

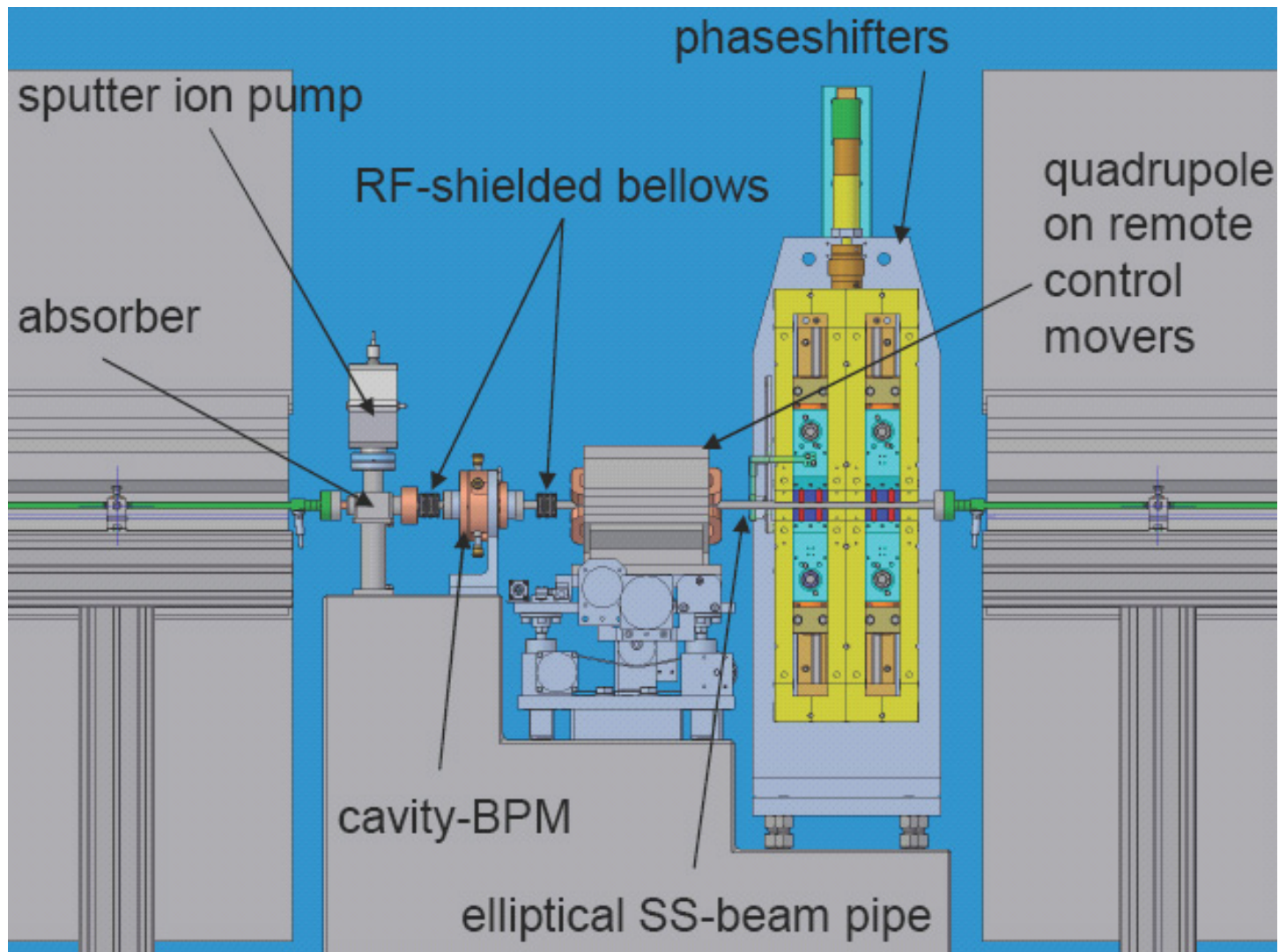


Wakefields impact on SASE2 XFEL performance

Igor Zagorodnov

Beam Dynamics Group Meeting

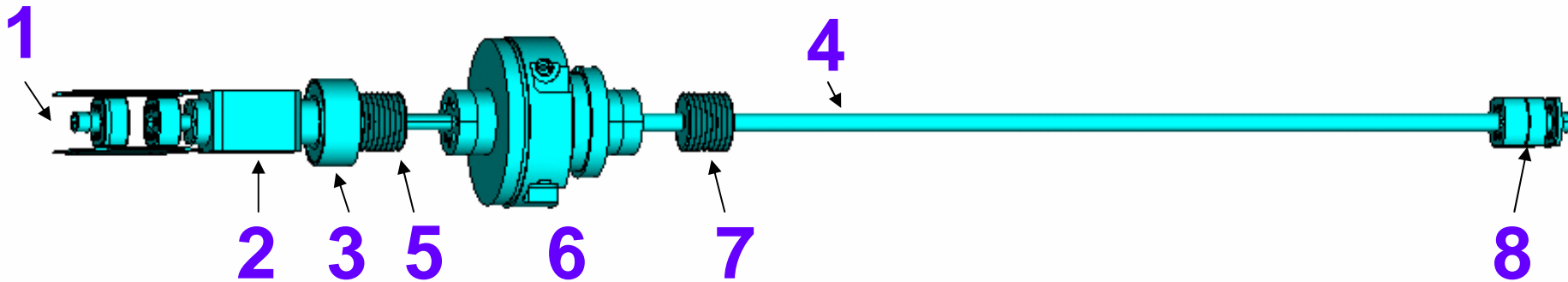
9.06.08



UNDULATOR- CELL(6.1m) = UNDULATOR (5m) + INTERSECTION (1.1m)

N	Element	from	to	Effective Length	Material	Conduct.	Relax. Time	Oxid layer	Roughness
		mm	mm	mm		1/Omm/m	sec	nm	nm
1	Elliptical pipe	0	5288	5161	Aluminium	3,66E+07	7,10E-15	5	300
2	Pump	5161	5266	105	Aluminium	3,66E+08	7,10E-15	5	300
3	Absorber/Round transition	5266	5288	22	Copper	5,80E+07	2,46E-14	5	300
4	Round pipe	5288	6100	652	Copper	5,80E+07	2,46E-14	5	300
5	Below	5288	5318	30	BeCu 174	2,78E+07	2,46E-14	5	300
6	BPM	5373	5473	100	Stainless Steel 304	1,40E+06	2,40E-15	5	300
7	Below	5513	5543	30	BeCu 174	2,78E+07	2,46E-14	5	300
8	Round/Elliptical transition	6100	6100	0					

6100



Katrin Schuett, ZM1
Dirk Lipka, MDI

$$\sigma = 25 \mu\text{m} \quad q = 1 \text{ nC}$$

N	Element	Geom Loss	Geom Spread	Loss	Spread
		kV	kV	kV	kV
1	Elliptical pipe	0	0	239	274
2	Pump	4,4	4,5	9	10
3	Absorber/Round transition	69	27	70	28
4	Round pipe	0	0	22	32
5	Below	24	9	25	10
6	BPM	42	17	70	34
7	Below	24	9	25	10
8	Round/Elliptical transition	36	14	36	14

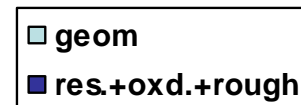
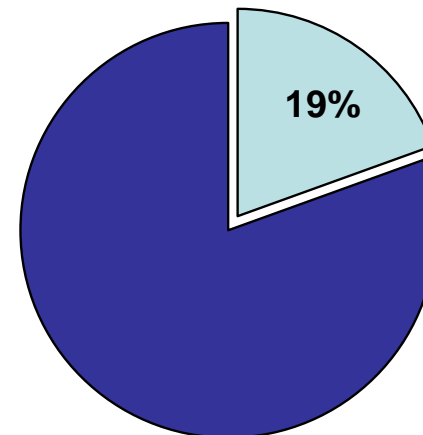
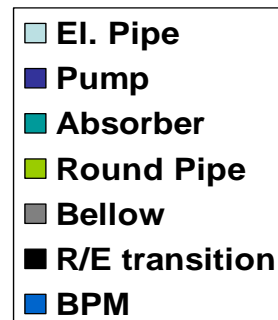
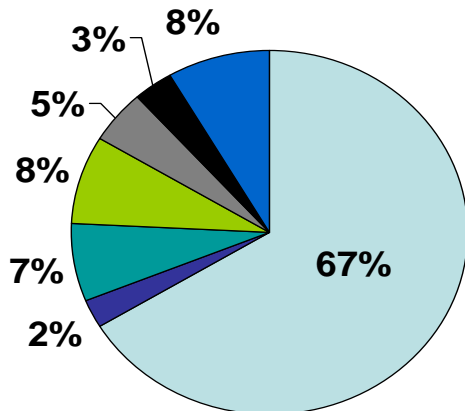
Energy Spread

199,4

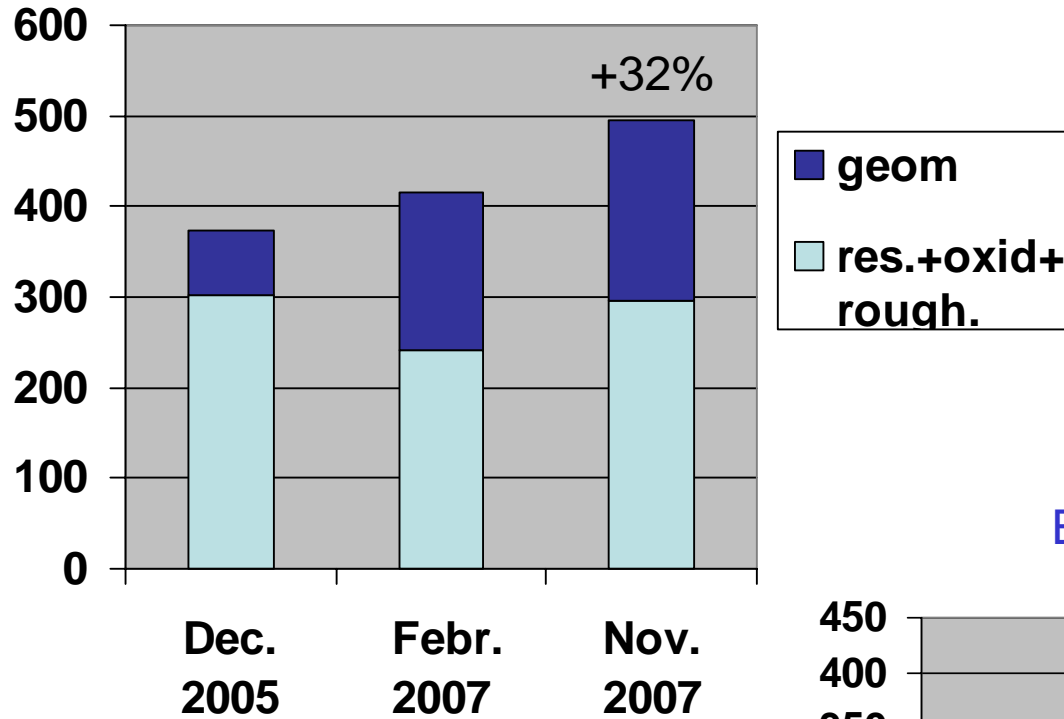
80,5

496

412(365)



Energy Loss



$$\sigma = 25 \mu\text{m}$$

TESLA-FEL Report 2005-10

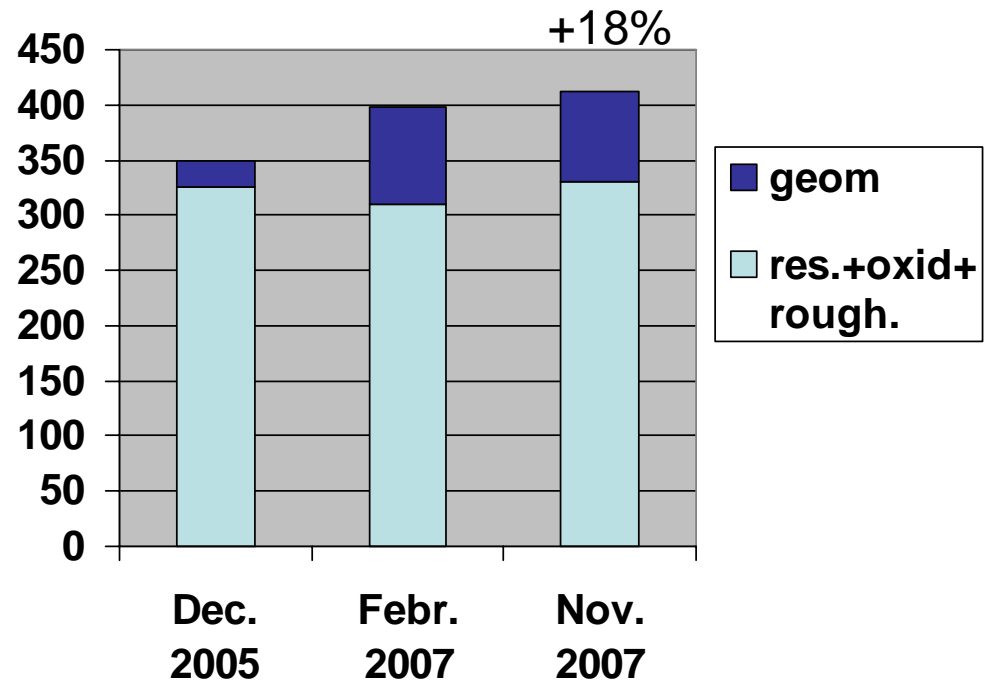
FEL simulations with
 $\varepsilon = 0.7 \text{ mm} \cdot \text{mrad}$

New FEL simulations with
new wakefields and

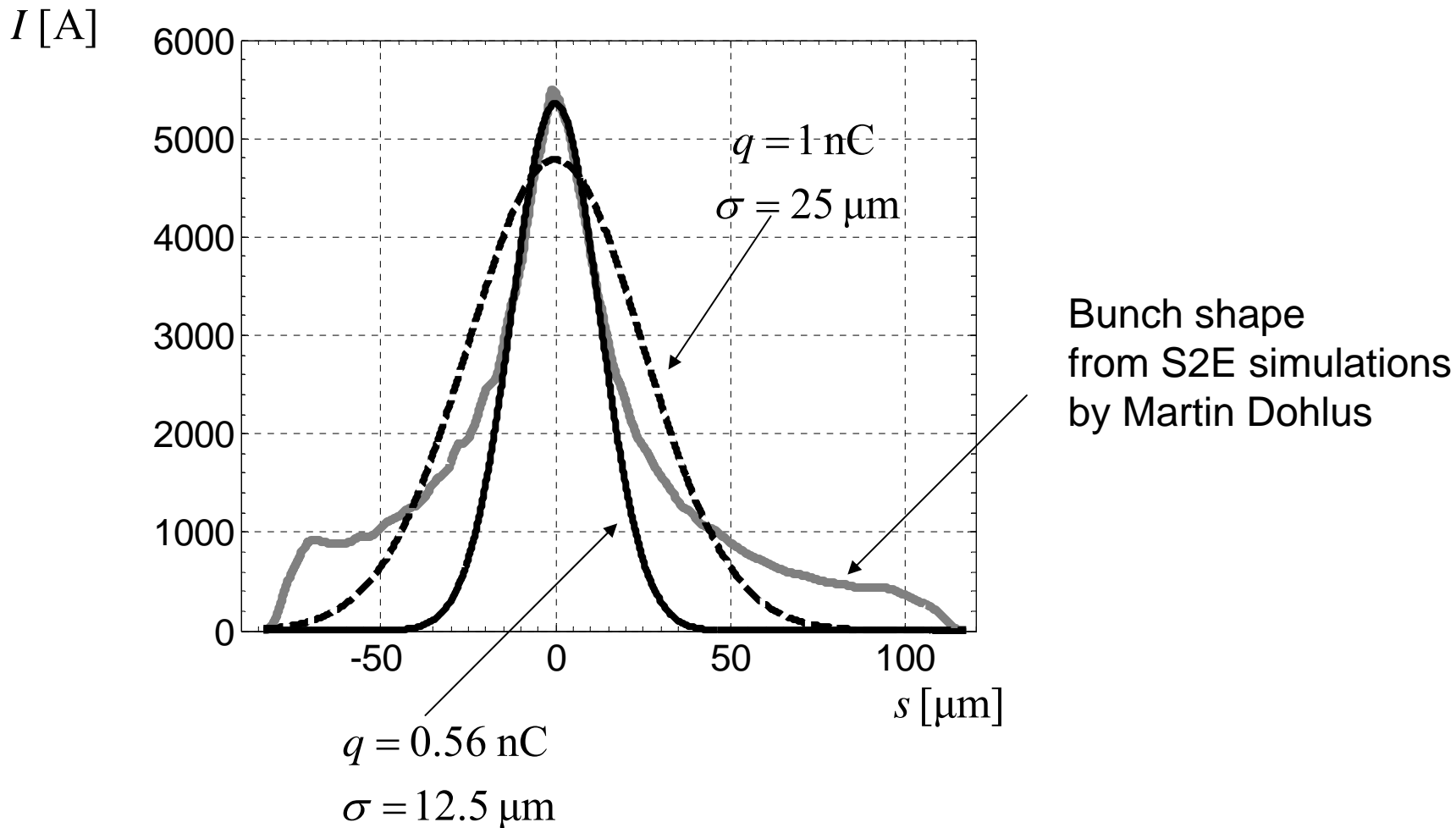
$$\varepsilon = 1.4 \text{ mm} \cdot \text{mrad}$$

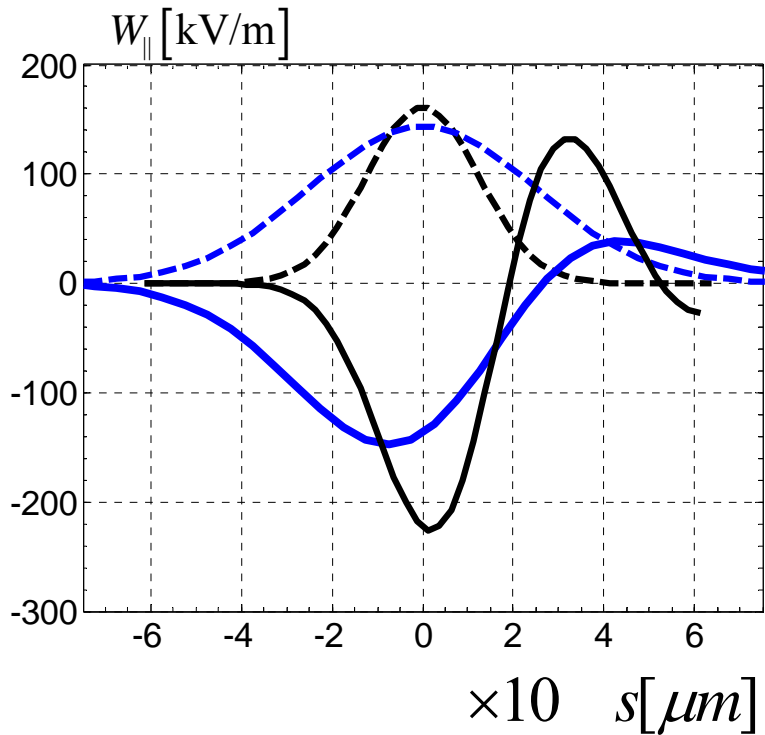
are required.

Energy Spread



Gaussian fit of the bunch shape from S2E simulations



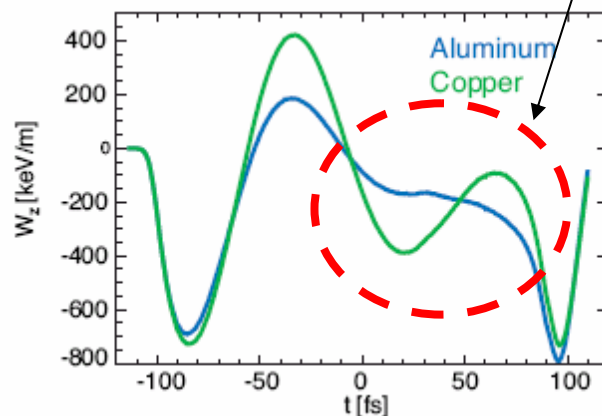
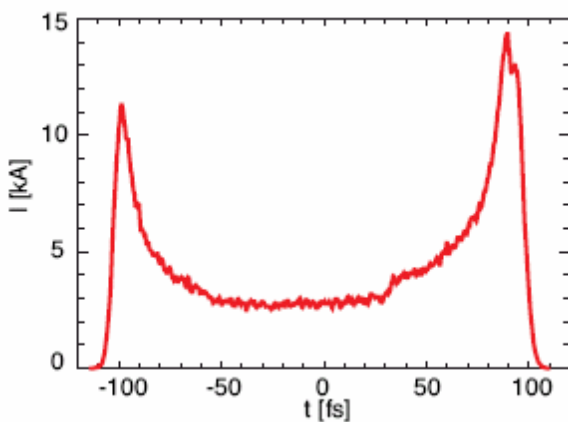


$$\delta_A = \frac{W_A L}{E \rho_1}$$

- fractional energy
oscillation amplitude

	LCLS	XFEL SASE2 (q=1nC, sig=25mkm)	XFEL SASE2 (q=0.56nC, sig=12.5mkm)
W_A , kV/m	200	140	220
L, m (L_sat)	100 (90)	200 (175)	200 (175)
E, GeV	14	17.5	17.5
ρ_1	3.2e-4	4e-4	4e-4
δ_A	4.5	4	6.3

K. Bane and G. Stupakov



Genesis (S.Reiche et al)

- only 3D
- 3D Cartesian field solver (ADI)
- Runge-Kutta integrator
- Dirichlet boundary conditions
- **transverse motion**
- many other physics
- parallel (MPI)

ALICE

- 1D/2D/3D
- 3D azimuthal field solver (Neumann)
- Leap-Frog integrator
- Perfectly Matched Layer
- **transverse motion**
- simplified model
- parallel (MPI)
- tested by me on the examples from the book of SSY

(~Saldin et al, 2000 „The Physics ...“ ,)

General properties of XFEL sources

- Operation at fixed electron energy 17.5 GeV
- Continuous covering of design wavelength range with three SASE FELs

Electron beam		
	Units	
Energy	GeV	17.5
Bunch charge	nC	1
Peak current	kA	5
Bunch length (rms)	μm	25
Norm. emittance (rms)	mm-mrad	1.4
Energy spread (rms)	MeV	1.5
# bunches p. pulse	#	3250
Repetition rate	Hz	10

2.5 MeV?



Undulators:

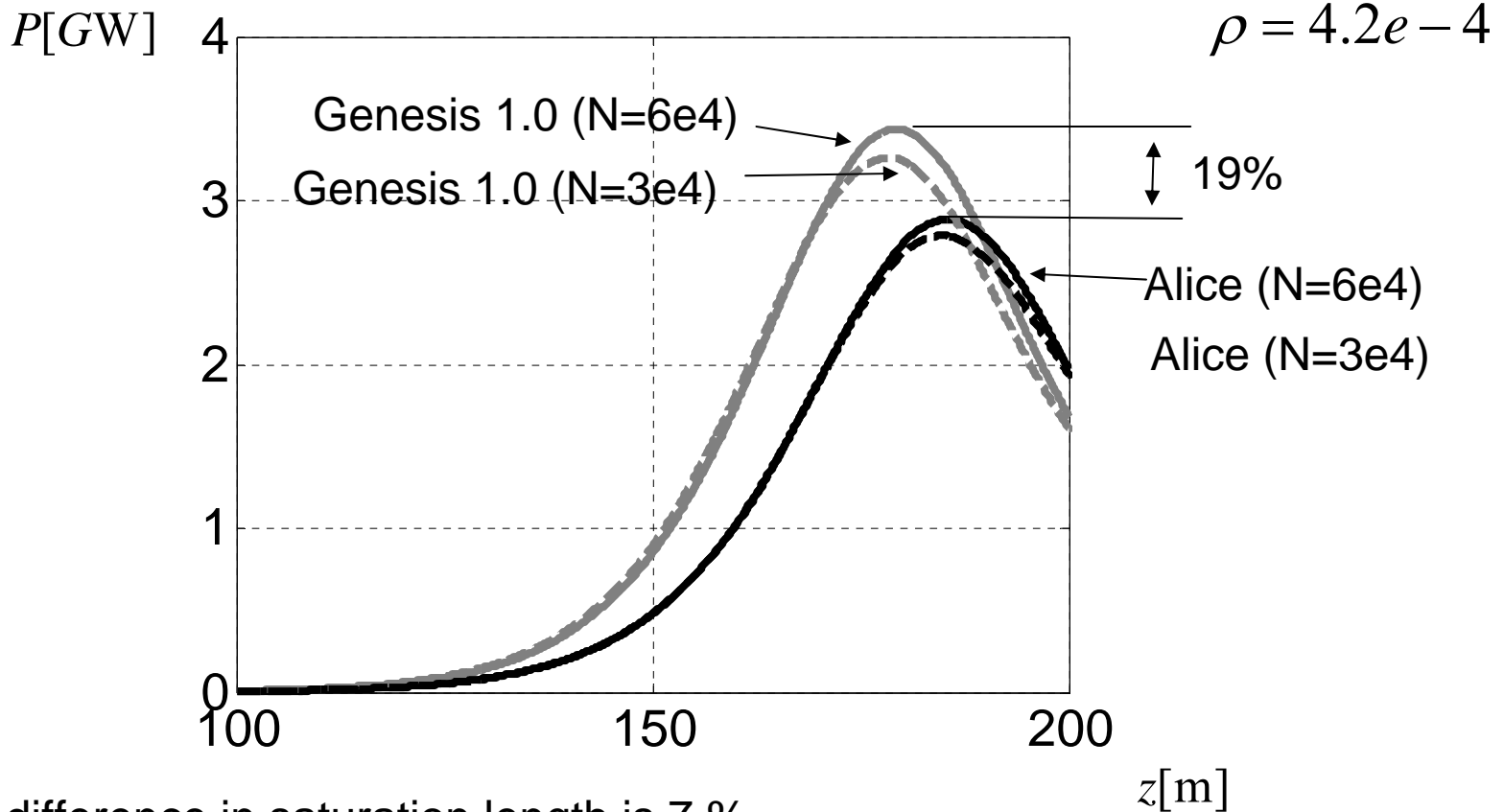
	λ_r nm	λ_U mm	L_w m
SASE1	0.1	35.6	200
SASE2	0.1-0.4	48	260
SASE3	0.4-1.6	65	130

Possible XUV option

SASE4	1.6-6.4	110	80
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Genesis vs. ALICE with transverse motion

$C = 0$ $I = 5 \text{KA}$
 $P_0 = 4 \text{ kW}$ $N_\lambda \sim 10\,400$
 $\sigma_E = 2.5 \text{ MeV}$ $\lambda_s = 0.1 \text{ nm}$
 $\varepsilon = 1.4 \text{ mm} \cdot \text{mrad}$



The difference in saturation length is 7 %.

The difference in power gain is 19 %.

The difference **does not reduce** with changing of the discrete model parameters ?!.

Genesis 2.0 released on 16.04.2008

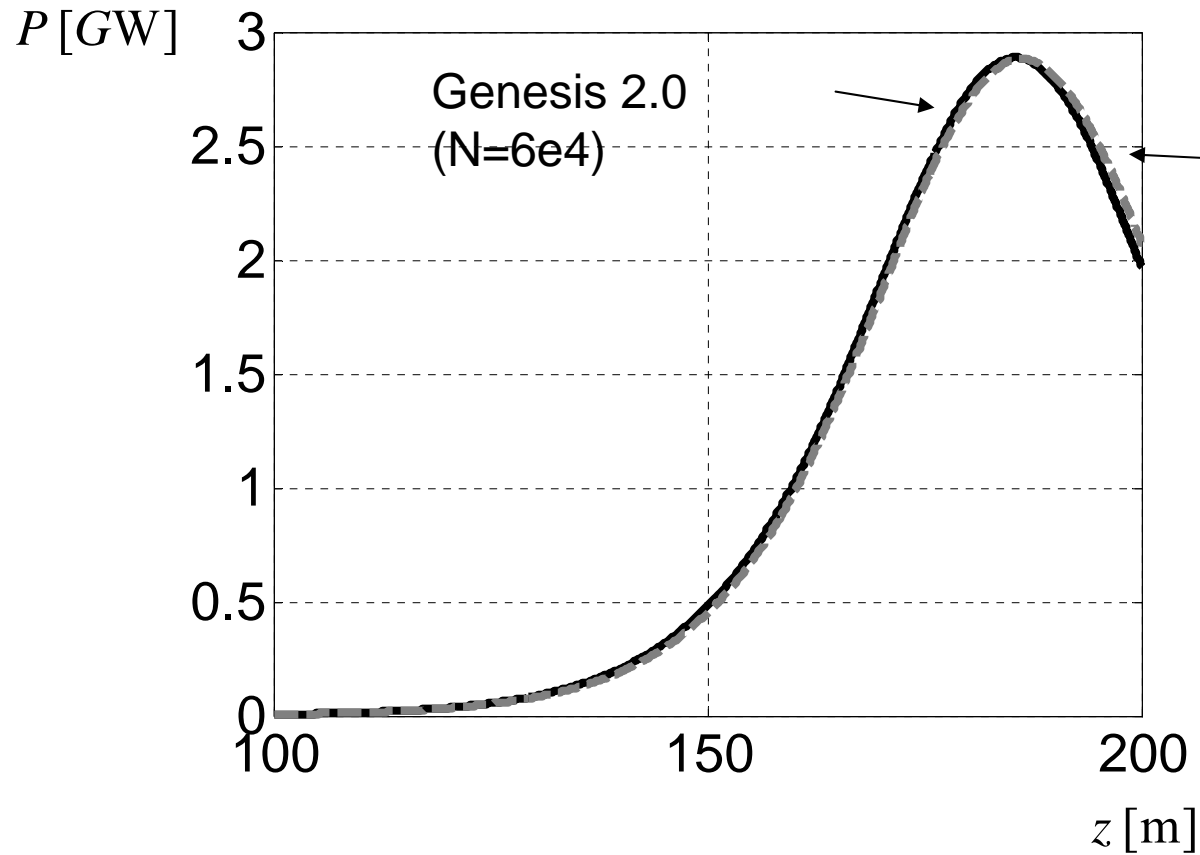
New Genesis 2.0 vs. ALICE with transverse motion

$$C = 0$$

$$P_0 = 4000 \text{ Watt}$$

$$\sigma_E = 2.5 \text{ MeV}$$

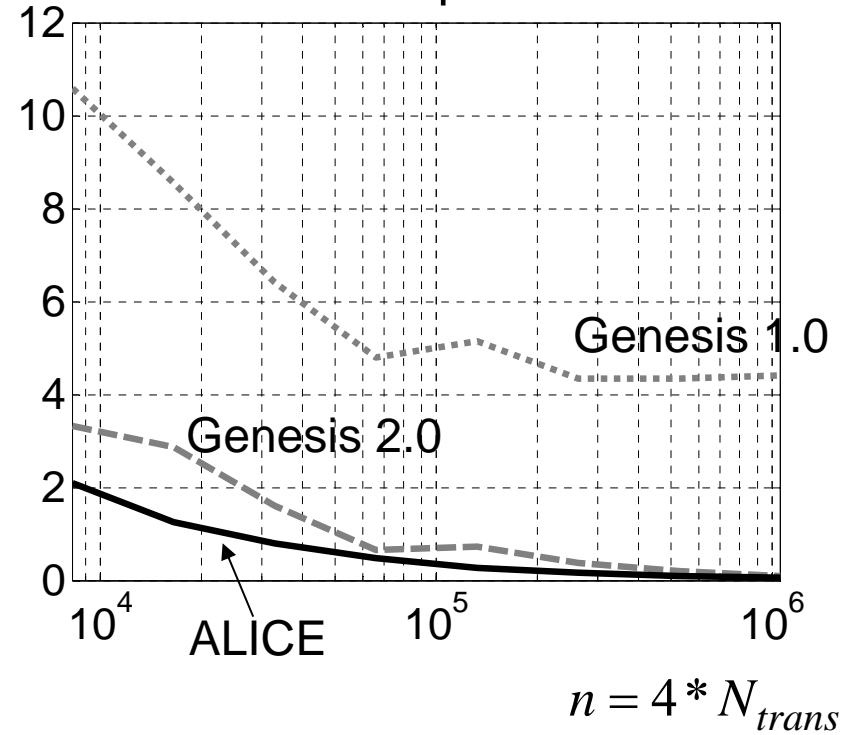
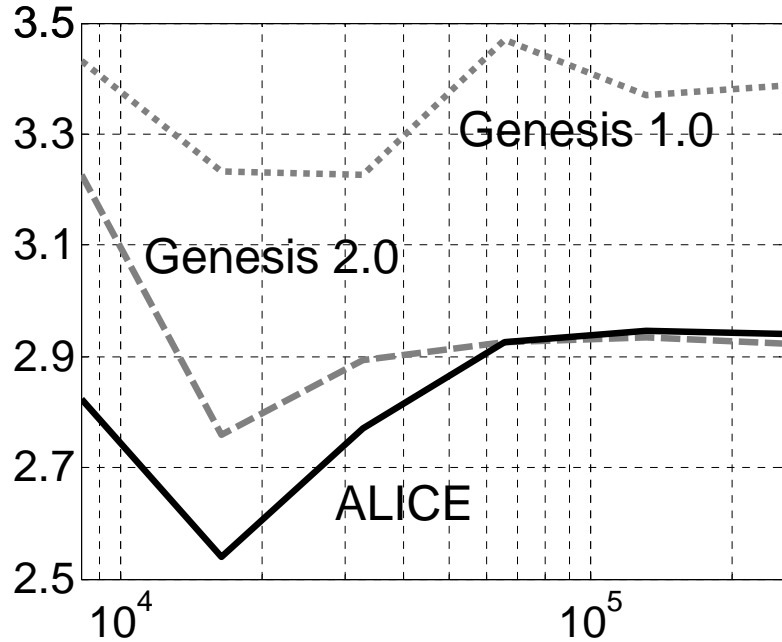
$$\varepsilon = 1.4 \text{ mm} \cdot \text{mrad}$$



Convergence

$$\delta = \frac{|\sigma_4 - \tilde{\sigma}_4|}{\sigma_4} 100\%$$

$P[GW]$ at saturation



$n = 4 * N_{trans}$

$n = 4 * N_{trans}$

Genesis 1.0:

Hammersley and Box-Mueller

Genesis 2.0:

Hammersley and the inverse error function

ALICE:

Sobol and the inverse error function

$\varepsilon = 1.4 \text{ mm} * \text{mrad}$

$C = 0$

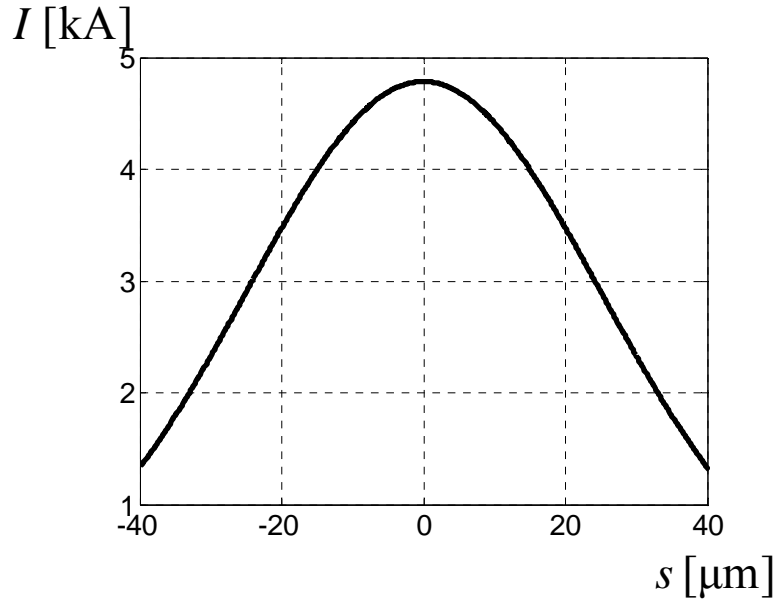
$I = 5 \text{ KA}$

$\sigma_E = 2.5 \text{ MeV}$

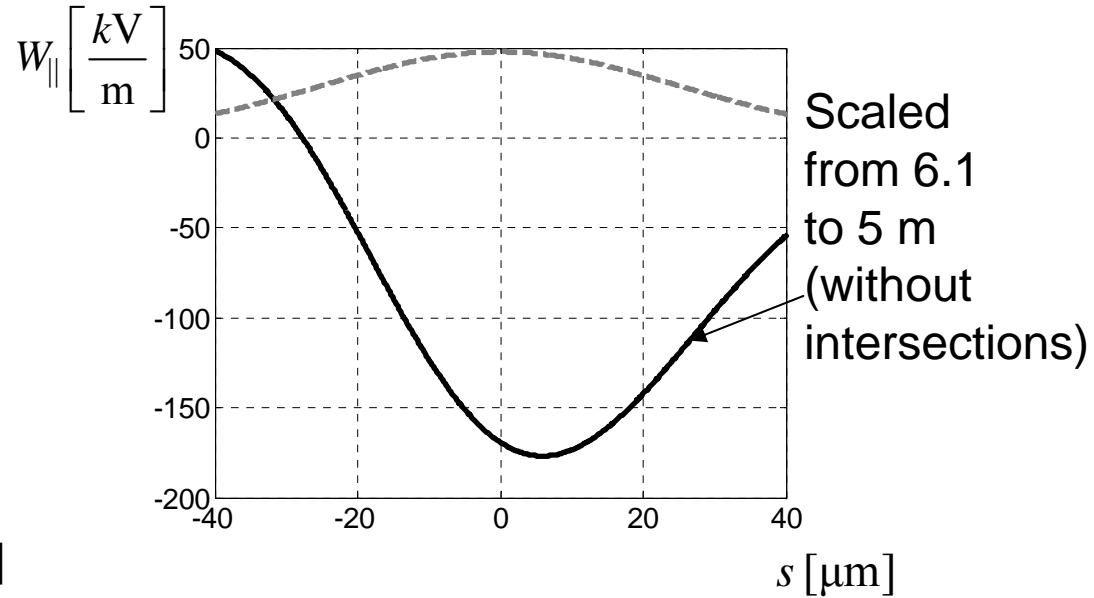
$\lambda_s = 0.1 \text{ nm}$

$N_\lambda \sim 10\ 400$

Matched Gaussian Beam Parameters

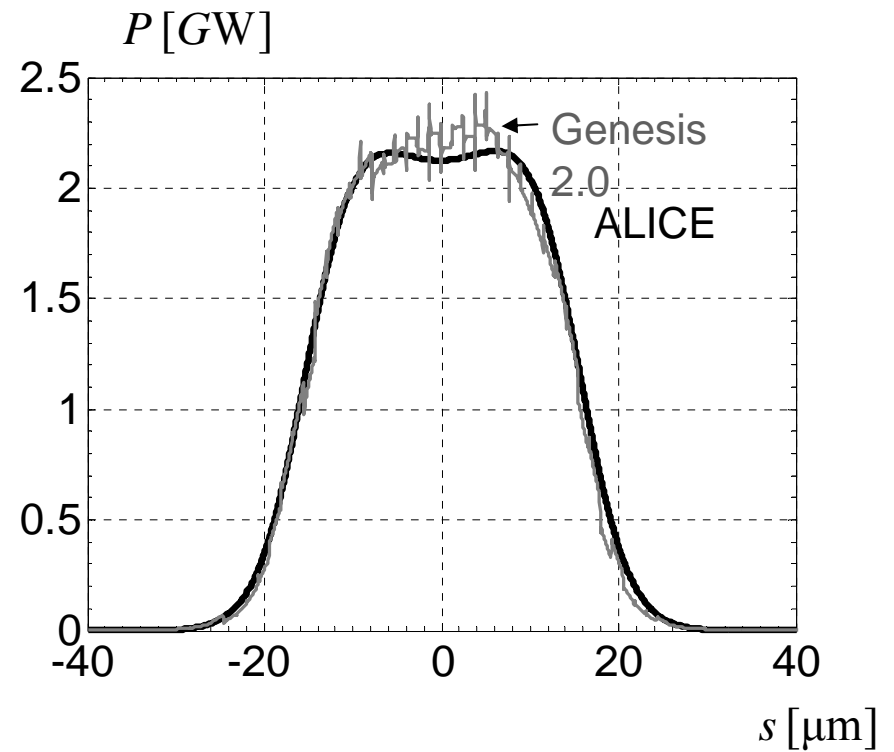
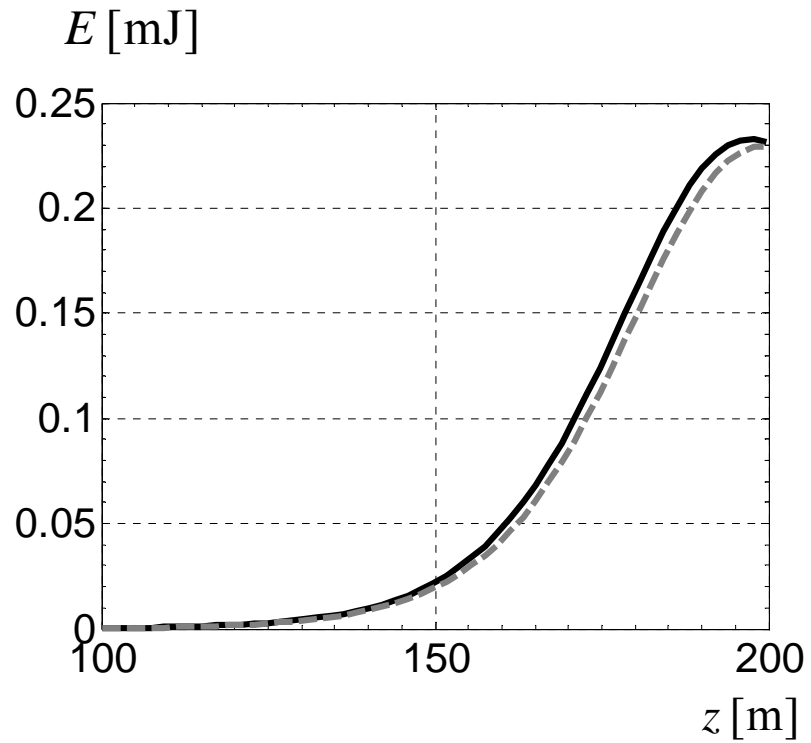


$$\begin{aligned}\varepsilon_x = \varepsilon_y &= 1.4 \text{ mm} \times \text{mrad} \\ \gamma &= 34246.667 \\ \sigma_E &= 2.5 \text{ MeV}\end{aligned}$$

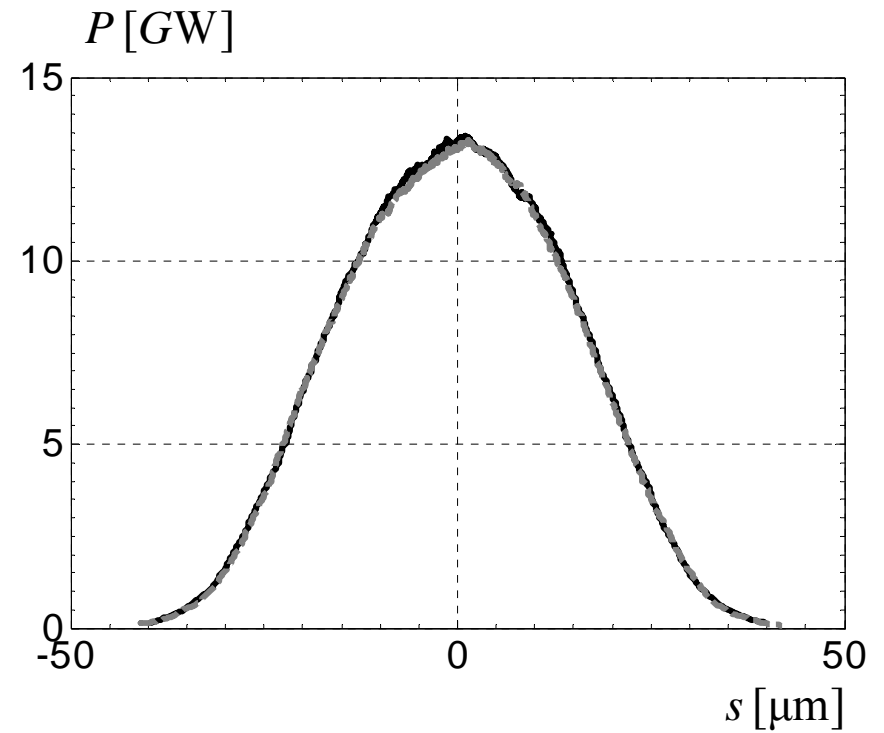
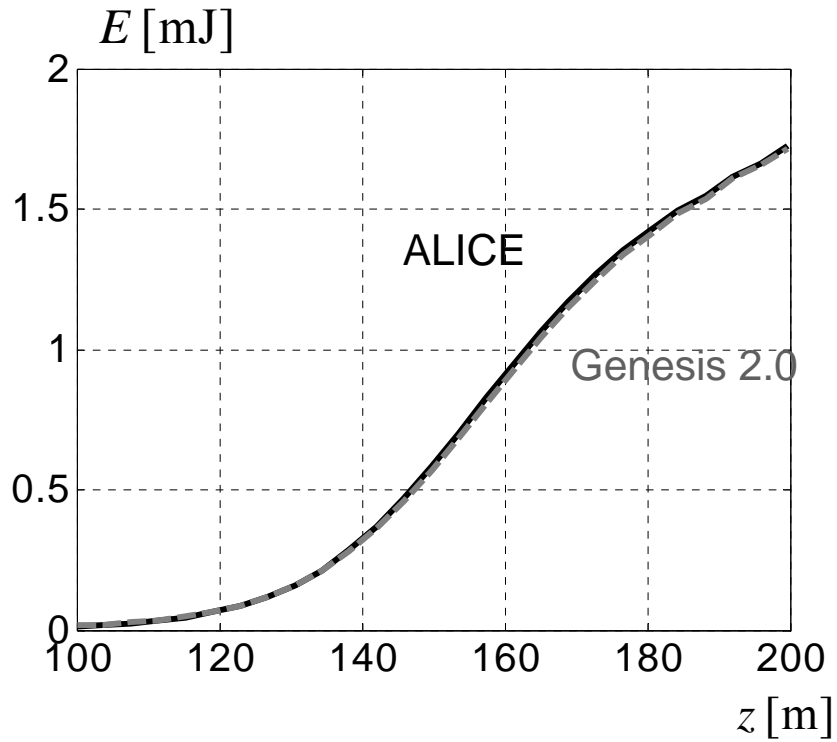


$$\begin{aligned}\beta_y &= 33 \text{ m} & \alpha_x = \alpha_y &= 0 \\ \beta_x &= 47 \text{ m} & \langle x \rangle = \langle y \rangle &= 0 \\ & & \langle x' \rangle = \langle y' \rangle &= 0\end{aligned}$$

Amplifier with matched Gaussian beam

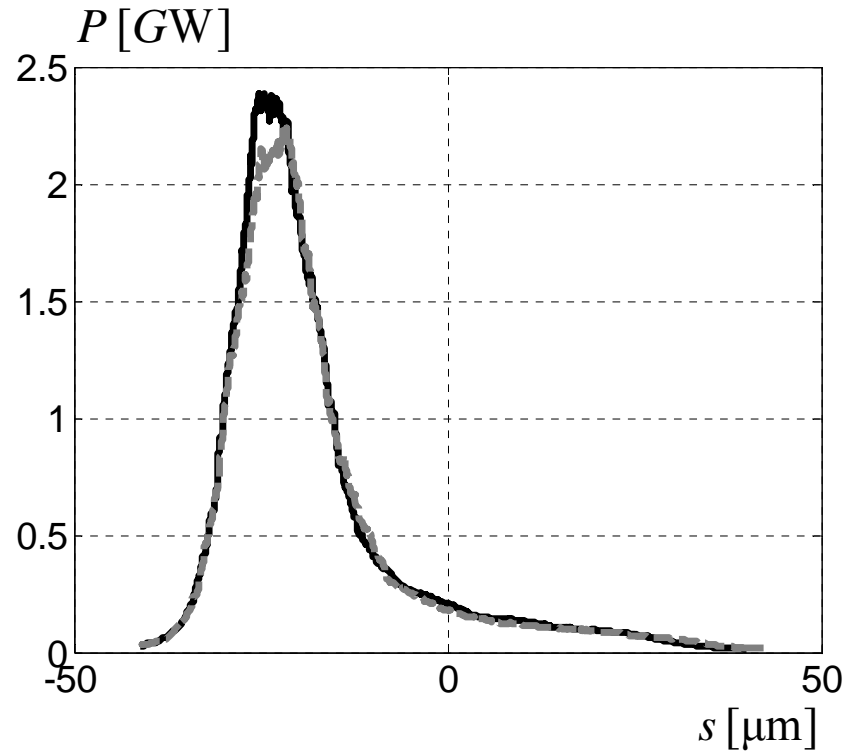
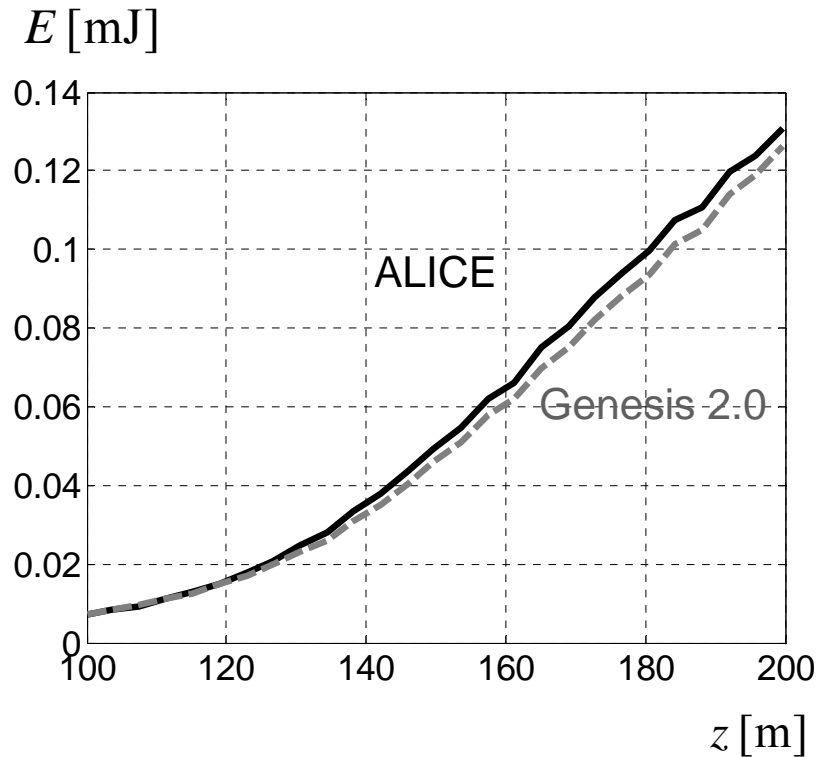


SASE with matched Gaussian beam



Averaged in space through 1500*56 slices

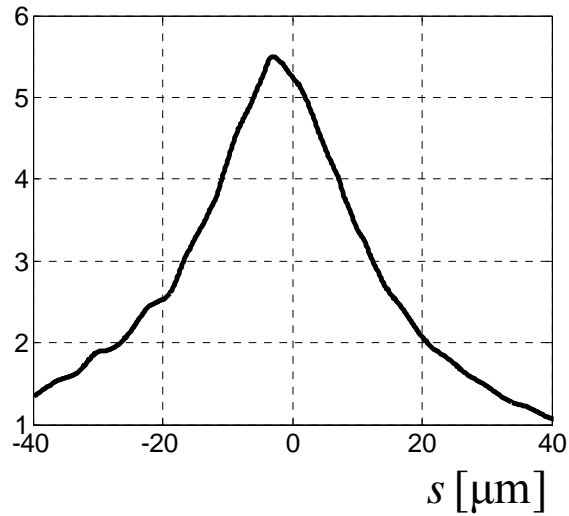
SASE with matched Gaussian beam and wake



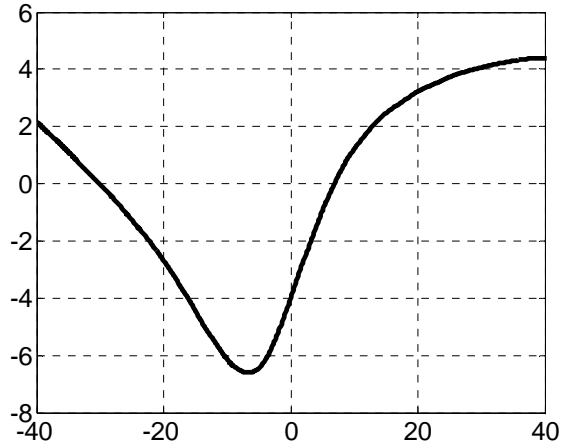
Averaged in space through 500*56 slices

Beam parameters (S2E)

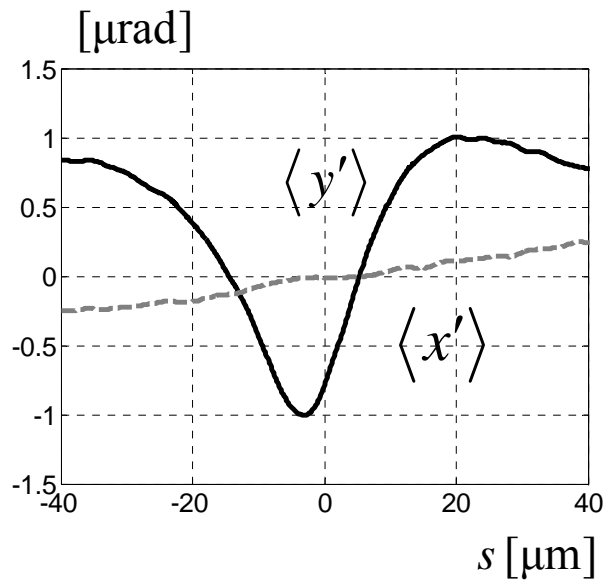
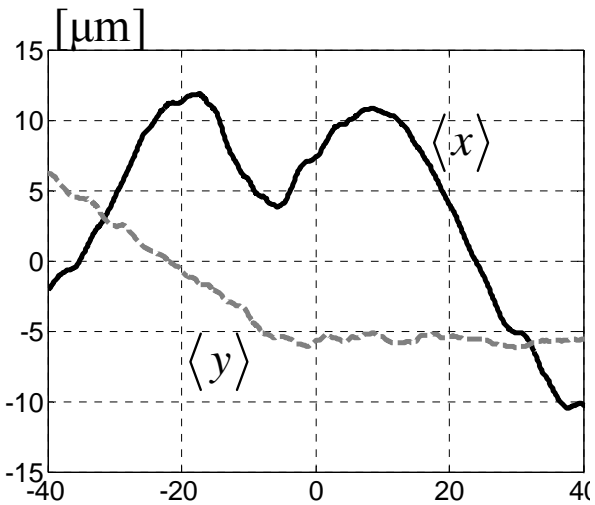
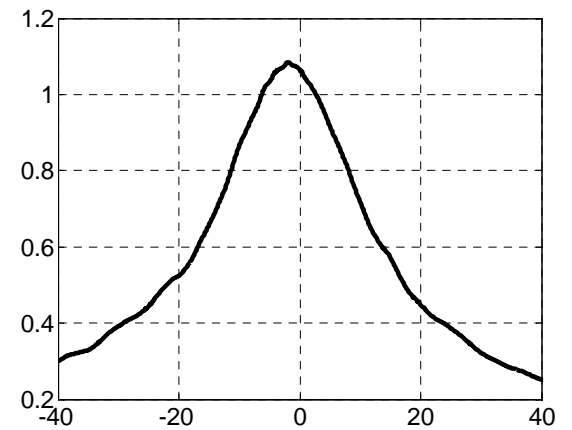
I [kA]



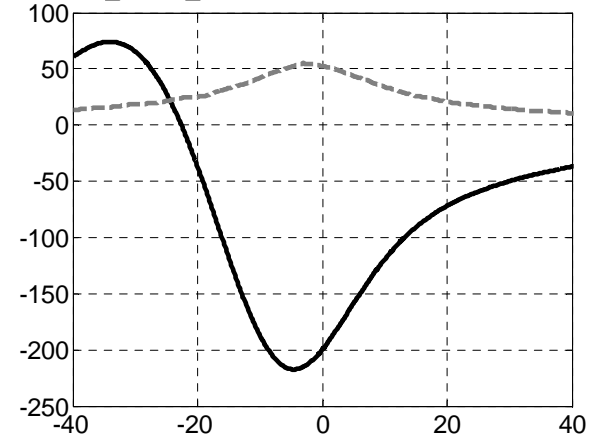
$\gamma - \langle \gamma \rangle \quad \langle \gamma \rangle = 34206.8$



σ_E [MeV]

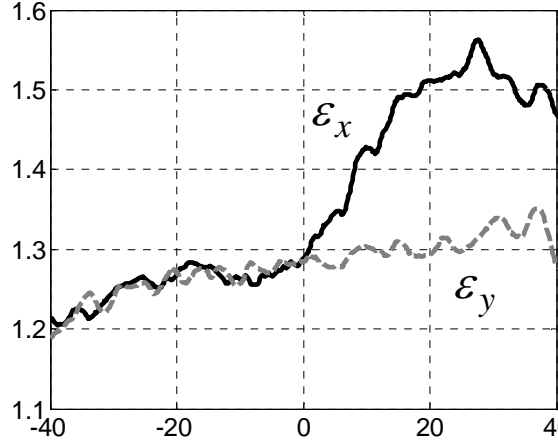


$W_{\parallel} \left[\frac{\text{kV}}{\text{m}} \right]$

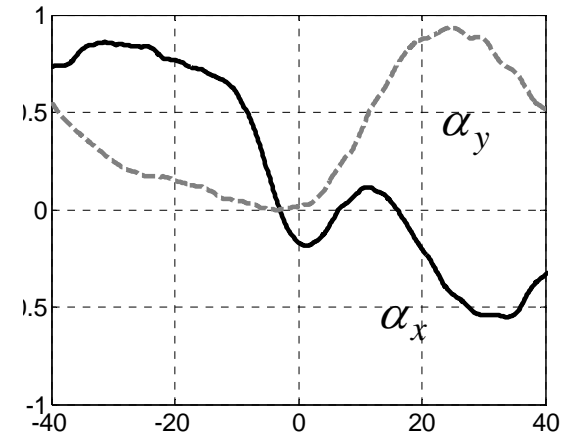
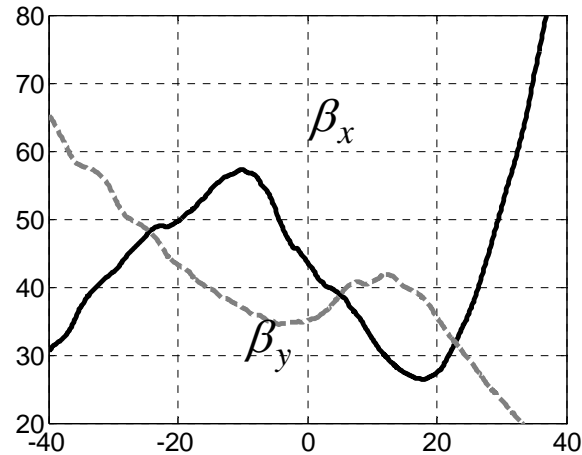


Beam parameters (S2E)

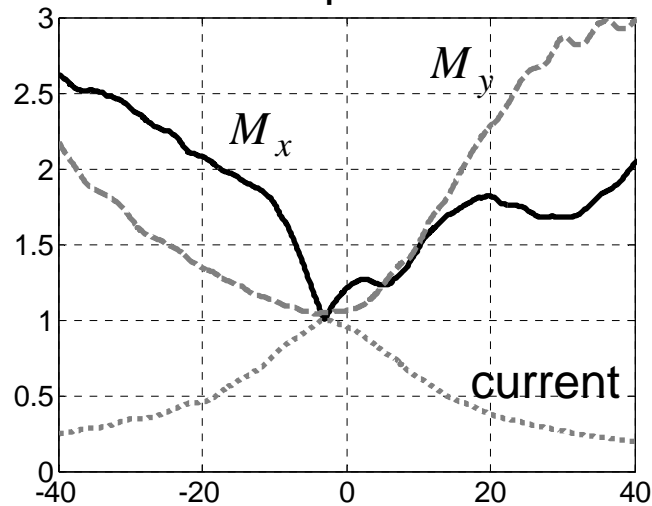
[mm×mrad]



[m]



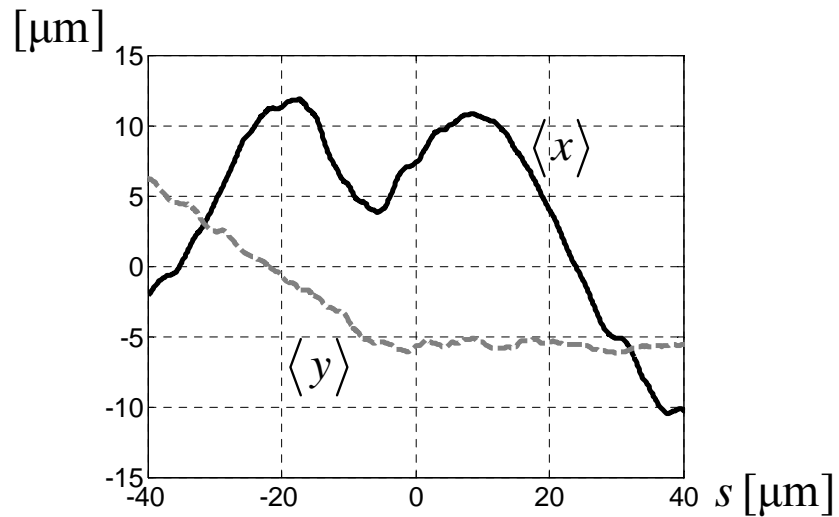
Mismatch parameters



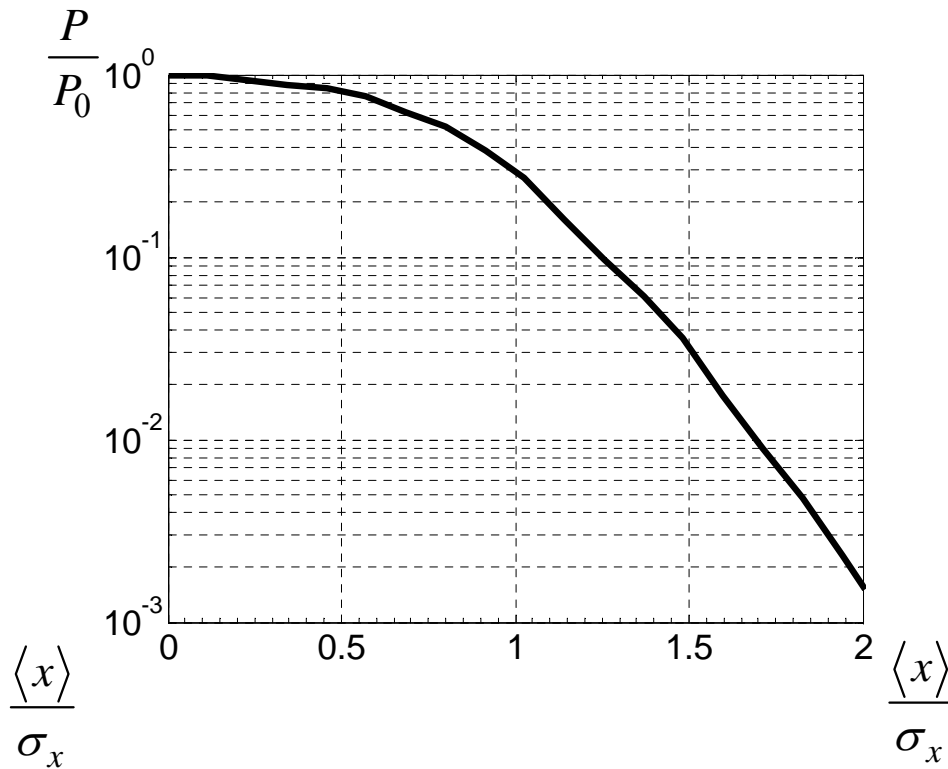
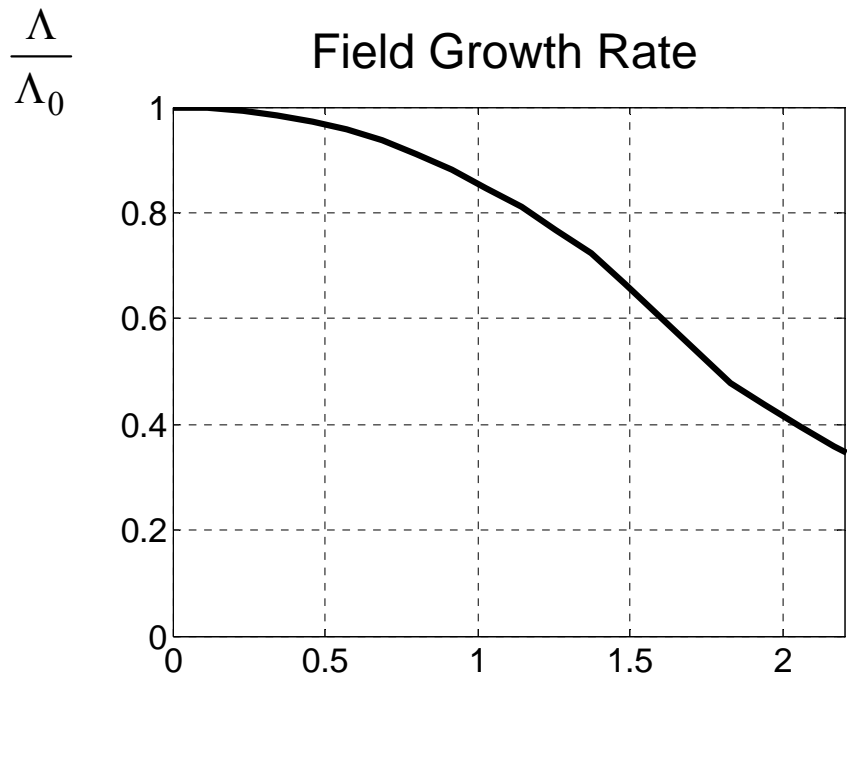
$$\beta_x^0 = 47$$

$$\beta_y^0 = 33$$

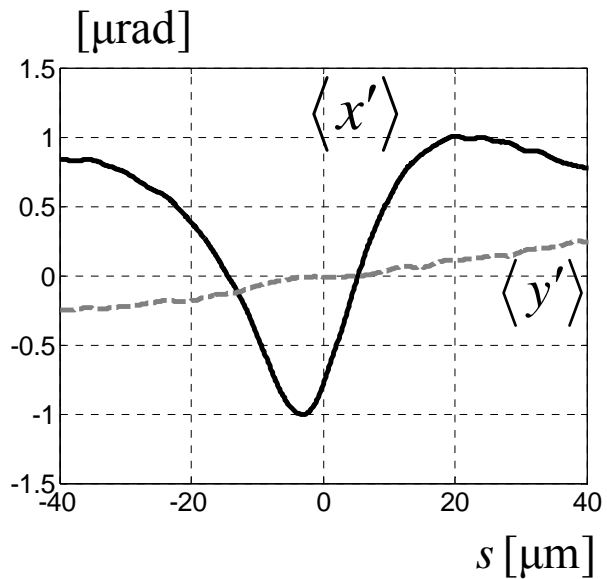
Beam parameters (S2E)



$$\sigma_x = 43.8 \mu\text{m}$$
$$P_0 = 14.4 \text{ GW}$$
$$\Lambda_0 = 0.055$$



Beam parameters (S2E)

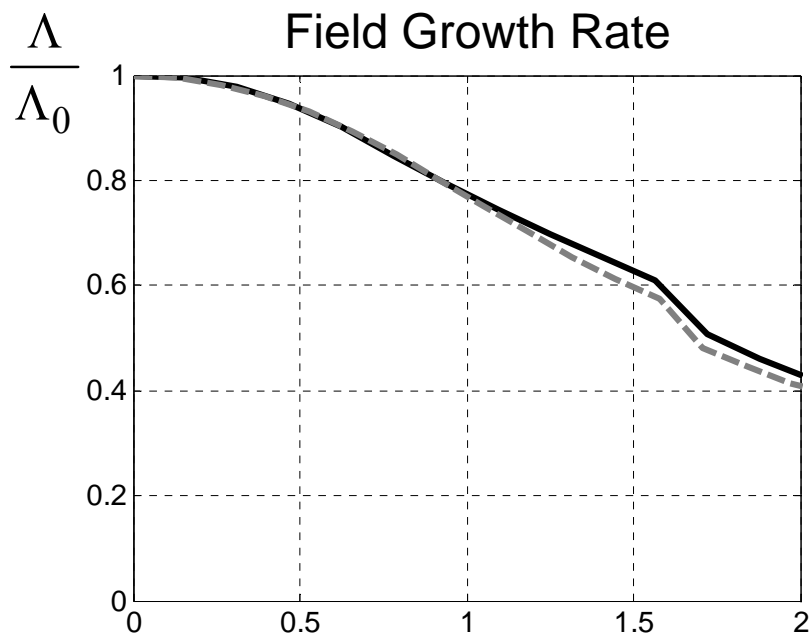


$$\sigma_{x'} = 0.93 \mu\text{rad}$$

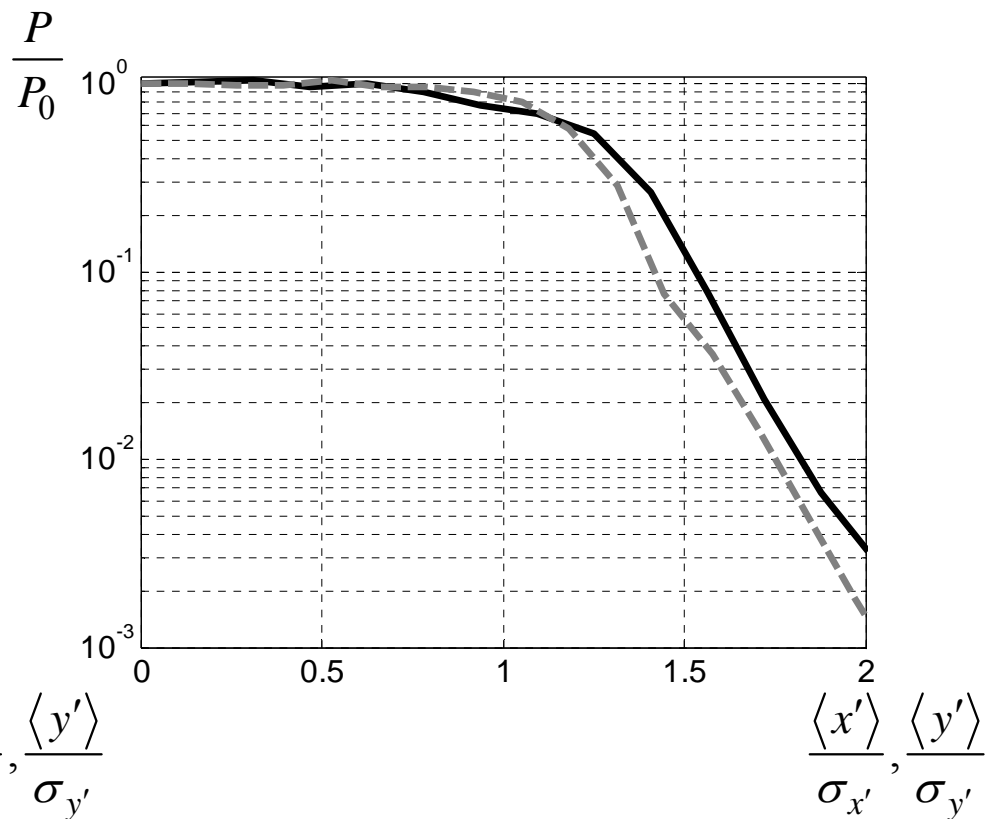
$$\sigma_{y'} = 1.1 \mu\text{rad}$$

$$P_0 = 14.4 \text{ GW}$$

$$\Lambda_0 = 0.055$$

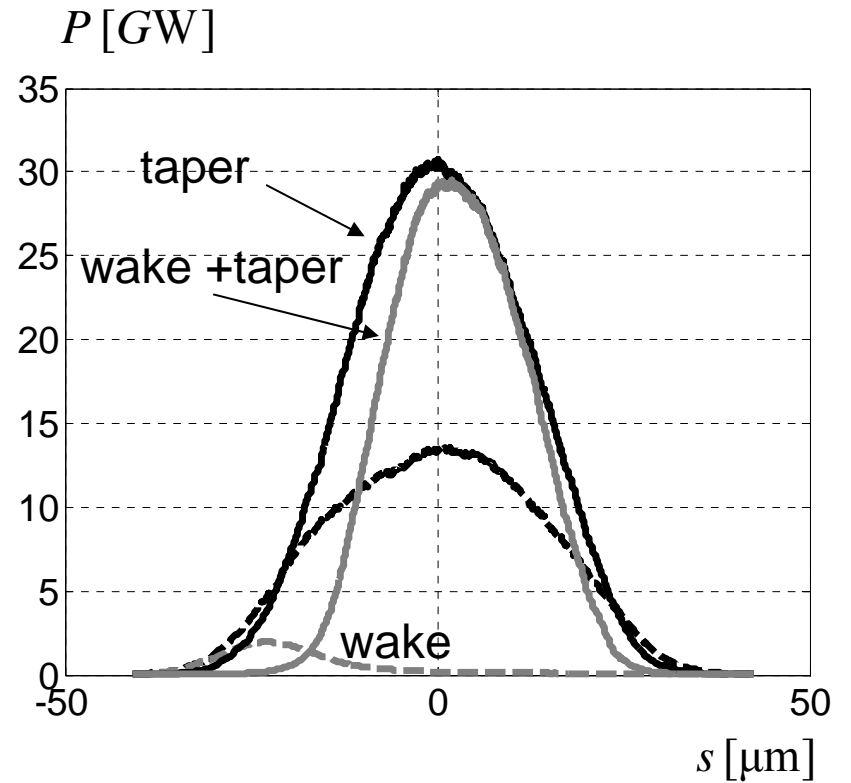
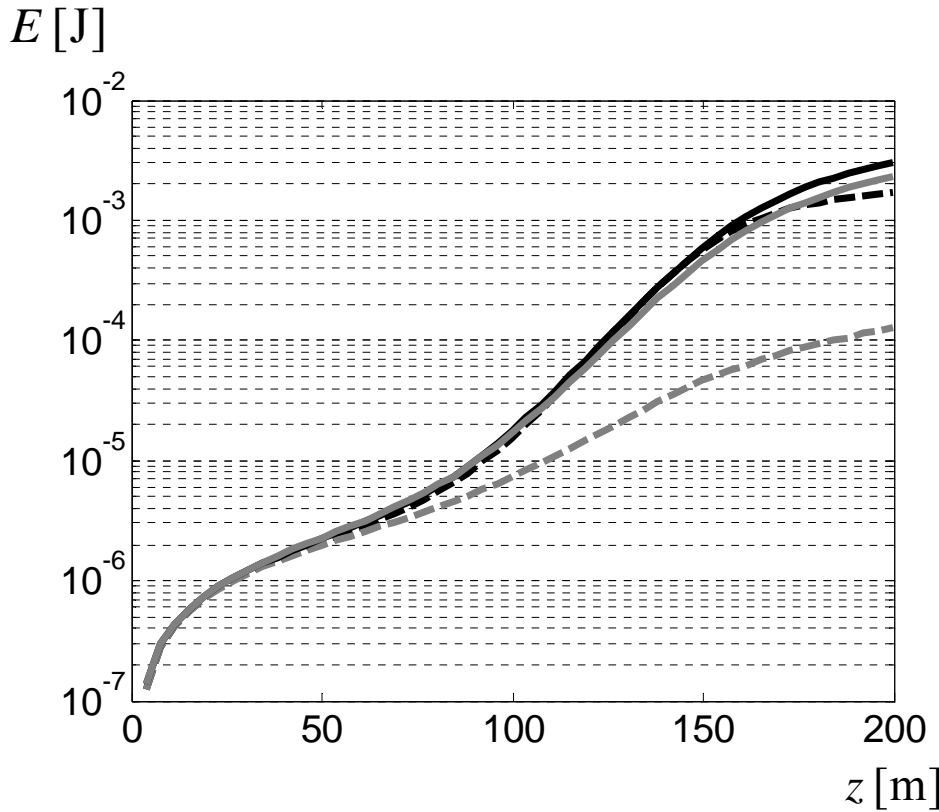


$$\frac{\langle x' \rangle}{\sigma_{x'}}, \frac{\langle y' \rangle}{\sigma_{y'}}$$



$$\frac{\langle x' \rangle}{\sigma_{x'}}, \frac{\langle y' \rangle}{\sigma_{y'}}$$

SASE with matched Gaussian beam

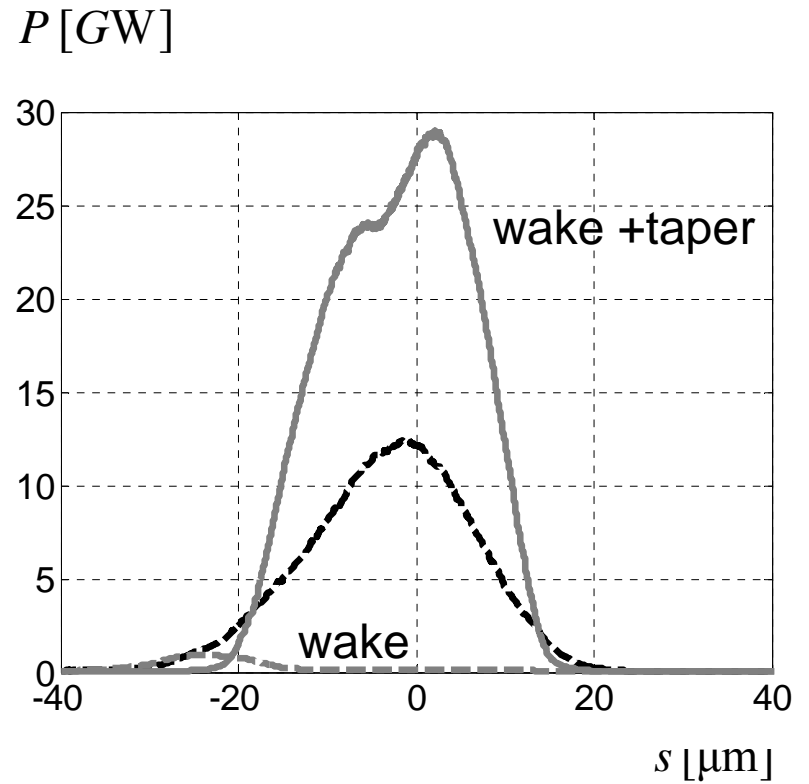
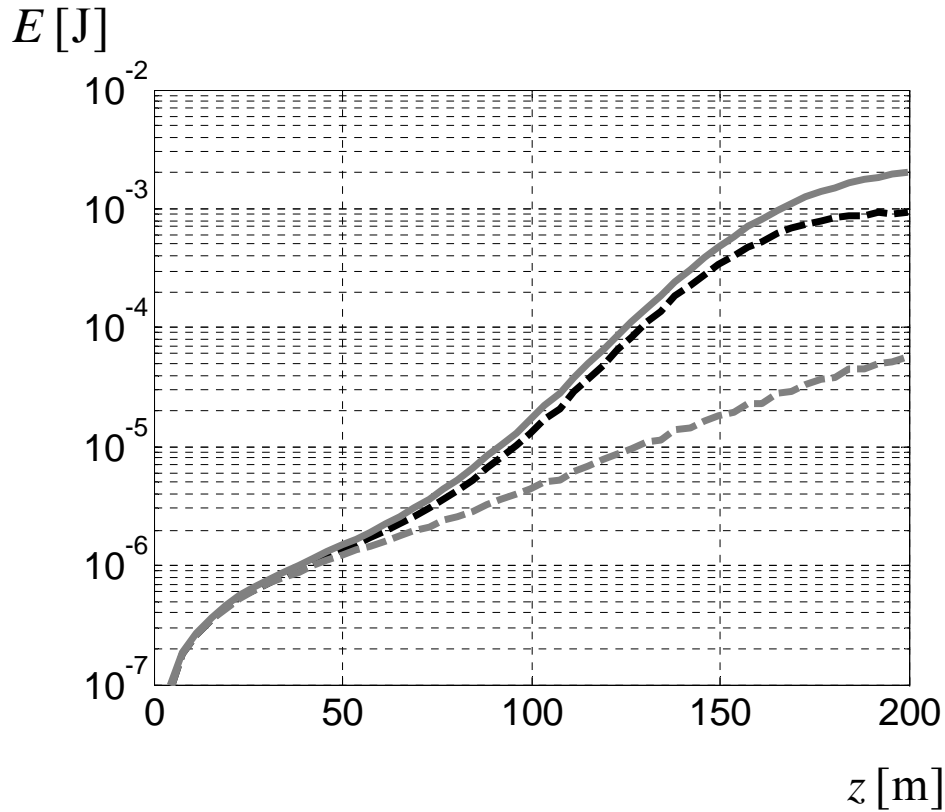


Averaged in space through 1000*56 slices

$$E_0 = 1.7 \text{ mJ}$$

	without wake, without taper	with taper	with wake	with wake, with taper
Energy, mJ	1.7	3.1	0.13	2.3
E/E_0	100%	180%	7.3%	136%

SASE with S2E beam



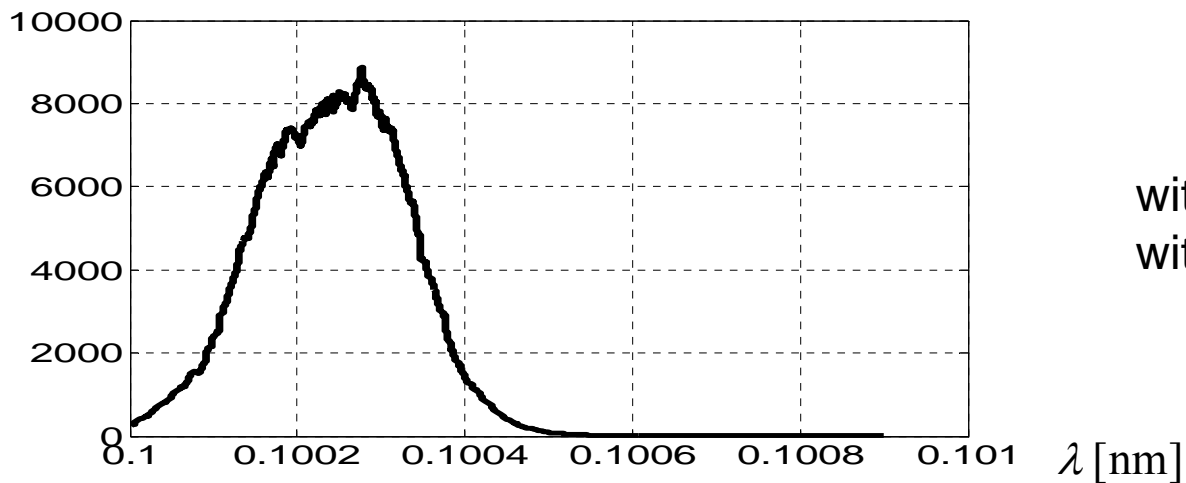
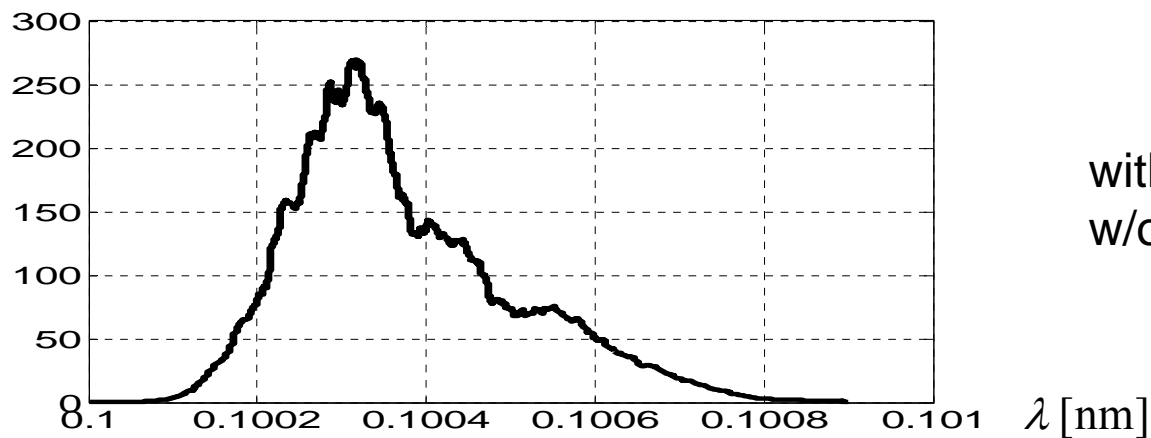
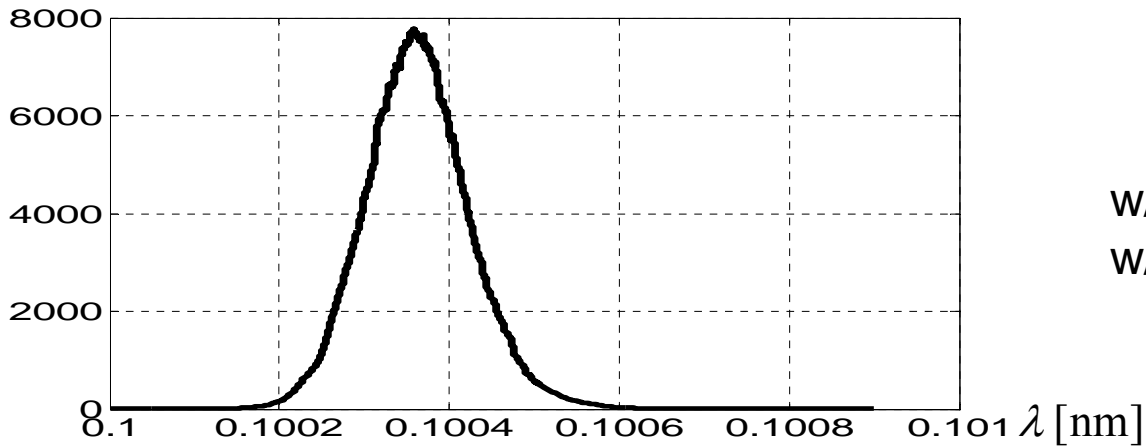
Averaged in space through 1000*56 slices

$E_0 = 0.93$ mJ

	without wake, without taper	with wake	with wake, with taper
energy, mJ	0.93	0.06	2
E/E_0	100%	6.1%	220%

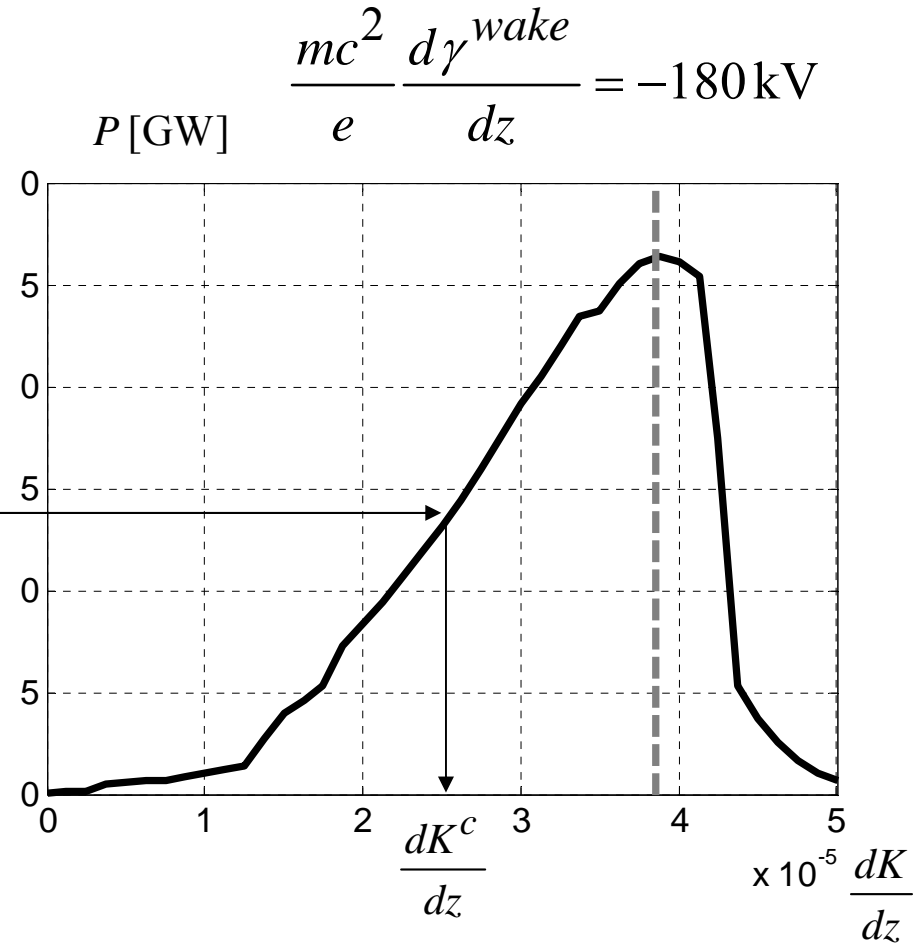
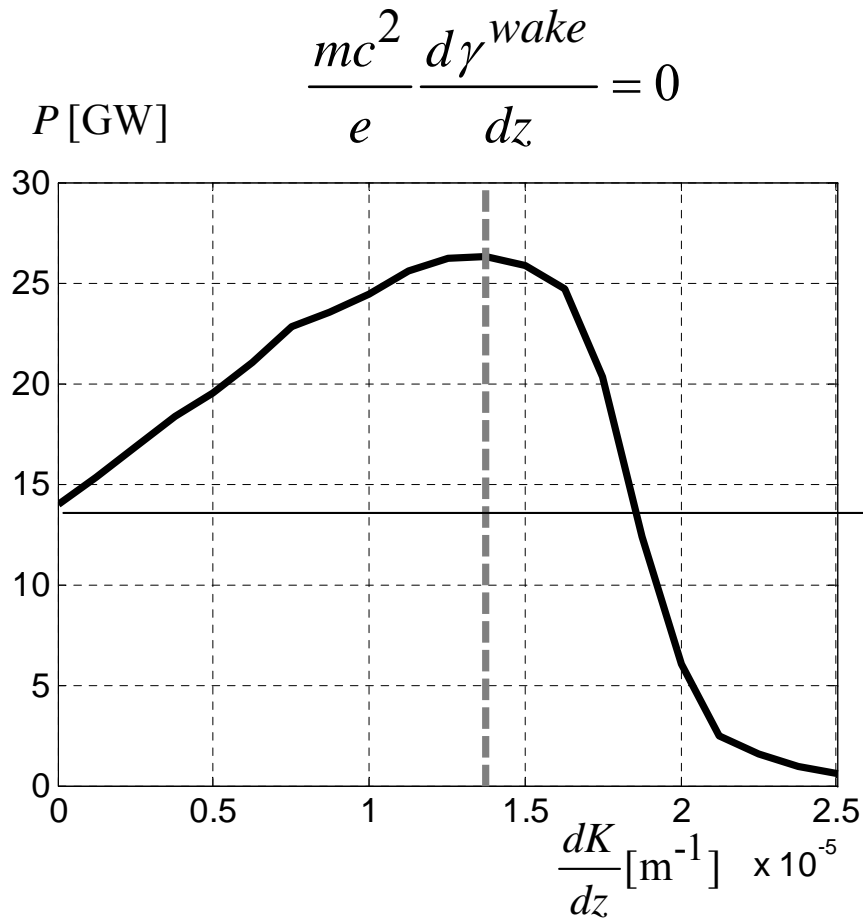
Spectrum
(S2E)

$P [a.u.]$



Optimal taper

$$\frac{\lambda_s}{\lambda_u} = \frac{1 + K_{av}^2}{2\gamma^2} \quad \frac{dK}{dz} = 2 \frac{\lambda_s}{\lambda_u} \frac{\gamma_0}{K_0} \frac{d\gamma}{dz} \quad \frac{dK^c}{dz} = -2.5 \cdot 10^{-5} \text{ m}^{-1}$$



Optimal taper

$$\frac{mc^2}{e} \frac{d\gamma^{wake}}{dz} = -180 \text{ kV}$$

$$\frac{dK}{dz} = -3.85 \cdot 10^{-5} \text{ m}^{-1}$$

$$B_u = 3.694 \exp\left(-5.068 \frac{g}{\lambda_u} + 1.52 \left(\frac{g}{\lambda_u}\right)^2\right)$$

$$\frac{\Delta K_{rms}}{K_{rms}} \approx -\frac{\Delta g}{g} \left(-5.068 \frac{g}{\lambda_u} + 3.04 \left(\frac{g}{\lambda_u}\right)^2\right)$$

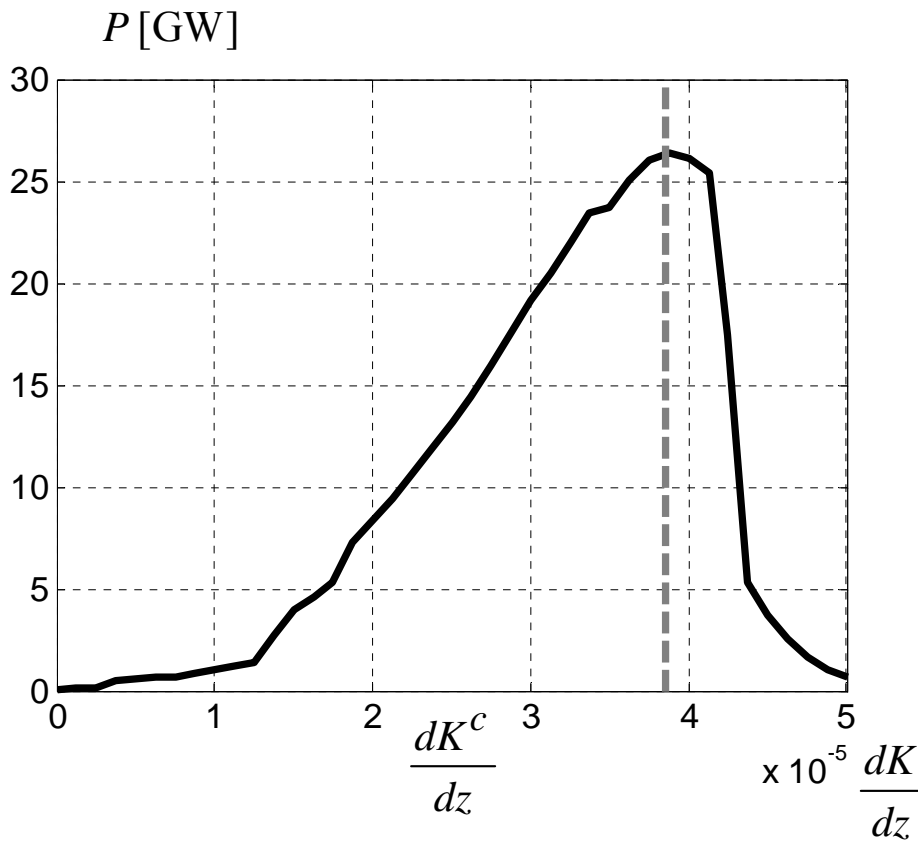
$$K_{rms} = 93.4 \lambda_u B_u / \sqrt{2}$$

$$\Delta g = -0.0124 \Delta K_{rms} / K_{rms}$$

$$\Delta g = -0.0124 \Delta K_{rms} / K_{rms} = 60 \cdot 10^{-6} [m]$$

$$\Delta g = -0.0124 \frac{\Delta K}{K} \approx -50 \mu m$$

$$\frac{dg}{dz} = -0.24 \frac{\mu m}{m} \approx -1.2 \frac{\mu m}{\text{module}}$$



Comparison with previous estimations

Undulator gap error
tolerances for wakefield
compensation in XFEL

Igor Zagorodnov

BDGM, DESY

27.03.06/08.05.06

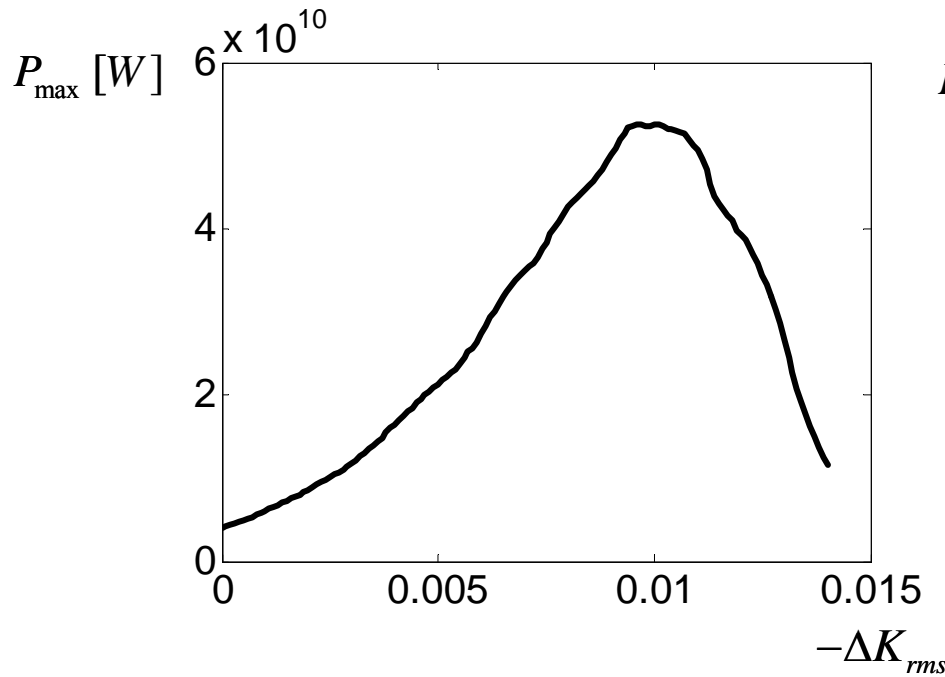
SASE (2005) $\varepsilon \approx 0.7 \text{ mm} \times \text{mrad}$

SASE 2 parameters

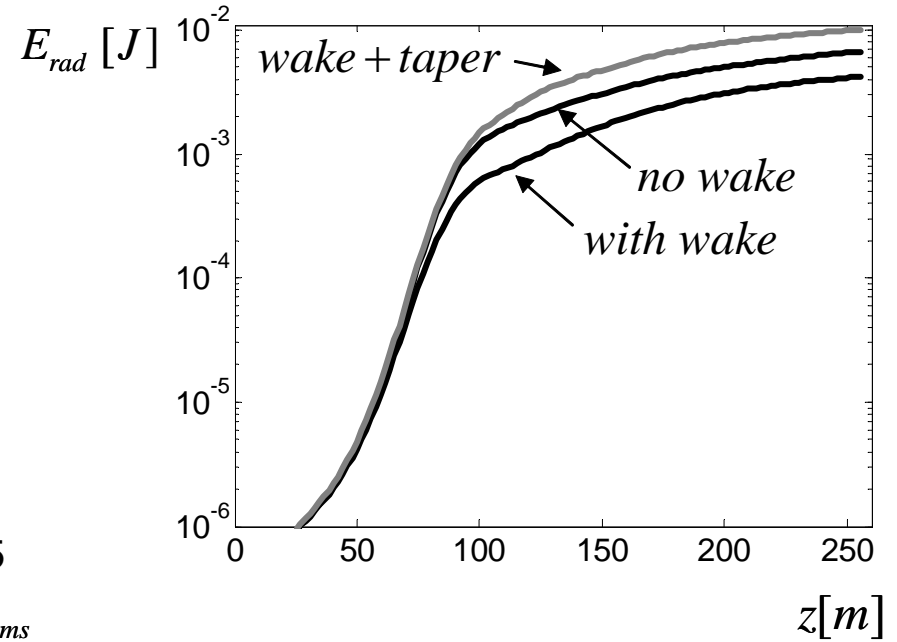
Parameter	symbol	unit	Value
radiation wavelength	λ	nm	0.1
Energy	E	GeV	17.5
energy spread	σ_E	MeV	1
undulator parameter	K_{rms}		1.97
Emittance	ε_n	mm*mrad	0.7
peak current	I	kA	5
average beta function	β	m	17.25
undulator section length	L_{sect}	m	5
intersection length	L_{inters}	m	1.1
total length	L_{total}	m	260
undulator period	λ_u	m	0.048

$$\rho = 7.1 \cdot 10^{-4}$$

Amplifier



SASE



The maximum power dependence on tapering (left) and the radiation power along the undulator (right)

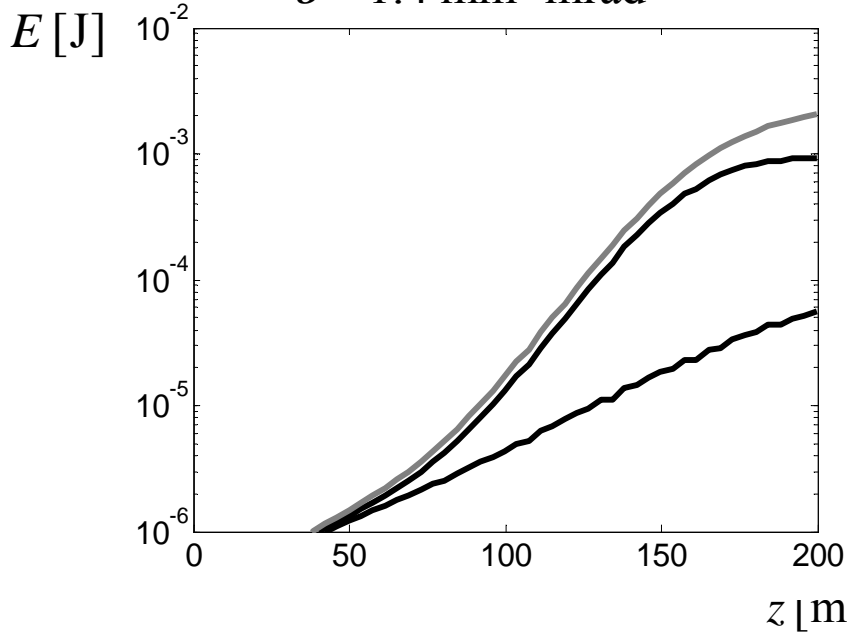
$$W_{sh} = 3\rho \frac{W_b}{N_c \sqrt{\pi \ln N_c}} = 11800 [W]$$

$$W_{\parallel} = 150 kV / nC / m$$

As one can see from this figure, in the absence of wakefields the radiation pulse energy is 2.3 mJ at 130m. It is reduced to 1.2 mJ by undulator wakefields. The optimal linear undulator tapering allows to avoid the degradation and to increase the radiation energy up to 3.5 mJ at 130m

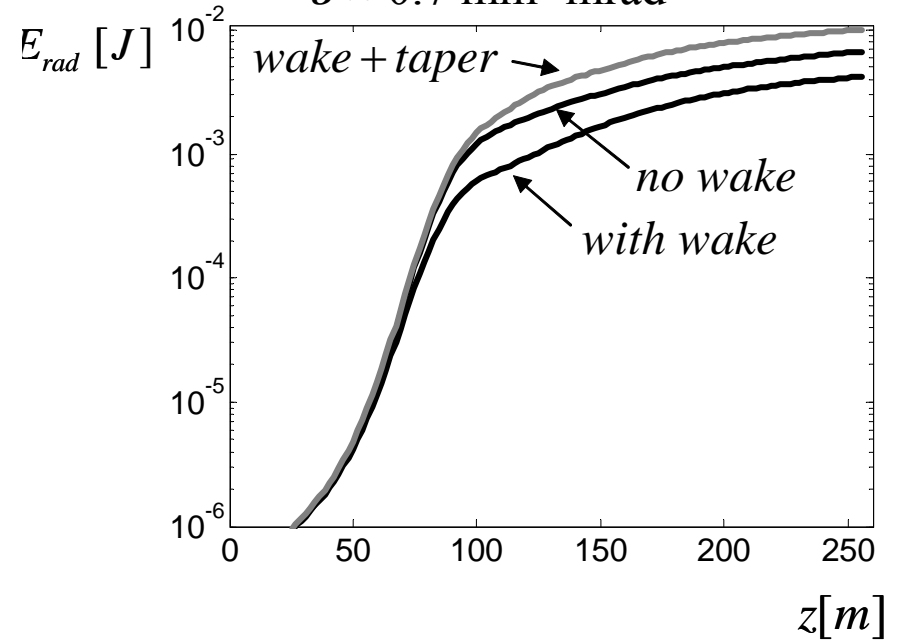
SASE (2008)

$\epsilon \approx 1.4 \text{ mm} \times \text{mrad}$



SASE (2005)

$\epsilon \approx 0.7 \text{ mm} \times \text{mrad}$

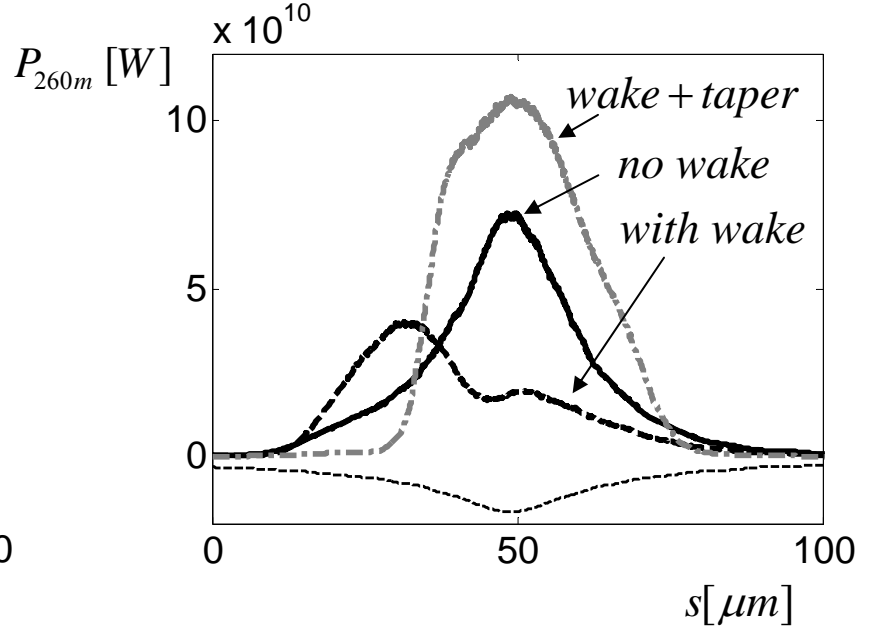
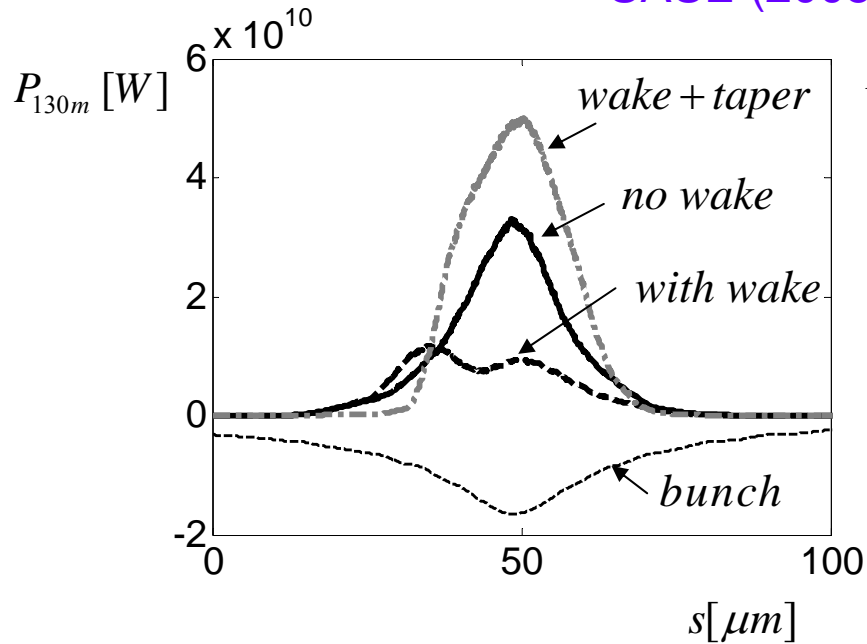


$E_0 = 0.93 \text{ mJ}$

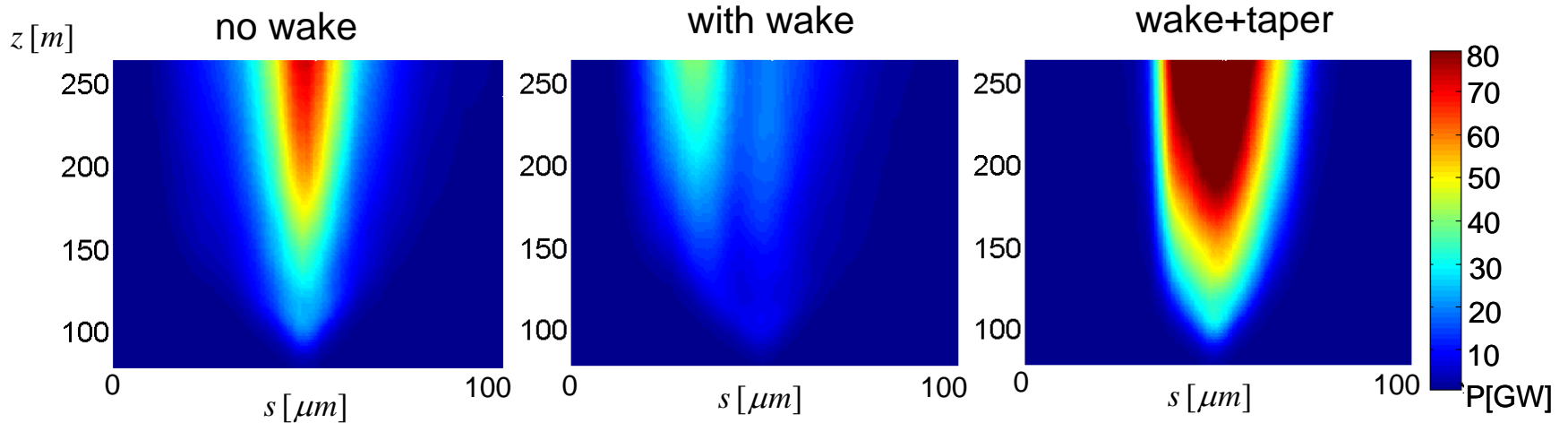
	without wake, without taper	with wake	with wake, with taper
energy,mJ	0.93	0.06	2
E/E_0	100%	6.1%	220%

As one can see from this figure, in the absence of wakefields the radiation pulse energy is 2.3 mJ at 130m. It is reduced to 1.2 mJ by undulator wakefields. The optimal linear undulator tapering allows to avoid the degradation and to increase the radiation energy up to 3.5 mJ at 130m

SASE (2005) $\varepsilon \approx 0.7 \text{ mm} \times \text{mrad}$



The radiation power in the middle (left) and at the end of the undulator (right)



SASE (2005) $\varepsilon \approx 0.7 \text{ mm} \times \text{mrad}$

$$B_u = 3.694 \exp \left(-5.068 \frac{g}{\lambda_u} + 1.52 \left(\frac{g}{\lambda_u} \right)^2 \right)$$

$$\frac{\Delta K_{rms}}{K_{rms}} \approx -\frac{\Delta g}{g} \left(-5.068 \frac{g}{\lambda_u} + 3.04 \left(\frac{g}{\lambda_u} \right)^2 \right)$$

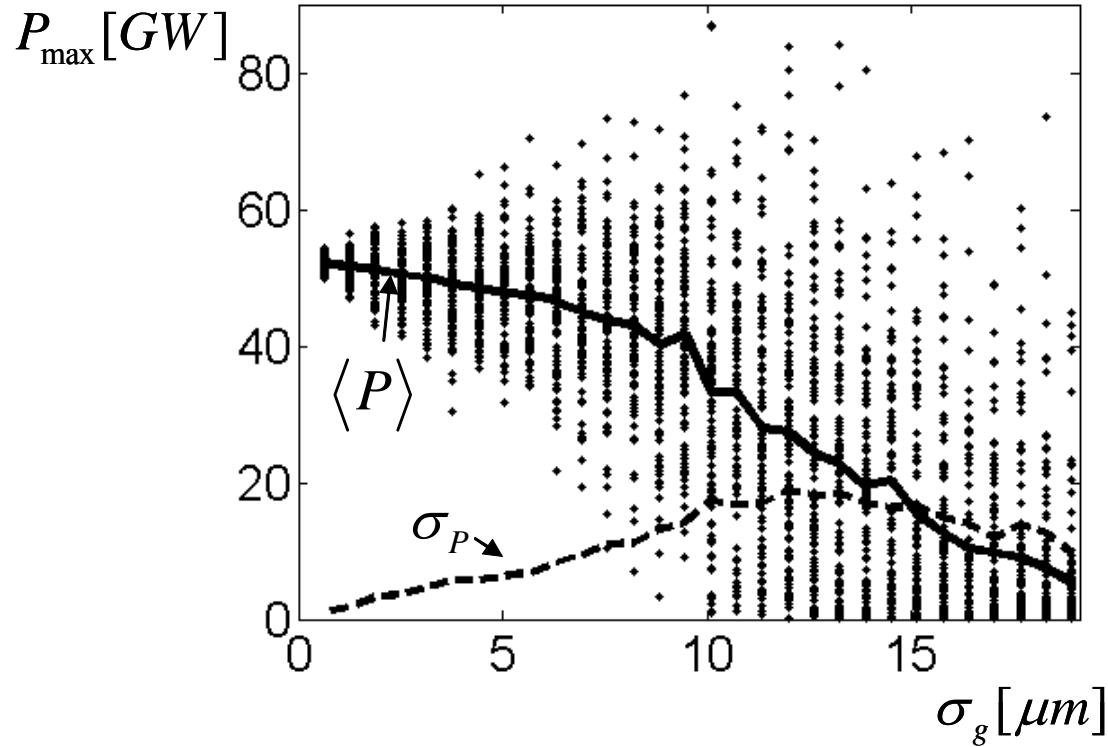
$$K_{rms} = 93.4 \lambda_u B_u / \sqrt{2}$$

$$\Delta g = -0.0124 \Delta K_{rms} / K_{rms}$$

Optimal taper

$$\Delta g = -0.0124 \Delta K_{rms} / K_{rms} = 60 \cdot 10^{-6} [m]$$

Steady-state

SASE (2005) $\varepsilon \approx 0.7 \text{ mm} \times \text{mrad}$ 

$$f(\delta g) = \frac{1}{\sqrt{2\pi}\sigma_g} \exp\left(-\frac{\delta g^2}{2\sigma_g^2}\right)$$

Impact of statistical errors of undulator gap on power gain.

$$\frac{P_0 - \langle P \rangle}{P_0} 100\% \approx 20\% \quad \text{for } \sigma_g = 10 \mu\text{m}$$

$$\frac{P_0 - [\langle P \rangle - 3\sigma_p]}{P_0} 100\% \approx 20\% \quad \text{for } \sigma_g = 2 \mu\text{m}$$

SASE (2005) $\varepsilon \approx 0.7 \text{ mm} \times \text{mrad}$

For 5 mkm gap error at position $z=130\text{m}$

Steady-state

$$\frac{\langle P_{\max}^{\sigma_g} \rangle}{P_{\max}^0} = 0.91$$

$$\sigma_P = 0.22$$

SASE

$$\frac{\langle E_{\max}^{\sigma_E} \rangle}{E_{\max}^0} = 0.88$$

$$\sigma_E = 0.16$$

