Trickle Heating

theory from SLAC-PUB-13854 Z. Huang et. al.



effect of transverse emittance \rightarrow xz-plane slice with $z_0 = 0$ $\delta_0 = 0$

$$\langle xx \rangle = R_{11}^2 \langle x_0 x_0 \rangle + 2R_{11}R_{12} \langle x_0 x' \rangle + R_{12}^2 \langle x'_0 x'_0 \rangle$$

$$\langle zz \rangle = R_{52}^2 \langle x'_0 x'_0 \rangle$$

$$\langle xz \rangle = R_{52}R_{11} \langle x_0 x' \rangle + R_{52}R_{12} \langle x'_0 x'_0 \rangle$$



slice at
$$z_0 \rightarrow$$
 distribution after LH

$$\begin{bmatrix} \langle xx \rangle & \langle xz \rangle \\ \langle xz \rangle & \langle zz \rangle \end{bmatrix} = \varepsilon_x \begin{bmatrix} \beta_{x0} R_{11}^2 - 2\alpha_0 R_{11} R_{12} + \gamma_{x0} R_{12}^2 & \cdots \\ \gamma_{x0} R_{12} R_{52} - \alpha_0 R_{11} R_{52} & \gamma_{x0} R_{52}^2 \end{bmatrix}$$
area det $[\cdots] = \varepsilon_x (R_{11} R_{52})^2$

energy modulation in $\text{LH} \rightarrow \text{tilted}$ microbunches







3D Impedance

generalization (on axis):

$$E_{z}(k_{0}) = \frac{-eik_{0}}{2\pi\varepsilon_{0}\gamma^{2}\lambda_{0}} \int dxdydz \times \rho(x, y, z)e^{-ik_{0}z}K_{0}\left(\frac{k_{0}r}{\gamma}\right)$$

$$\downarrow$$

$$E_{z}(k_{0}) = \frac{-eik_{0}}{2\pi\varepsilon_{0}\gamma^{2}\lambda_{0}} \int dxdx'dydy'dzd\delta \times f(x, x', y, y', z, z')e^{-ik_{0}z}K_{0}\left(\frac{k_{0}r}{\gamma}\right)$$

integration for (nominal) Gaussian transverse phase space:

$$E_{z}(k_{0}) \approx \frac{iI_{0}Z_{0}}{2\pi k_{0}\sigma_{r}^{2}} J_{1}(k_{0}R_{56}\delta_{L}) \exp\left(-\frac{1}{2}(k_{0}R_{56}\sigma_{\delta 0})^{2}\right) \exp\left(-\frac{\varepsilon}{2\beta}(k_{0}R_{52}R_{11})^{2}\right) \frac{1}{1+\gamma^{2}R^{2}}$$

for $k_0 \sigma_r / \gamma >> 1$ with $\varepsilon, \alpha, \beta$ Twiss parameters $R = -R_{52} \left(R_{21} + \frac{\alpha}{\beta} R_{11} \right)$



Trickle Heating

induced energy modulation:

$$\begin{split} \delta_{\text{LSC}} &= \frac{1}{\gamma m_0 c^2} \int E_z(k_0) dz \\ \delta_{\text{LSC}} &= \frac{2i}{k_0 \gamma} \frac{L_{\text{eff}}}{\varepsilon \overline{\beta}} \frac{I_0}{I_A} J_1(k_0 R_{56} \delta_L) \exp\left(-\frac{1}{2} (k_0 R_{56} \sigma_{\delta 0})^2\right) \\ & \text{ with } L_{\text{eff}} = \int dz \times \frac{\varepsilon \overline{\beta}}{\sigma_r^2} \exp\left(-\frac{\varepsilon}{2\beta} (k_0 R_{52} R_{11})^2\right) \frac{1}{1+\gamma^2 R^2} \\ & \overline{\beta} \quad \text{typical beta function} \\ & \sigma_r^2 \approx \sigma_x \sigma_y \quad \text{ (round beam)} \end{split}$$

rms energy spread with trickle heating:

$$\begin{split} \sigma_{\delta} &\approx \sqrt{\sigma_{\delta 0}^{2} + 0.5(\delta_{L}(\delta_{0}))^{2} + 2|\delta_{LSC}(\delta_{L}(\delta_{0}))|} \\ & \text{with } \delta_{L}(\delta_{0}) = \sqrt{s_{f}} \delta_{0} \\ & s_{f} \approx 1 \quad \text{shape factor (electron/photon beam size)} \\ & \sigma_{\delta 0} \quad \text{uncorr. spread before heater} \end{split}$$



Trickle Heating II

for: $\sigma_{\delta 0} \ll \sigma_{\delta}$

$$\sigma_{\delta} \approx \sqrt{A \delta_0^2 + (BJ_1(C \delta_0))^2} \quad \text{with} \quad A = 0.5s_f$$

$$B = \frac{2\sqrt{2}}{k_0 \gamma} \frac{L_{\text{eff}}}{\varepsilon \beta} \frac{I_0}{I_A} \exp\left(-\frac{1}{2} (k_0 R_{56} \sigma_{\delta 0})^2\right)$$
example LCLS:
$$C = \sqrt{s_f} k_0 R_{56}$$

$$R_{56} = 3.9 \text{ mm} \quad \text{(last two magnets of chicane)}$$

$$\lambda_0 = 758 \text{ nm}$$

$$I_0 = 37 \text{ A}$$

$$\begin{split} \gamma \varepsilon &= 0.4 \,\mu\text{m} \\ m_0 \gamma c^2 &= 135 \,\text{MeV} \qquad \rightarrow \qquad A \approx 0.331 \\ L_{\text{eff}} &= 0.81 \,\text{m} \text{ for } \overline{\beta} = 5 \,\text{m} \qquad B \approx 2.73 \cdot 10^{-4} \quad \text{(to spectrometer)} \\ s_f &= 0.662 \qquad C \approx 2.63 \cdot 10^4 \end{split}$$



Example LCLS





Comparison XFEL, LCLS



XFEL 1nC, λ = 1047 nm, 800nm, 523nm





Simplified

$$\left(\frac{\sigma_{\delta}}{\delta_0}\right)^2 = A + \left(B\frac{J_1(C\delta_0)}{\delta_0}\right)^2 \approx A \left(1 + \left(\frac{BC}{2\sqrt{A}}\right)^2\right) \quad \text{for} \quad C\delta_0 < \approx 1$$

enhancement factor:

$$F = \frac{BC}{2\sqrt{A}} = \frac{2}{\gamma} \frac{L_{\text{eff}} R_{56}}{\varepsilon \overline{\beta}} \frac{I_0}{I_A} \exp\left(-\frac{1}{2} (k_0 R_{56} \sigma_{\delta 0})^2\right)$$

weak

... see summary



Effective length
$$L_{\text{eff}} = \int dz \times \exp\left(-\frac{\varepsilon}{2\beta} (k_0 R_{52} R_{11})^2\right) \left[\frac{\varepsilon \overline{\beta}}{\sigma_r^2}\right] \frac{1}{1+\gamma^2 R^2}$$

 $W_1 \qquad W_2 \qquad W_3 \qquad W = W_1 W_2 W_3$







$$R_{11}(z) = 0 \qquad \rightarrow \cos \psi + \alpha_0 \sin \psi = 0$$

$$R(z) = 0 \qquad \rightarrow \langle xz \rangle = \varepsilon R_{52}(\gamma_0 R_{12} - \alpha_0 R_{11}) \qquad \rightarrow \sin \psi - \alpha_0 \cos \psi = 0$$

therefore: 90 deg phase shift between both conditions



$$L_{\rm eff} = \int dz \times \exp\left(-\frac{\varepsilon}{2\beta} \left(k_0 R_{52} R_{11}\right)^2\right) \frac{\varepsilon \overline{\beta}}{\sigma_r^2} \frac{1}{1 + \gamma^2 R^2}$$



$$\int dz \times \exp\left(-\frac{\varepsilon}{2\beta} \left(k_0 R_{52} R_{11}\right)^2\right) \approx \frac{\sqrt{2\pi \beta/\varepsilon}}{k_0 R_{52} R_{11}'}$$
$$L_{\text{eff}} \approx \sqrt{2\pi} \frac{\overline{\beta}}{k_0 R_{52}} \sum_{\nu} \left(\frac{1}{R_{11}'} \frac{\sigma_x}{\sigma_r^2} \frac{1}{1+\gamma^2 R^2}\right)_{z=z_{\nu}^{(R11=0)}}$$







Summary





