left(\frac{dE}{dm}\right) = \frac{1}{c} \cdot \frac{1}{\rho} \frac{dE}{dz} \cdot \frac{N_t}{2\pi \cdot \sigma^2} = 1.9 \frac{\text{MeV} \cdot \text{cm}^2}{\text{g}} \cdot \frac{1}{c} \cdot \frac{N_t}{2\pi \cdot \sigma^2}$$

$$\Rightarrow \max(\Delta T_{\text{inst}}) = 48\text{K} \cdot 1 / c [\text{J/g/K}] \cdot N_t [10^{13}] \cdot 1 / \sigma^2 [\text{mm}^2]$$

- reduction factor by fast circular sweep with radius  $R_f$ :  $\approx 2.5 \cdot R_f / \sigma$ , for  $R_f \gg \sigma$

$$^*) \Lambda = \sqrt{\frac{\lambda \cdot T_t}{\rho \cdot c}} \Big|_{T_t=1\text{ms}} = \begin{cases} 200\mu\text{m in C} \\ 280\mu\text{m in Al} \end{cases}$$

	300MeV on C $\max(\Delta T_{\text{inst}}) \leq 150\text{K} \Leftrightarrow \leq 150\text{J/g}$			300MeV on Al $\max(\Delta T_{\text{inst}}) \leq 50\text{K} \Leftrightarrow \leq 45\text{J/g}$		
	$\sigma$	$R_f$	$N_t$	$\sigma$	$R_f$	$N_t$
	<b>0.89mm</b>	<b>0</b>	<b><math>2.5 \cdot 10^{13}</math></b>	<b>1.6mm</b>	<b>0</b>	<b><math>2.5 \cdot 10^{13}</math></b>
thermal diffusion is not included *)	0.1mm	0	<b><math>3.1 \cdot 10^{11}</math></b>	0.1mm	0	<b><math>9.8 \cdot 10^{10}</math></b>
		<b>3.5mm</b>	<b><math>2.5 \cdot 10^{13}</math></b>		<b>10mm</b>	<b><math>2.5 \cdot 10^{13}</math></b>
single bunch limit (since fast sweep is not intra bunch sweep)	$\approx 20\mu\text{m}$	---	$2\text{nC} \Leftrightarrow 1.25 \cdot 10^{10}$	$\approx 35\mu\text{m}$	---	$2\text{nC} \Leftrightarrow 1.25 \cdot 10^{10}$

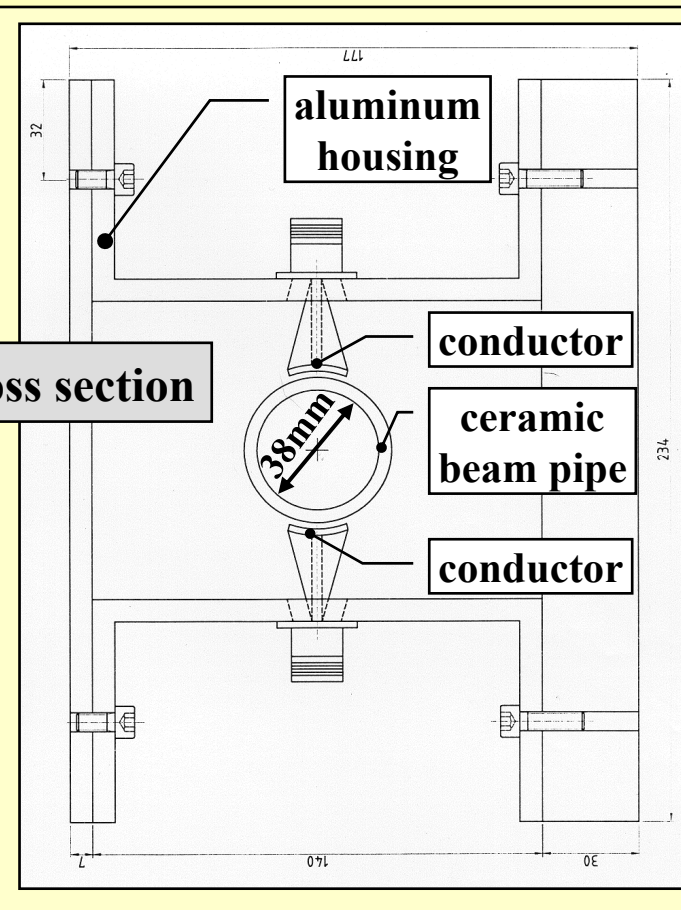
- w/o intra train sweep  $\Rightarrow \sigma \approx 1$  to  $2$  mm to tolerate inst. heating by full bunch trains
- smaller spot sizes require less charge or fast sweep radii of 4 to 10mm

## Kicker Scheme (F. Obier et al.)

- 1 winding current loop  
outside of ceramic vacuum chamber NW35
- inner surface of chamber sputtered  
with  $1\mu\text{m}$  Ti stabilized stainless steel
- $B \approx 2.15\text{mT} / 100\text{A}$
- reasonable length  $\approx 1\text{m}$
- both deflection planes can be put on same chamber
- operation as resonant L-C circuit in cw-mode  
pro: easy control, no sync. with beam necessary  
cons: C's close to beam line may degrade with time  
 $\rightarrow 100\text{A @}50\text{kHz}$  possible

$\Rightarrow 1\text{m Kicker gives } \int B \cdot dl \approx 2\text{mT} \cdot \text{m}$

kicker cross section



	max. Kick	$R_f$	$\Rightarrow$ drift
300 MeV	2 mrad	5 mm – 10mm	2.5 m – 5 m

$\Rightarrow$  dump arm should provide 1m installation space +  $\geq 2.5\text{m}$  drift towards window

## Summary

- Average heating no issue, slow sweep not required
- Cyclic effects determine the beam size  
single bunch limit  $\geq 20\mu\text{m}$  to  $35\mu\text{m}$ , can not be decreased by fast sweeping  
bunch train limit  $\geq 0.9\text{mm}$  to  $1.6\text{mm}$  w/o fast sweep
- Fast sweeper requires 1m installation length and 2.5m resp. 5m drift space
- C-Cu dump can deal with smaller spot size than Al dump

## Questions

1. Should we install beam profile measurement integrated in the window ?
2. How to guarantee, that relation of beam size and charge stays within safe limits ?
3. What is maximum single bunch charge ?
4. Is there enough space available for fast sweeper + drift ?
5. Beam position variation at dump entrance ? (defines C-core & beam pipe aperture)
6. What is going to be installed in the dump arm ?