# Angular analysis of the decay $B \to K^* l^+ l^-$ at the Belle experiment

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This report describes my project within the Desy Summer Student Programme 2014 in the Belle group. I implemented a fit to angular distributions in the decay  $B \to K^*(\to K\pi)l^+l^-$  to extract parameters that might be sensitive to physics beyond the Standard Model. I performed a Monte Carlo toy study in order to test four different realisations of the fit. Althought the Belle experiment has rather limited statistics, it is sufficient to make a significant measurement of these parameters.

## I. INTRODUCTION

The  $b \rightarrow sl^+l^-$  process in  $B \rightarrow K^*(\rightarrow$  $K\pi)l^+l^-$ , where l stands for e or  $\mu$ , is a flavor changing neutral current which is forbidden in the Standard Model (SM) at tree level and can occur at lowest order in electroweak penguin and box diagrams (see Figure 1). The angular distribution of the  $K\pi l^+l^-$  final state is sensitive to physics beyond the SM that could contribute to these diagrams. The decay has been studied extensively by Belle [2], BaBar [2], CDF [3], and LHCb [4] and the results on various observables have been found to be in agreement with the SM. Last year LHCb published a measurement of observables in the angular distribution of this decay and found a  $3.7 \sigma$  descrepancy to the SM prediction for  $P'_5$  (definition see section III Eq. 1 and 2) in one dimuon invariant mass squared bin of  $4.30 \,\text{GeV}^2/c^4$  -  $8.68 \,\text{GeV}^2/c^4$  [5]. To clarify the nature of this discrepancy, a second independent measurement is needed. In this report the first stage of a study is presented to evaluate the sensitivity of the Belle experiment to the same observables as measured by LHCb.

The next section is a brief description of the Belle detector. In Section III the kinematic variables and the differential decay rate together with an angle transformation is presented. The different fitting techniques and the Monte Carlo (MC) toy study is explained and its result is shown in Section IV. Conclusions and a short outlook can be found in Section V.

## II. THE BELLE DETECTOR

The Belle detector collected ~  $1000 \,\mathrm{fb}^{-1}$  of data at the asymmetric  $e^+e^-$  collider KEK-B operating at the  $\Upsilon(nS)$  resonances at KEK in Tsukuba, Japan. It is a multipurpose largesolid-angle megnetic spectrometer designed to measure time dependent CP violation in *B* meson decays. It covers a polar angle between 17° and 150° and has the typical 'onion skin' layout.



FIG. 1. Above: One possible electroweak penguin diagram for the process  $B^0 \to K^{*0} \mu^+ \mu^-$ . Below: A box diagram for the same process [1].



FIG. 2. Schematic view of the Belle detector, courtesy of Torben Ferber.

The central part of the detector is a multilayer double sided silicon strip detector surounding the beryllium beam pipe for precise vertex reconstruction. Tracking of charged particles is per-



FIG. 3. Definitions of the angles in  $B \to K^* l^+ l^-$  [1].

formed by a central drift chamber (CDC). Particle identification is provided by aerogel threshold Cherenkov counters, time-of-flight plastic scintillators and the dE/dx information from the CDC. Eletromagentic showers are reconstructed in the CsI(Tl) calorimeter inside the 1.5 T superconducting solenoid coil. The iron flux return is used to detect  $K_L$  mesons und muons (see Figure 2). A detailed description of the detector can be found elsewhere [6].

# III. THE PROBABILITY DENSITY FUNCTION (PDF)

### A. Definition of kinematic variables

The angular distribution of the decay  $B^0 \rightarrow K^{*0}(\rightarrow K^+\pi^-)l^+l^-$  where l denotes either e or  $\mu$  can be described by four kinematic variables:  $q^2$  is the squared invariant mass of the dilepton system,  $\theta_K$  is the angle between the direction of the kaon and the opposite direction of the  $B^0$  $(\overline{B}^0)$  in the  $K^{*0}$   $(\overline{K}^{*0})$  rest frame,  $\theta_l$  is the angle between the direction of the  $l^+$   $(l^-)$  and the opposite direction of the  $B^0$  ( $\overline{B}^0$ ) in the dilepton

rest frame, and the angle  $\phi$  is defined as the angle between the  $K^{*0}$  ( $\overline{K}^{*0}$ ) decay plane and the dilepton decay plane in the  $B^0$  ( $\overline{B}^0$ ) meson rest frame (see Figure 3). A more formal definition of the angles can be found in Ref. [7].

#### В. The differential decay rate

Using the definitions of Ref. [8], neglecting the lepton masses and summing over  $B^0$  and  $\overline{B}^0$  decays, the differential decay rate can be expressed as

$$\frac{1}{\mathrm{d}\Gamma/\mathrm{d}q^2} \frac{\mathrm{d}\Gamma}{\mathrm{d}q^2 \mathrm{d}\cos\theta_K \mathrm{d}\cos\theta_l \mathrm{d}\phi} = \frac{9}{32\pi} \left[ \frac{3}{4} (1 - F_L) \sin^2\theta_K + F_L \cos^2\theta_K + \frac{1}{4} (1 - F_L) \sin^2\theta_K \cos 2\theta_l - F_L \cos^2\theta_K \cos 2\theta_l + S_3 \sin^2\theta_K \sin^2\theta_l \cos 2\phi + S_4 \sin 2\theta_K \sin 2\theta_l \cos \phi + S_5 \sin 2\theta_K \sin 2\theta_l \cos \phi + S_6 \sin^2\theta_K \cos \theta_l + S_7 \sin 2\theta_K \sin 2\theta_l \sin \phi + S_8 \sin 2\theta_K \sin 2\theta_l \sin \phi + S_9 \sin^2\theta_K \sin^2\theta_l \sin 2\phi \right],$$
(1)

to new physics. The observables

$$P_{4,5,6,8}' = \frac{S_{4,5,7,8}}{\sqrt{F_L(1-F_L)}} \tag{2}$$

are regarded as largely independent of form factor uncertainties [9].

We assume that the pdf defined in Eq. 1 is also valid for charged B meson decays.

### Binning in $q^2$ and transformation of the С. angles

Due to the  $q^2$  dependence of the observables in the angular distribution the fit is performed in six  $q^2$  bins (see Table I). The gaps between  $8.68 \,\mathrm{GeV}^2/c^4$  -  $10.09 \,\mathrm{GeV}^2/c^4$  and

with  $F_L$  and  $S_i$  being  $q^2$  dependent and sensitive  $10.90 \,\mathrm{GeV}^2/c^4$  -  $14.18 \,\mathrm{GeV}^2/c^4$  are vetos for background from  $B^0$   $\rightarrow$   $K^{*0}J/\psi(\rightarrow$   $l^+l^-)$  and  $B^0 \to K^{*0} \psi(2S) (\to l^+ l^-).$ 

> The most straight forward way in order to extract the observables  $P'_4$ ,  $P'_5$ ,  $P'_6$  and  $P'_8$  would be to fit the pdf defined in Eq. 1 to the angular distribution measured in an experiment. Such a fit is expected to be very unstable if statistics is limited because of the large number of free parameters in the fit. To reduce the number of parameters per fit, the angles are transformed in one of the following manners:

$$P_4' / S_4 : \begin{cases} \phi \to -\phi & \text{for } \phi < 0\\ \phi \to \pi - \phi & \text{for } \theta_l > \pi/2 \\ \theta_l \to \pi - \theta_l & \text{for } \theta_l > \pi/2, \end{cases}$$
(3)

$$P_5' / S_5 : \begin{cases} \phi \to -\phi & \text{for } \phi < 0\\ \theta_l \to \pi - \theta_l & \text{for } \theta_l > \pi/2, \end{cases}$$
(4)

$$P_6' / S_7 : \begin{cases} \phi \to \pi - \phi & \text{for } \phi > \pi/2 \\ \phi \to -\pi - \phi & \text{for } \phi < -\pi/2 \\ \theta_l \to \pi - \theta_l & \text{for } \theta_l > \pi/2, \end{cases}$$
(5)

$$P_8' / S_8 : \begin{cases} \phi \to \pi - \phi & \text{for } \phi > \pi/2 \\ \phi \to -\pi - \phi & \text{for } \phi < -\pi/2 \\ \theta_K \to \pi - \theta_K & \text{for } \theta_l > \pi/2 \\ \theta_l \to \pi - \theta_l & \text{for } \theta_l > \pi/2. \end{cases}$$
(6)

These transformations exploit the symmetries of the angular terms in Eq. 1, so that only the first five terms and one of the terms containing the  $P'_i$  survive. One gets four datasets and four pdfs, each containing only three parameters:  $F_L$ ,  $S_3$ and one of the  $P'_i$ . These angular transformations were also done in the analysis described in Ref. [5].

### IV. MONTE CARLO TOY STUDY

# A. Estimation of the number of signal events

For the MC study it is important to know, how many signal events are expected. For this aim a large MC data sample of  $B \to K^* l^+ l^-$  was generated, propagated through the detector and reconstructed [10]. The numbers of events per  $q^2$ bin were scaled down so that the total number of

TABLE I. Dividing the data into bins of  $q^2$ . Additionally the expected number of events per bin is given for the case of 300 signal events in all bins together.

bin	$q^2  [ { m GeV}^2/c^4  ]$	expected number
		of signal events
1	0.10 - 2.00	59
2	2.00 - 4.30	37
3	4.30 - 8.68	77
4	10.09 - 12.90	59
5	14.18 - 16.00	34
6	16.00 - 19.00	34

events is 300, which is reasonable if we sum over neutral and charged B mseons. The expected numbers of signal events per bin are listed in Table I.

### **B.** Fitting techniques

I always performed an unbinned maximum likelihood fit using RooFit [11]. After every fit asymmetric errors are calculated. These are then referred to as the upper and the lower error.

Four different possibilities of performing the fit were considered: One can fit the pdfs to the distributions in  $\cos \theta_l$ ,  $\cos \theta_K$  and  $\phi$  or one can fit the pdfs to the distributions in  $\theta_l$ ,  $\theta_K$  and  $\phi$ . The latter requires the transformation

$$\frac{\mathrm{d}\Gamma}{\mathrm{d}\theta_l \mathrm{d}\theta_K \mathrm{d}\phi} = \frac{\mathrm{d}\Gamma}{\mathrm{d}\cos\theta_l \mathrm{d}\cos\theta_K \mathrm{d}\phi} \times \sin\theta_l \sin\theta_K.$$
(7)

Additionally, one can perform the fit for each of the four datasets and pdfs independently or

#### С. Procedure of the Monte Carlo toy study

One major part of my project was to evaluate how sensitive this fit is to the observables defined in Eq. 2, i.e. how large the errors of these observables are. Therefore, 10000 data samples with the number of entries given in Table I are generated according to the 'untransformed' pdf defined in Eq. 1. For the generation, the parameters  $F_L$ ,  $S_3$ ,  $P'_4$ ,  $P'_5$ ,  $P'_6$  are fixed to SM predictions from Ref. [9], whereas  $P'_8$  is fixed to the measurement by LHCb [5] and  $S_6$  and  $S_9$ are chosen such that the pdf stays not negative in the allowed range of the angles. Then these data samples are transformed as described in (3)- (6). The next step is to perform each of the four fits to every of the 10000 data samples and to store the fitted values and the asymmetric errors of the values. The mean values of the resulting distributions of the errors are regarded as good measures for the errors of the fit to data. A pull can be defined as

$$pull_{value} = \frac{value_{fitted} - value_{true}}{error_{value}}.$$
 (8)

If  $value_{fitted} - value_{true} > 0$  then the magnitude of the lower error will be asigned. Otherwise the upper error will be asigned. With this definition it is easy to see that a perfect pull distribution should have a mean of zero and a standard deviation of one. Therefore, the mean and the

simultaniously in a combined fit since all four standard deviation of the pull distribution is a pdfs share two common parameters:  $F_L$  and  $S_3$ . measure for the quality of the fitting technique.

#### D. Results

The results of this study are presented in Tables II and III. The mean value of the error for all observables  $P'_i$  is approximately the same and is independent of the fitting technique. As expected, the absolute value of the mean error is close to an antiproportional behavior compared to the number of generated events per bin (see Table I). Figures 4 and 5 show the mean value of the fit error of  $P'_4$  and  $P'_5$ .

The pull distributions for  $P'_6$  and  $P'_8$  are almost perfect. The deviations from the ideal values are always less than 0.15. For  $P'_4$  and  $P'_5$  the pull distributions show a larger deviation from the ideal values (up to 0.5). To be sure that this is not caused by a bug in the MC toy study, it is repeated: once 100 events are generated in each bin and a second time 1000 events are generated per bin. In Figures 6 and 7 the result is shown for  $P'_5$ . One can see that with increasing statistics the pull distributions improve. This behavior is also found for  $P'_4$ . The outcome of this additional study is that the deviation of the pull distribution from the ideal one is related to the low statistics.

In Figures 8 and 9 the expected sensitivity to the parameters  $P'_4$  and  $P'_5$  in comparison to the LHCb measurement [5] is shown.



FIG. 4. The mean value of the asymmetric error of FIG. 6. The mean value of the pull distribution for six  $q^2$  bins. The positive value is the upper error and erated events in the six  $q^2$  bins. the negative is the lower error.



FIG. 5. The mean value of the asymmetric error of the parameter  $P'_5$  for all four fitting techniques in the six  $q^2$  bins. The positive value is the upper error and the negative is the lower error.

#### v. CONCLUSION AND OUTLOOK

Although LHCb has higher statistics than Belle (~ 880 signal events [7]), this study has shown that the sensitivity of Belle is sufficient to make a significant independent measurement of the observables  $P'_{4,5,6,8}$ . Nevertheless, this is



the parameter  $P'_4$  for all four fitting techniques in the the parameter  $P'_5$  for three different numbers of gen-



FIG. 7. The RMS value of the pull distribution for the parameter  $P'_5$  for three different numbers of generated events in the six  $q^2$  bins.

only the first stage of the whole sensitivity study, since background and efficiency corrections need to be included in the pdf to get a more realistic picture.

In the near future, LHCb will analyze more data which will clear up the behavior of the measured  $3.7 \sigma$  effect. Also Belle II will start operating in the next years to provide a second measurement with higher statistics.



FIG. 8. The expected statistical error for the fit of the parameter  $P'_4$  (MC Simulation) in comparison to the measurement of LHCb [5] (including systematic uncertainties) and SM predictions [9].



FIG. 9. The expected statistical error for the fit of the parameter  $P'_5$  (MC Simulation) in comparison to the measurement of LHCb [5] (including systematic uncertainties) and SM predictions [9].

## ACKNOWLEDGMENTS

I want to thank the Helmholtz Association, Desy, Belle, and especially the Desy Belle group to give me the opportunity to participate in this program and to be part of state-of-the-art research. A big thank you goes to the organization team of the Summer Student Programme. From the Belle group at Desy, I want to mention the names of Oliver Frost, Sergey Yashchenko and the one who deserves the most acknowledgments, Simon Wehle.

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$P_4'$ fit	simulta	nious, $\theta$	indeper	ndent, $\theta$	simultani	ous, $\cos \theta$	independe	nt, $\cos \theta$
bin	upper	lower	upper	lower	upper	lower	upper	lower
1	0.313	-0.325	0.322	-0.330	0.313	-0.325	0.322	-0.330
2	0.520	-0.505	0.502	-0.517	0.525	-0.507	0.502	-0.516
3	0.261	-0.230	0.266	-0.240	0.261	-0.230	0.266	-0.240
4	0.294	-0.255	0.301	-0.270	0.294	-0.255	0.301	-0.270
5	0.422	-0.372	0.440	-0.422	0.422	-0.372	0.440	-0.422
6	0.434	-0.384	0.449	-0.443	0.434	-0.384	0.449	-0.443
D/ C	• 1	• •		1 0	• 1, •	0		
$P'_5$ fit	simulta	nious, $\theta$	indeper	ident, $\theta$	simultani	ous, $\cos\theta$	independe	nt, $\cos\theta$
bın	upper	lower	upper	lower	upper	lower	upper	lower
1	0.260	-0.289	0.276	-0.294	0.260	-0.289	0.276	-0.294
2	0.498	-0.487	0.492	-0.519	0.500	-0.491	0.492	-0.519
3	0.233	-0.199	0.241	-0.221	0.233	-0.199	0.241	-0.221
4	0.254	-0.209	0.261	-0.230	0.254	-0.209	0.261	-0.230
5	0.376	-0.319	0.387	-0.365	0.376	-0.319	0.386	-0.365
6	0.379	-0.334	0.387	-0.373	0.379	-0.334	0.387	-0.373
$P'_{c}$ fit	simulta	nious. $\theta$	indeper	ndent. $\theta$	simultani	ous. $\cos \theta$	independe	nt. $\cos\theta$
$P'_6$ fit	simulta	nious, $\theta$	indeper	ndent, $\theta$	simultani	ous, $\cos \theta$	independe	nt, $\cos \theta$
$P'_6$ fit bin 1	simulta upper	anious, $\theta$ lower	indeper upper	ndent, $\theta$ lower	simultani upper	ous, $\cos \theta$ lower	independe upper	nt, $\cos \theta$ lower
$\frac{P_6' \text{ fit}}{1}$	simulta upper 0.295 0.496	anious, $\theta$ lower -0.290	indeper upper 0.299 0.501	ndent, $\theta$ lower -0.297 -0.507	simultani upper 0.295 0.501	ous, $\cos \theta$ lower -0.290 -0.497	independe upper 0.299 0.500	nt, $\cos \theta$ lower -0.297 -0.507
$     \frac{P'_6 \text{ fit}}{1}     2     3   $	simulta upper 0.295 0.496 0.261	anious, $\theta$ lower -0.290 -0.494 -0.260	indeper upper 0.299 0.501 0.264	ndent, $\theta$ lower -0.297 -0.507 -0.263	simultani upper 0.295 0.501 0.261	ous, $\cos \theta$ lower -0.290 -0.497 -0.260	independe upper 0.299 0.500 0.264	nt, $\cos \theta$ lower -0.297 -0.507 -0.263
$ \begin{array}{c} P_6' \text{ fit} \\ \hline bin \\ 1 \\ 2 \\ 3 \\ 4 \end{array} $	simulta upper 0.295 0.496 0.261 0.285	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285	indeper upper 0.299 0.501 0.264 0.289	ndent, $\theta$ lower -0.297 -0.507 -0.263 -0.288	simultani upper 0.295 0.501 0.261 0.285	ous, $\cos \theta$ lower -0.290 -0.497 -0.260 -0.285	independe upper 0.299 0.500 0.264 0.289	$     nt, \cos \theta \\     lower \\     -0.297 \\     -0.507 \\     -0.263 \\     -0.288 $
$ \begin{array}{c} P_6' \text{ fit} \\ \hline bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \end{array} $	simulta upper 0.295 0.496 0.261 0.285 0.388	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285 -0.388	indeper upper 0.299 0.501 0.264 0.289 0.400	ndent, $\theta$ lower -0.297 -0.507 -0.263 -0.288 -0.400	simultani upper 0.295 0.501 0.261 0.285 0.388	ous, $\cos \theta$ lower -0.290 -0.497 -0.260 -0.285 -0.388	independe upper 0.299 0.500 0.264 0.289 0.400	nt, $\cos \theta$ lower -0.297 -0.507 -0.263 -0.288 -0.400
$ \begin{array}{c} P_6' \text{ fit} \\ \hline bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{array} $	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285 -0.388 -0.401	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414	ndent, $\theta$ lower -0.297 -0.507 -0.263 -0.288 -0.400 -0.414	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400	ous, $\cos \theta$ lower -0.290 -0.497 -0.260 -0.285 -0.388 -0.401	independe upper 0.299 0.500 0.264 0.289 0.400 0.414	$     nt, \cos \theta \\     lower \\     -0.297 \\     -0.507 \\     -0.263 \\     -0.288 \\     -0.400 \\     -0.414 $
$\begin{array}{c} P_6' \text{ fit} \\ \hline \\ bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \end{array}$	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400	$\begin{array}{c} \text{mious, } \theta \\ \hline \\ 10 \text{wer} \\ -0.290 \\ -0.494 \\ -0.260 \\ -0.285 \\ -0.388 \\ -0.401 \end{array}$	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414	ndent, $\theta$ lower -0.297 -0.507 -0.263 -0.288 -0.400 -0.414	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401	independe upper 0.299 0.500 0.264 0.289 0.400 0.414	$ \begin{array}{r}     \text{nt, } \cos \theta \\     \text{lower} \\     -0.297 \\     -0.507 \\     -0.263 \\     -0.288 \\     -0.400 \\     -0.414 \\ \end{array} $
$ \begin{array}{c} P_6' \text{ fit} \\ \hline bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \hline P_8' \text{ fit} \end{array} $	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400 simulta	unious, $θ$ lower         -0.290         -0.494         -0.260         -0.285         -0.388         -0.401	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414 indeper	ndent, $\theta$ lower -0.297 -0.507 -0.263 -0.288 -0.400 -0.414 ndent, $\theta$	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400 simultani	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401	independe upper 0.299 0.500 0.264 0.289 0.400 0.414 independe	$ \begin{array}{c c} \text{nt, } \cos \theta \\ \hline & \text{lower} \\ \hline -0.297 \\ -0.507 \\ -0.263 \\ -0.288 \\ -0.288 \\ -0.400 \\ -0.414 \\ \hline \\ \hline \\ \text{nt, } \cos \theta \end{array} $
$\begin{array}{c} P_6' \text{ fit} \\ \hline \\ bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \hline \\ P_8' \text{ fit} \\ bin \\ \end{array}$	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400 simulta upper	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285 -0.388 -0.401 anious, $\theta$ lower	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414 indeper upper	ndent, $\theta$ lower -0.297 -0.507 -0.263 -0.288 -0.400 -0.414 ndent, $\theta$ lower	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400 simultani upper	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401         ous, $\cos \theta$ lower	independe upper 0.299 0.500 0.264 0.289 0.400 0.414 independe upper	
$\begin{array}{c} P_6' \text{ fit} \\ \hline \\ bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \hline \\ P_8' \text{ fit} \\ \hline \\ bin \\ 1 \\ \end{array}$	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400 simulta upper 0.322	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285 -0.388 -0.401 mious, $\theta$ lower -0.318	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414 indeper upper 0.328	ndent, $\theta$ lower -0.297 -0.507 -0.263 -0.288 -0.400 -0.414 ndent, $\theta$ lower -0.325	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400 simultani upper 0.322	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401         ous, $\cos \theta$ lower         -0.318	independe upper 0.299 0.500 0.264 0.289 0.400 0.414 independe upper 0.328	
$\begin{array}{c} P_6' \text{ fit} \\ \hline \\ bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \hline \\ P_8' \text{ fit} \\ \hline \\ bin \\ 1 \\ 2 \\ \end{array}$	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400 simulta upper 0.322 0.509	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285 -0.388 -0.401 mious, $\theta$ lower -0.318 -0.506	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414 indeper upper 0.328 0.502	$\begin{array}{c c} \text{adent, } \theta \\ \hline \\ \text{lower} \\ -0.297 \\ -0.507 \\ -0.263 \\ -0.288 \\ -0.400 \\ -0.414 \\ \hline \\ \text{adent, } \theta \\ \hline \\ \text{lower} \\ -0.325 \\ -0.508 \\ \end{array}$	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400 simultani upper 0.322 0.515	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401         ous, $\cos \theta$ lower         -0.318         -0.509	independe upper 0.299 0.500 0.264 0.289 0.400 0.414 independe upper 0.328 0.501	
$     \begin{array}{r}       P_{6}' \text{ fit} \\       bin \\       1 \\       2 \\       3 \\       4 \\       5 \\       6 \\       \hline       P_{8}' \text{ fit} \\       bin \\       1 \\       2 \\       3 \\       3       \end{array} $	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400 simulta upper 0.322 0.509 0.268	$\begin{array}{c c} \text{unious, } \theta \\ \hline \\ 1 \text{ower} \\ \hline \\ -0.290 \\ -0.494 \\ -0.260 \\ -0.285 \\ -0.388 \\ -0.401 \\ \hline \\ \text{unious, } \theta \\ \hline \\ 1 \text{ower} \\ \hline \\ -0.318 \\ -0.506 \\ -0.265 \\ \end{array}$	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414 indeper upper 0.328 0.502 0.270	$\begin{array}{c c} \text{adent, } \theta \\ \hline \\ \text{lower} \\ \hline \\ -0.297 \\ -0.507 \\ -0.263 \\ -0.268 \\ -0.288 \\ -0.400 \\ -0.414 \\ \hline \\ \text{adent, } \theta \\ \hline \\ \text{lower} \\ -0.325 \\ -0.325 \\ -0.508 \\ -0.267 \\ \end{array}$	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400 simultani upper 0.322 0.515 0.268	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401         ous, $\cos \theta$ lower         -0.318         -0.509         -0.265	independe upper 0.299 0.500 0.264 0.289 0.400 0.414 independe upper 0.328 0.501 0.270	
$\begin{array}{c} P_6' \text{ fit} \\ \hline \\ bin \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \hline \\ P_8' \text{ fit} \\ \hline \\ bin \\ 1 \\ 2 \\ 3 \\ 4 \\ \end{array}$	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400 simulta upper 0.322 0.509 0.268 0.303	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285 -0.388 -0.401 anious, $\theta$ lower -0.318 -0.506 -0.265 -0.298	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414 indeper upper 0.328 0.502 0.270 0.305	$\begin{array}{c c} \text{adent, } \theta \\ \hline \\ \text{lower} \\ \hline -0.297 \\ -0.507 \\ \hline \\ -0.263 \\ -0.288 \\ -0.288 \\ \hline \\ -0.400 \\ -0.414 \\ \hline \\ \hline \\ \text{adent, } \theta \\ \hline \\ \hline \\ \text{lower} \\ \hline \\ -0.325 \\ -0.508 \\ -0.267 \\ -0.301 \\ \hline \end{array}$	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400 simultani upper 0.322 0.515 0.268 0.303	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401         ous, $\cos \theta$ lower         -0.318         -0.509         -0.265         -0.298	independe upper 0.299 0.500 0.264 0.289 0.400 0.414 independe upper 0.328 0.501 0.270 0.305	
$\begin{array}{c} P_{6}' \mbox{ fit } \\ \mbox{bin} \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ \hline P_{8}' \mbox{ fit } \\ \mbox{bin} \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ \end{array}$	simulta upper 0.295 0.496 0.261 0.285 0.388 0.400 simulta upper 0.322 0.509 0.268 0.303 0.421	anious, $\theta$ lower -0.290 -0.494 -0.260 -0.285 -0.388 -0.401 mious, $\theta$ lower -0.318 -0.506 -0.265 -0.298 -0.419	indeper upper 0.299 0.501 0.264 0.289 0.400 0.414 indeper upper 0.328 0.502 0.270 0.305 0.434	$\begin{array}{c c} \text{adent, } \theta \\ \hline \\ \text{lower} \\ \hline -0.297 \\ -0.507 \\ -0.263 \\ -0.288 \\ -0.288 \\ -0.400 \\ -0.414 \\ \hline \\ \hline \\ \text{adent, } \theta \\ \hline \\ \hline \\ \text{lower} \\ -0.325 \\ -0.508 \\ -0.267 \\ -0.301 \\ -0.433 \\ \end{array}$	simultani upper 0.295 0.501 0.261 0.285 0.388 0.400 simultani upper 0.322 0.515 0.268 0.303 0.421	ous, $\cos \theta$ lower         -0.290         -0.497         -0.260         -0.285         -0.388         -0.401         ous, $\cos \theta$ lower         -0.318         -0.509         -0.265         -0.298         -0.401	independe upper 0.299 0.500 0.264 0.289 0.400 0.414 independe upper 0.328 0.501 0.270 0.305 0.434	$\begin{array}{c c} \text{nt, } \cos \theta \\ \hline \\ \text{lower} \\ \hline -0.297 \\ -0.507 \\ -0.263 \\ -0.263 \\ -0.288 \\ -0.400 \\ -0.414 \\ \hline \\ \hline \\ \text{nt, } \cos \theta \\ \hline \\ \text{nt, } \cos \theta \\ \hline \\ \hline \\ \text{lower} \\ -0.325 \\ -0.507 \\ -0.267 \\ -0.301 \\ -0.433 \\ \end{array}$

TABLE II. Mean values of the upper and lower fit errors for the paramters  $P'_i$  for the four fitting techniques.

$P_4'$ fit	simulta	nious, $\theta$	indepen	ident, $\theta$	simultani	ous, $\cos \theta$	independer	nt, $\cos \theta$
bin	mean	RMS	mean	RMS	mean	RMS	mean	RMS
1.	0.027	1.055	0.033	1.057	0.027	1.055	0.033	1.057
2.	-0.071	1.157	-0.049	1.105	-0.070	1.157	-0.049	1.105
3.	-0.075	1.096	-0.108	1.090	-0.075	1.096	-0.108	1.090
4.	-0.115	1.168	-0.151	1.156	-0.115	1.168	-0.151	1.156
5.	-0.199	1.295	-0.226	1.236	-0.199	1.295	-0.226	1.236
6.	-0.276	1.379	-0.296	1.296	-0.276	1.379	-0.296	1.296
D' 6+	simulto	nious A	indopor	dont A	simultani		indopondor	at and
$I_5$ III	moon	DMS	moon	DMS	moon	DUS, COSU	moon	DMS
1	0.070	1 091	0.119	1.074	0.070	1 091	0.119	1.074
1. 0	0.079	1.001	0.110	1.074	0.079	1.001	0.110	1.074
2. 3	-0.055	1.112	-0.007	1.104	-0.000	1.112 1.943	-0.007	1 1 1 0 0
<b>у</b> . Д	-0.102	1.245 1.347	-0.205	1.135	-0.102	1.245 1.347	-0.200	1.133
ч. 5	-0.338	1.047	-0.410	1.304	-0.300	1.947	-0.410	1.304
6.	-0.338	1.420 1 342	-0.357	1 306	-0.330	1.420 1 342	-0.350	1 306
0.	0.230	1.042	0.002	1.000	-0.250	1.042	-0.002	1.000
$P_6'$ fit	simulta	nious, $\theta$	indepen	dent, $\theta$	simultani	ous, $\cos \theta$	independer	nt, $\cos \theta$
$P'_6$ fit bin	simulta mean	nious, θ RMS	indepen mean	dent, $\theta$ RMS	simultani mean	ous, $\cos \theta$ RMS	independer mean	nt, $\cos \theta$ RMS
$\frac{P'_6 \text{ fit}}{1.}$	simulta mean -0.021	nious, $\theta$ RMS 1.049	indepen mean -0.026	adent, $\theta$ RMS 1.058	simultani mean -0.021	ous, $\cos \theta$ RMS 1.049	independer mean -0.026	$\frac{\text{nt, } \cos \theta}{\text{RMS}}$
$     \begin{array}{c}             P_6' \text{ fit} \\             bin \\             1. \\             2.         $	simulta mean -0.021 0.000	nious, θ RMS 1.049 1.081	indepen mean -0.026 -0.002	adent, θ RMS 1.058 1.089	simultani mean -0.021 -0.002	ous, $\cos \theta$ RMS 1.049 1.080	independer mean -0.026 -0.002	$\frac{\text{nt, } \cos \theta}{\text{RMS}}$ $1.058$ $1.089$
$     \hline     \hline     P_6' fit     bin     1.     2.     3.   $	simulta mean -0.021 0.000 -0.013	nious, θ RMS 1.049 1.081 1.031	indepen mean -0.026 -0.002 -0.016	ident, θ RMS 1.058 1.089 1.040	simultani mean -0.021 -0.002 -0.013	ous, $\cos \theta$ RMS 1.049 1.080 1.031	independer mean -0.026 -0.002 -0.016	$\frac{\text{RMS}}{1.058}$ $1.089$ $1.040$
$     \hline     \hline     P_6' fit     bin     1.     2.     3.     4.     $	simulta mean -0.021 0.000 -0.013 -0.011	nious, $\theta$ RMS 1.049 1.081 1.031 1.042	indepen mean -0.026 -0.002 -0.016 -0.010	$\begin{array}{c} \text{dent, } \theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042	independer mean -0.026 -0.002 -0.016 -0.010	$     \text{nt, } \cos \theta \\     \text{RMS} \\     1.058 \\     1.089 \\     1.040 \\     1.053     $
$     \hline     \hline     P_6' fit     bin     1.     2.     3.     4.     5.      $	simulta mean -0.021 0.000 -0.013 -0.011 0.001	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001	$\begin{array}{c} \text{adent, } \theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074	independer mean -0.026 -0.002 -0.016 -0.010 -0.001	$\begin{array}{c} \text{nt, } \cos\theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \end{array}$
$     \begin{array}{c}         P_6' \text{ fit} \\         bin \\         1. \\         2. \\         3. \\         4. \\         5. \\         6. \\         \end{array}     $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074 1.056	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006	$\begin{array}{c} \text{ident, } \theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.056	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006	$\begin{array}{c} \text{nt, } \cos\theta \\ \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \end{array}$
$     \hline     \hline     P_6' \text{ fit}     \\     bin     1.     2.     3.     4.     5.     6.     \hline     P_6' \text{ fit}   $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008 simulta	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074 1.056 nious, $\theta$	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 indepen	adent, $\theta$ RMS 1.058 1.089 1.040 1.053 1.080 1.060 adent, $\theta$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008 simultani	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.056 ous, $\cos \theta$	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 independer	$\begin{array}{c} \text{nt, } \cos \theta \\ \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{nt, } \cos \theta \end{array}$
$     \hline     \hline     P_{6}' \text{ fit} \\     \hline     bin     1.     2.     3.     4.     5.     6.     \hline     P_{8}' \text{ fit} \\     bin     bin   $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008 simulta mean	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074 1.056 nious, $\theta$ RMS	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 indepen mean	dent, $\theta$ RMS 1.058 1.089 1.040 1.053 1.080 1.060	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008 simultani mean	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.056 ous, $\cos \theta$ RMS	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 independer mean	$\begin{array}{c} \text{nt, } \cos \theta \\ \text{RMS} \\ 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{nt, } \cos \theta \\ \text{RMS} \end{array}$
$     \hline     \hline     P_{6}' \text{ fit} \\     bin \\     1. \\     2. \\     3. \\     4. \\     5. \\     6. \\     \hline     \hline     P_{8}' \text{ fit} \\     bin \\     1. \\     1.   $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008 simulta mean -0.028	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074 1.074 1.056 nious, $\theta$ RMS 1.045	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 indepen mean -0.030	$\begin{array}{c c} \text{adent, } \theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \hline \\ \text{adent, } \theta \\ \hline \\ \text{RMS} \\ \hline \\ 1.047 \\ \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008 simultani mean -0.028	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.056 ous, $\cos \theta$ RMS 1.045	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 independer mean -0.030	$ \begin{array}{c} \text{nt, } \cos \theta \\ \text{RMS} \\ 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \text{nt, } \cos \theta \\ \hline \text{RMS} \\ 1.047 \\ \end{array} $
$     \hline     \hline     P_6' fit     bin     1.     2.     3.     4.     5.     6.     \hline     P_8' fit     bin     1.     2. $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008 simulta mean -0.028 -0.019	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074 1.074 1.056 nious, $\theta$ RMS 1.045 1.134	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 indepen mean -0.030 -0.006	$\begin{array}{c c} \text{adent, } \theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{adent, } \theta \\ \hline \\ \text{RMS} \\ \hline 1.047 \\ 1.105 \\ \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008 simultani mean -0.028 -0.020	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.074 1.056 ous, $\cos \theta$ RMS 1.045 1.134	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 independer mean -0.030 -0.006	$\begin{array}{c} \text{nt, } \cos \theta \\ \text{RMS} \\ 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.080 \\ 1.060 \\ \hline \\ \text{nt, } \cos \theta \\ \hline \\ \text{RMS} \\ 1.047 \\ 1.105 \end{array}$
$     \hline     \hline         P_6' fit     \\         bin     \hline         1.         2.         3.         4.         5.         6.     \hline         P_8' fit     bin     \hline         1.         2.         3.     }     $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008 simulta mean -0.028 -0.019 -0.005	nious, $\theta$ RMS 1.049 1.081 1.031 1.031 1.042 1.074 1.056 nious, $\theta$ RMS 1.045 1.134 1.046	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 -0.006 -0.030 -0.006 -0.007	$\begin{array}{c} \text{adent, } \theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{adent, } \theta \\ \hline \\ \text{RMS} \\ \hline 1.047 \\ 1.105 \\ 1.051 \\ \hline \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008 simultani mean -0.028 -0.020 -0.020 -0.005	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.056 ous, $\cos \theta$ RMS 1.045 1.134 1.046	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 independer mean -0.030 -0.006 -0.007	$\begin{array}{c} \text{nt, } \cos\theta \\ \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{nt, } \cos\theta \\ \hline \\ \text{RMS} \\ \hline 1.047 \\ 1.105 \\ 1.051 \\ \end{array}$
$     \hline     \hline         P_6' fit     \\         bin     \hline         1.         2.         3.         4.         5.         6.     \hline         P_8' fit     bin         1.         2.         3.         4.          4.         4.     }     $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008 simulta mean -0.028 -0.019 -0.005 -0.039	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074 1.056 nious, $\theta$ RMS 1.045 1.134 1.046 1.051	indepen mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 -0.001 -0.006 -0.030 -0.006 -0.007 -0.041	$\begin{array}{c} \text{adent, } \theta \\ \\ \text{RMS} \\ \hline 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{adent, } \theta \\ \\ \\ \text{RMS} \\ \hline 1.047 \\ 1.105 \\ 1.051 \\ 1.056 \\ \hline \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008 simultani mean -0.028 -0.020 -0.020 -0.005 -0.039	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.056 ous, $\cos \theta$ RMS 1.045 1.134 1.046 1.051	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 independer mean -0.030 -0.006 -0.007 -0.041	$\begin{array}{c} \text{nt, } \cos \theta \\ \text{RMS} \\ 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{nt, } \cos \theta \\ \text{RMS} \\ \hline \\ 1.047 \\ 1.105 \\ 1.051 \\ 1.056 \\ \end{array}$
$     \hline     \hline     P_6' fit     bin     1.     2.     3.     4.     5.     6.     \hline     P_8' fit     bin     1.     2.     3.     4.     5.     4.     5. $	simulta mean -0.021 0.000 -0.013 -0.011 0.001 0.008 simulta mean -0.028 -0.019 -0.005 -0.039 -0.013	nious, $\theta$ RMS 1.049 1.081 1.031 1.042 1.074 1.074 1.056 nious, $\theta$ RMS 1.045 1.134 1.046 1.051 1.085	indepen mean -0.026 -0.002 -0.016 -0.010 -0.010 -0.001 0.006 -0.006 -0.030 -0.006 -0.007 -0.041 -0.017	$\begin{array}{c c} \text{adent, } \theta \\ \hline \text{RMS} \\ \hline 1.058 \\ 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \hline \\ \text{adent, } \theta \\ \hline \\ \hline \\ \text{RMS} \\ \hline \\ 1.047 \\ 1.105 \\ 1.051 \\ 1.056 \\ 1.083 \\ \hline \end{array}$	simultani mean -0.021 -0.002 -0.013 -0.011 0.001 0.008 simultani mean -0.028 -0.020 -0.020 -0.005 -0.039 -0.013	ous, $\cos \theta$ RMS 1.049 1.080 1.031 1.042 1.074 1.056 ous, $\cos \theta$ RMS 1.045 1.134 1.046 1.051 1.085	independer mean -0.026 -0.002 -0.016 -0.010 -0.001 0.006 independer mean -0.030 -0.006 -0.007 -0.041 -0.017	$\begin{array}{c} \text{nt, } \cos \theta \\ \text{RMS} \\ 1.058 \\ 1.089 \\ 1.040 \\ 1.053 \\ 1.080 \\ 1.060 \\ \hline \\ \text{nt, } \cos \theta \\ \hline \\ \text{RMS} \\ 1.047 \\ 1.105 \\ 1.051 \\ 1.056 \\ 1.083 \\ \end{array}$

TABLE III. Mean values and standard deviation (RMS) of the pull distributions for the paramters  $P'_i$  for the four fitting techniques.