

# Wakefield effects in XFEL undulator

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## SASE 1-2 parameters

name	symbol	unit	value
energy	E	GeV	20
energy spread	$\Delta E$	MeV	2.5
emittance	$\epsilon_n$	$\pi$ mm-mrad	1.4
bunch charge	Q	nC	1
bunch length	$\sigma$	$\mu\text{m}$	25
peak current	$I_P$	kA	4.76
undulator period	$\lambda_u$	cm	4.8
undulator parameter	$a_u$		2.33
quadrupole length	$L_Q$	cm	20
quadrupole gradient	$G_Q$	T/m	19.5
section length	$L_u$	m	5
beta function (waist)	$\beta_x,$ $\beta_y,$	m	42.5 29.3

## Parameters (XFEL theory)

$$\lambda_s = \frac{\lambda_u}{2\gamma^2} (1 + a_u^2) = 0.10072 \text{ [nm]}$$

$$\sigma_{x,y} = \sqrt{\frac{\epsilon_n}{\gamma}} \beta_{x,y} = \begin{pmatrix} 39 \\ 32.4 \end{pmatrix} [\mu m]$$

$$\sigma_r = 0.5(\sigma_x + \sigma_y) = 35.7 [\mu m]$$

$$z_R = \frac{\pi w_0^2}{\lambda_s} = \frac{2\pi\sigma_r^2}{\lambda_s} = 79.5 [m]$$

## Parameters (XFEL theory)

Gain parameter

$$\Gamma_3 = \left[ \left( \frac{A_{JJ} \omega_s \theta_l}{c \gamma_l} \right)^2 \frac{I_P}{2 \gamma I_A} \right]^{1/2} = 0.48 [cm] \quad \Gamma_1 = \Gamma_3 B^{-1/3} = 0.14 [cm]$$

Efficiency parameter

$$\rho_3 = \frac{c \gamma_l^2 \Gamma_3}{\omega} = 18.5e-4 \quad \rho_1 = \frac{c \gamma_l^2 \Gamma_1}{\omega} = 5.5e-4$$

Diffraction parameter

$$B = \Gamma_3 \sigma_r^2 \frac{\omega_s}{c} = 38$$

Effective power of the input signal

$$P_{sh} = 3\rho_1 \frac{W_b}{N_c \sqrt{\pi \ln N_c}} = 7864 [W]$$

Electron beam power

$$W_b = \gamma I_P \frac{mc^2}{e} = 9.56e+13 [W]$$

Number of cooperating electrons

$$N_c = \frac{N_\lambda}{2\pi\rho_1} = 2.9e+6$$

Number of electrons per wavelength

$$N_\lambda = \frac{I_P}{ec} \lambda_s = 1.0033e+4$$

Gain length\*

$$L_g = L_{g0}(1+\delta) \approx 17.6 \text{ [m]}$$

Optimal beta-function

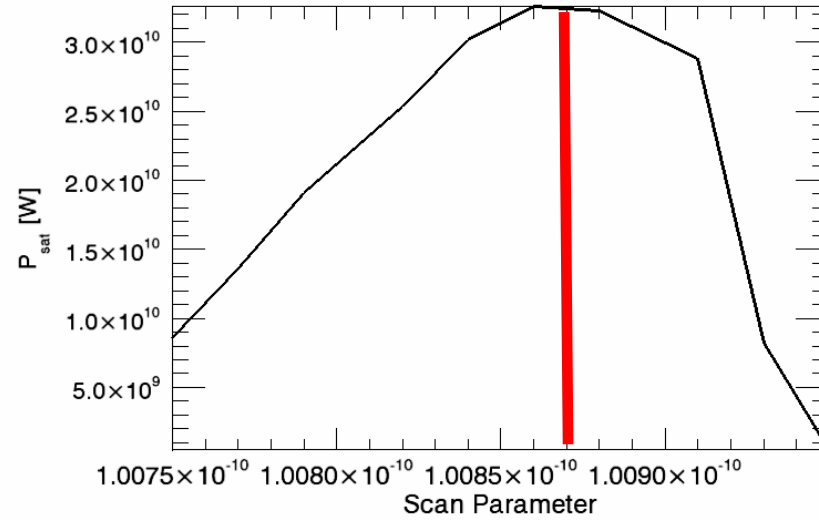
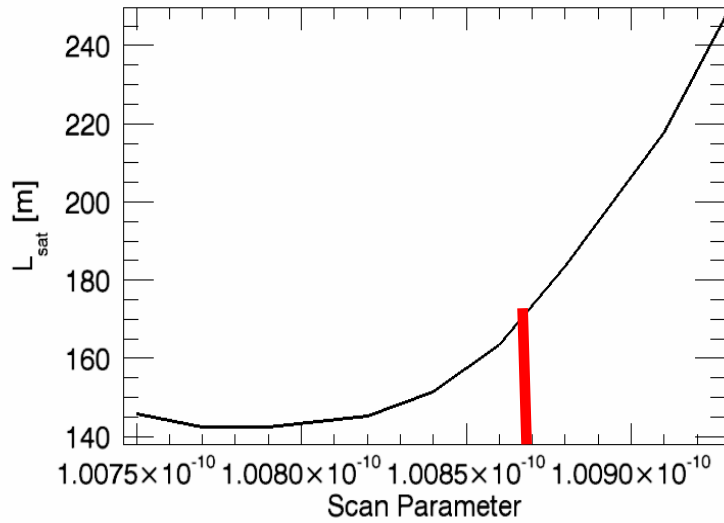
$$\beta_{opt} \approx 37 \text{ [m]}$$

Saturation length

$$L_{sat} \approx 10L_{g0} = 176 \text{ [m]}$$

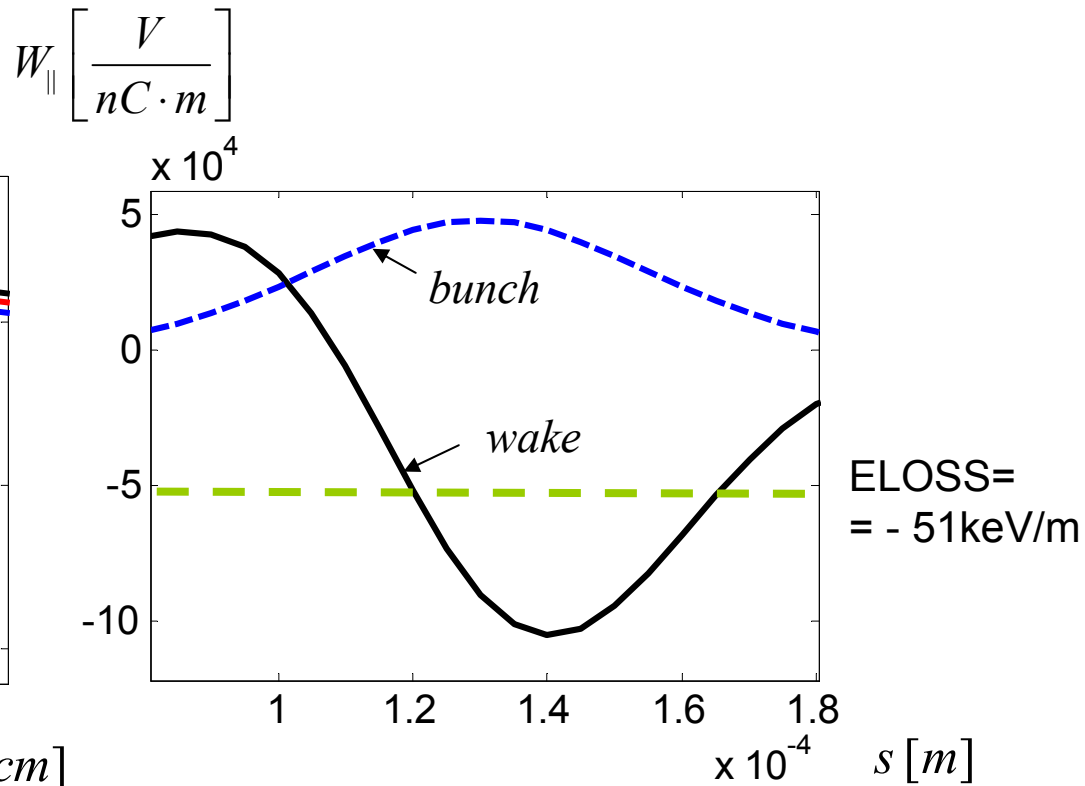
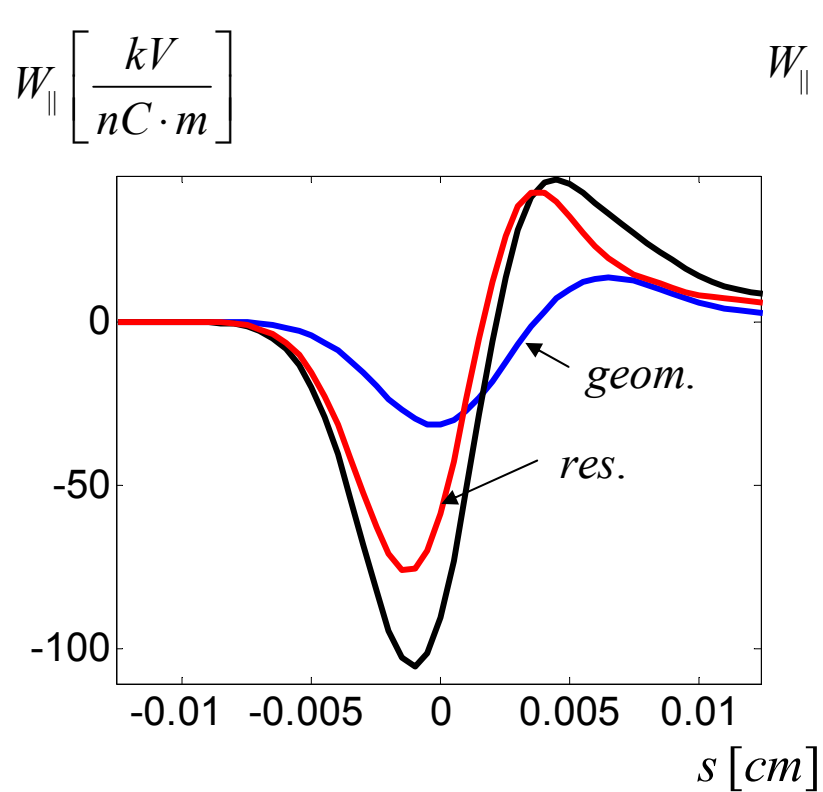
\* E.L.Saldin et al./Optics Communications 235 (2004) 415-420

## Genesis steady state simulation



$$\lambda_s^{num} = 0.10087 \text{ [nm]}$$

$$\lambda_s = \frac{\lambda_u}{2\gamma^2} (1 + a_u^2) = 0.10072 \text{ [nm]}$$



head

tail

tail

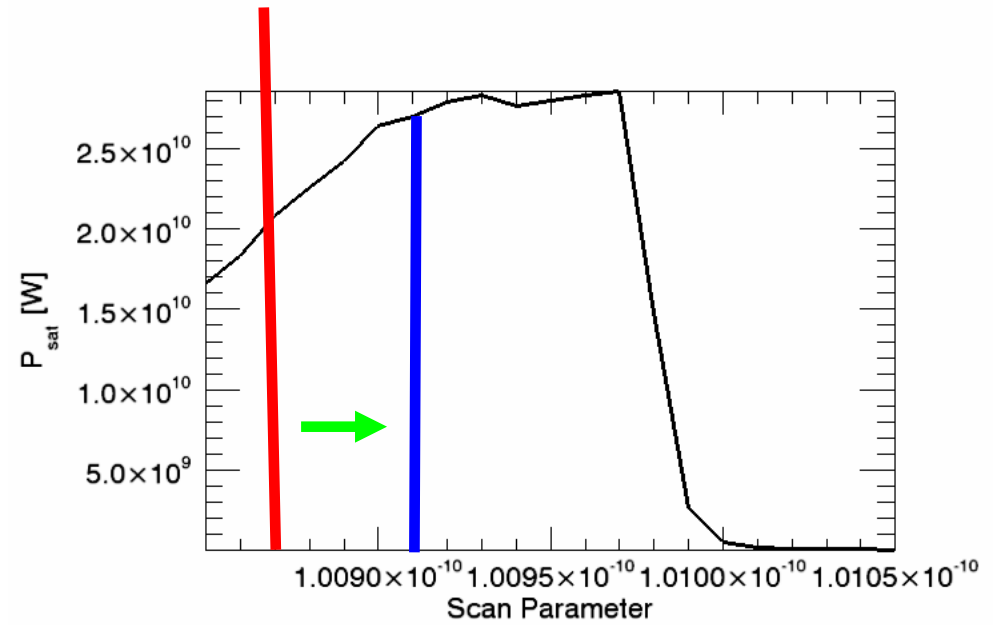
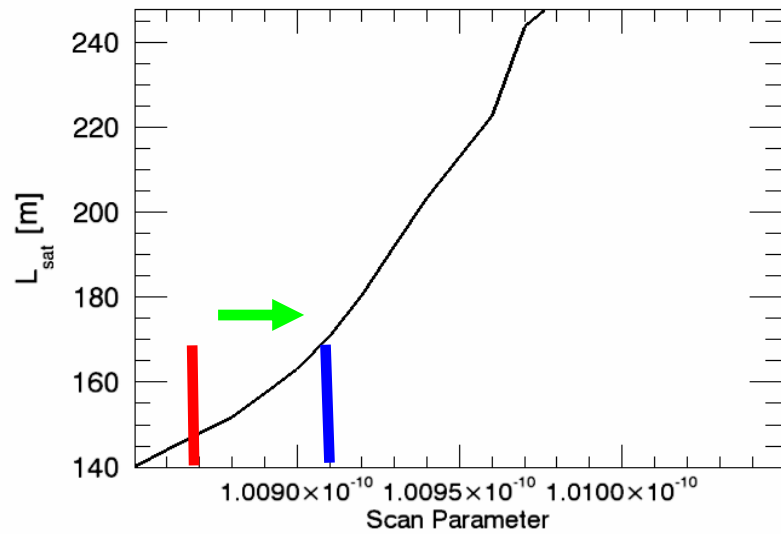
head

	Loss, kV/nC/m	Spread, kV/nC/m	Peak, kV/nC/m
geometrical	20	12	-32
resistive	31	39	-75
<b>total</b>	<b>51</b>	49	-105



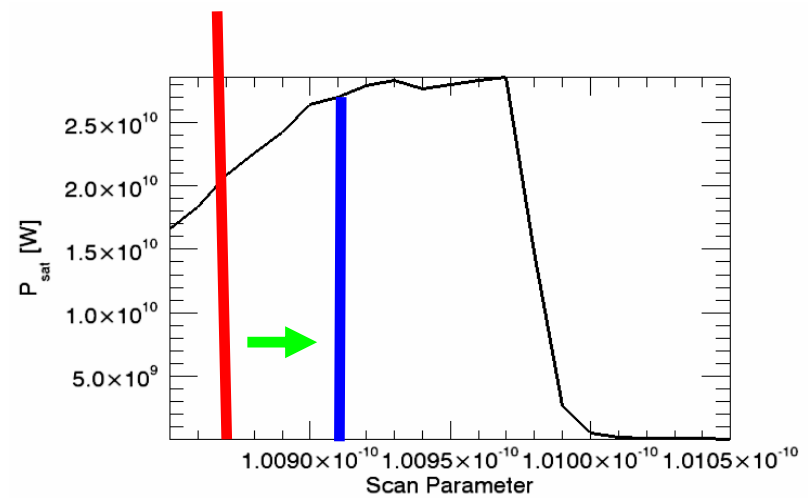
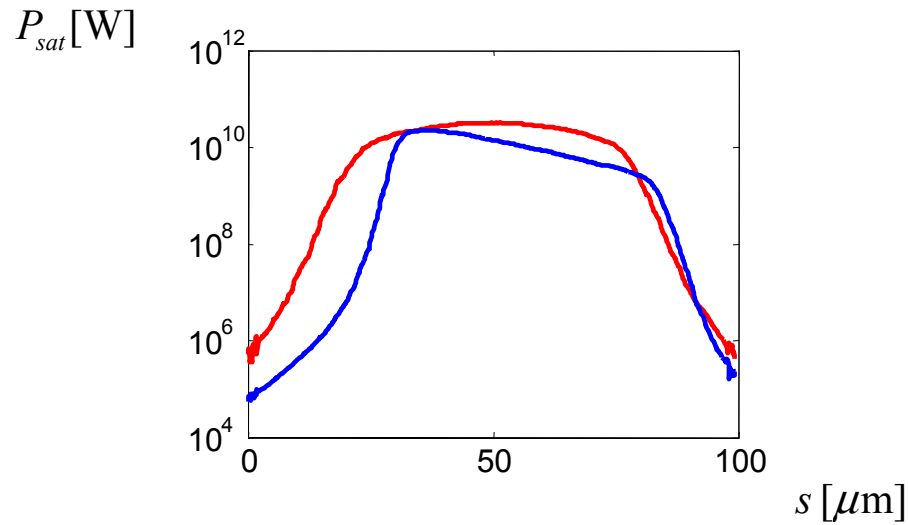
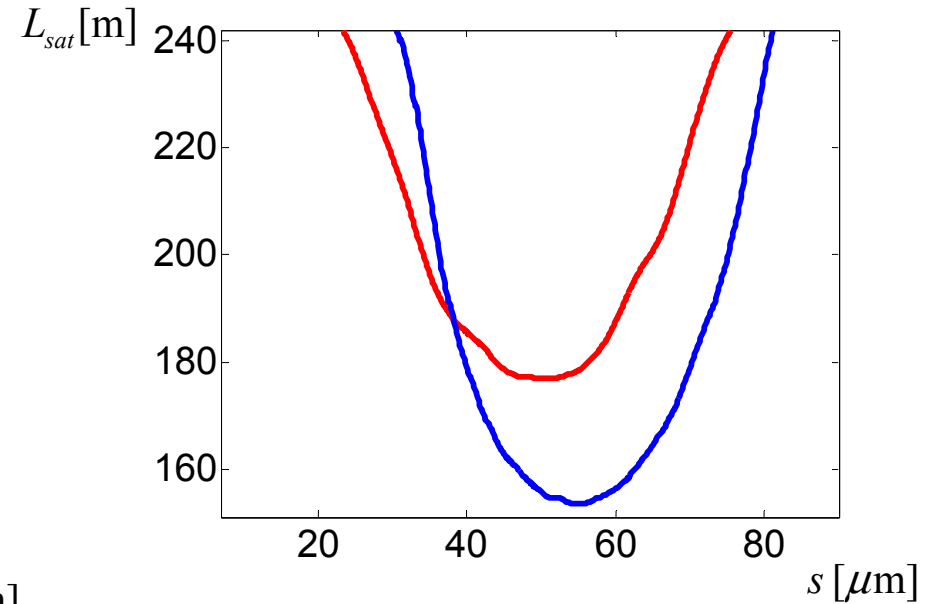
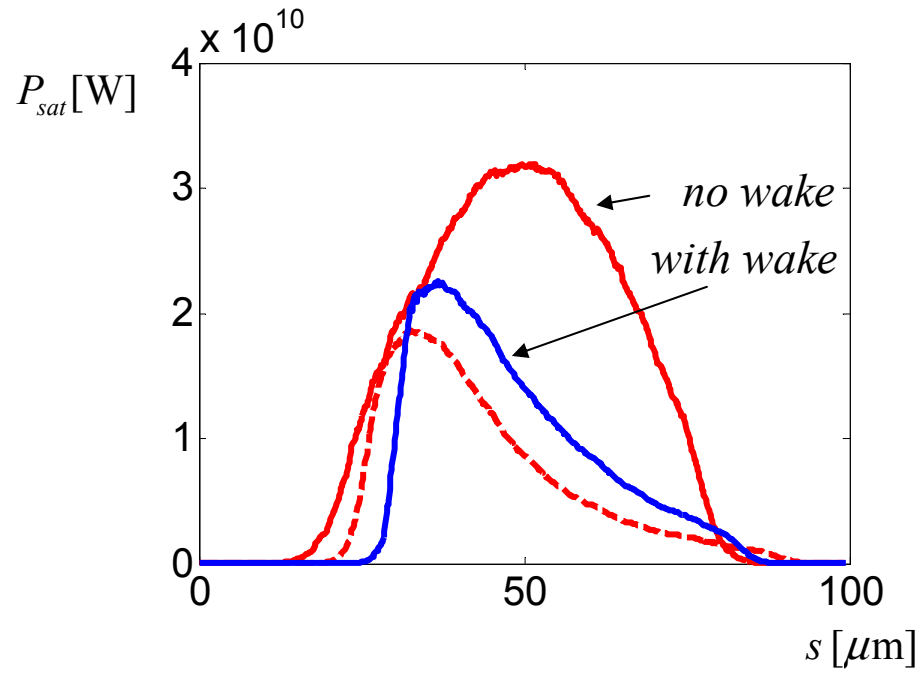
# Genesis steady state simulation

Scan with ELOSS = - 51keV/m

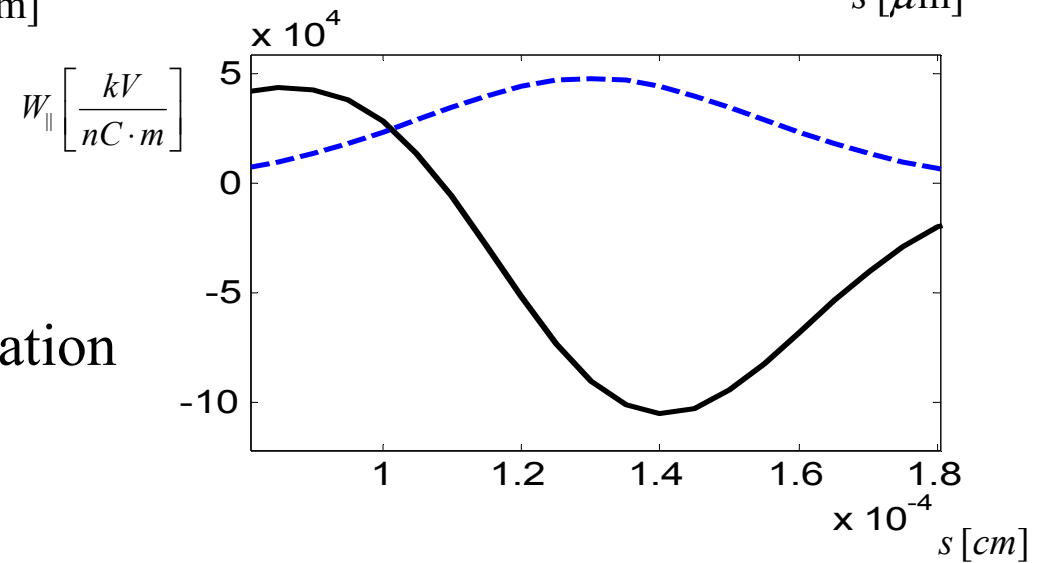
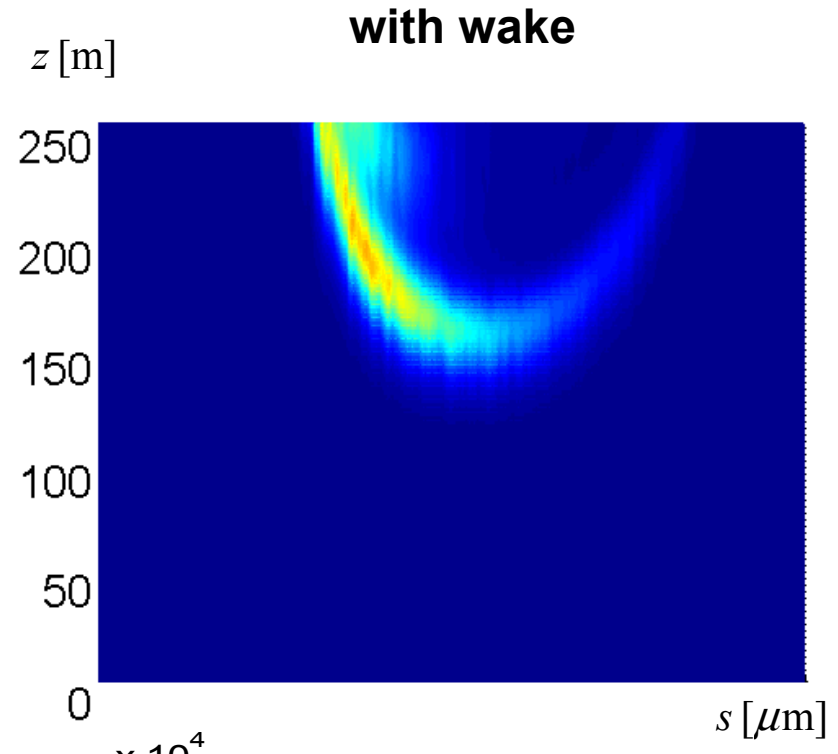
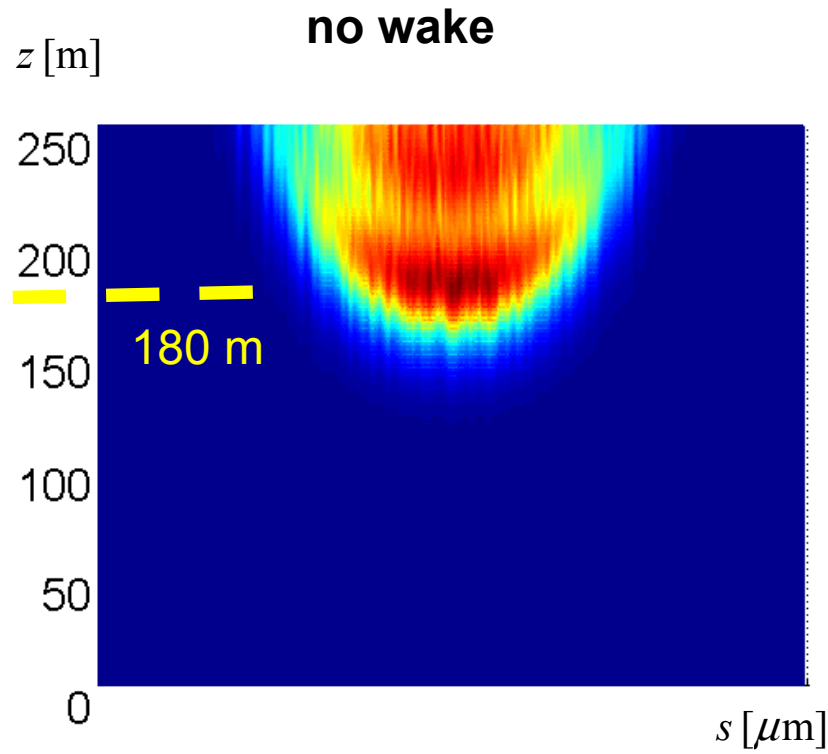


$$\lambda_s^{num} = 0.10087 \text{ [nm]} \quad \longrightarrow \quad 0.10091 \text{ [nm]}$$

# Genesis time dependent simulation (amplifier)

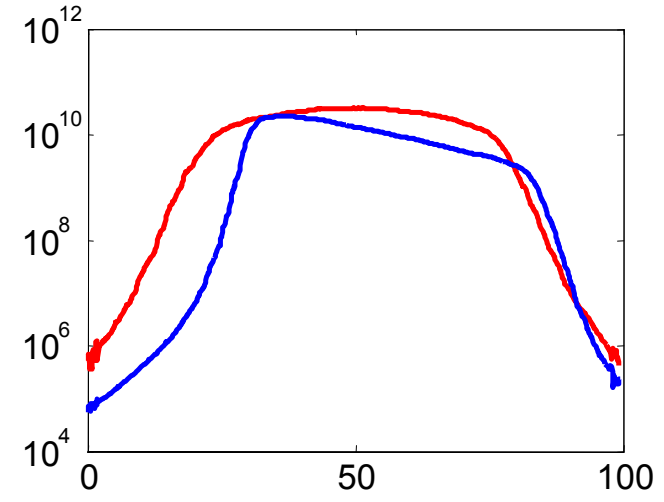
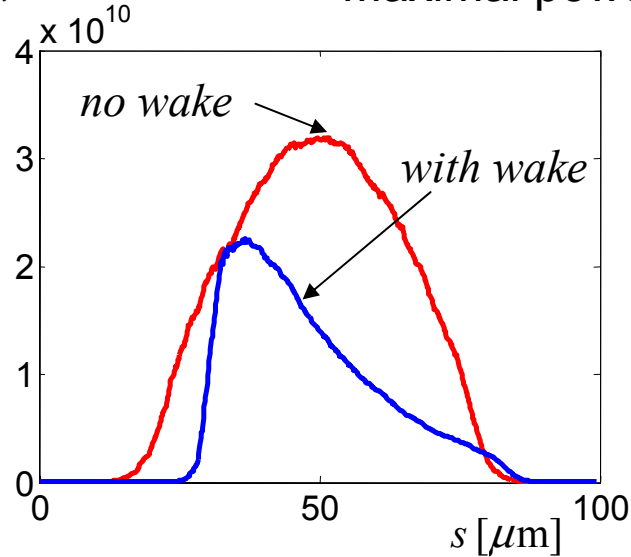


# Power

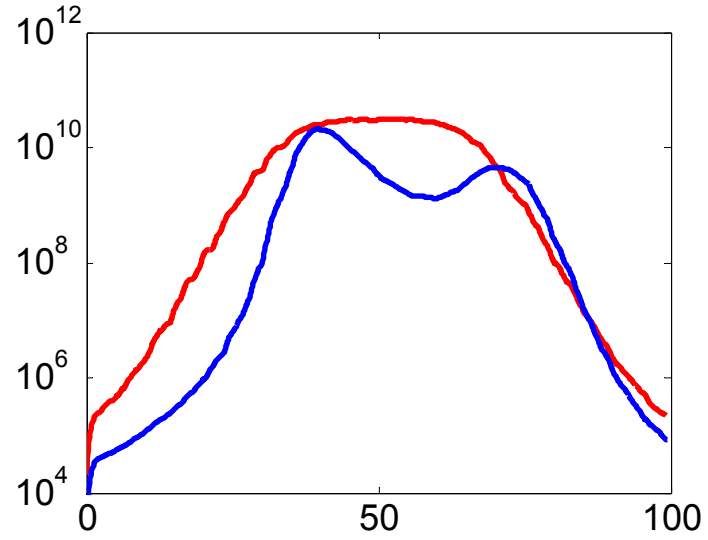
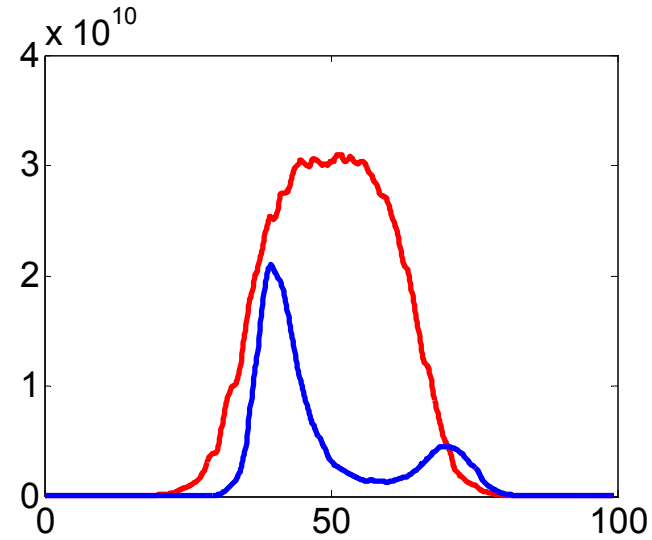


$$d = \frac{\langle P_{total} \rangle}{\langle P_{total}^{wake} \rangle} = 3.3 - \text{power degradation}$$

$P_{sat}$  [W] Maximal power along the undulator up to  $z = 250$  m



$$\frac{\langle P_{sat} \rangle}{\langle P_{sat}^{wake} \rangle} = 2.1$$

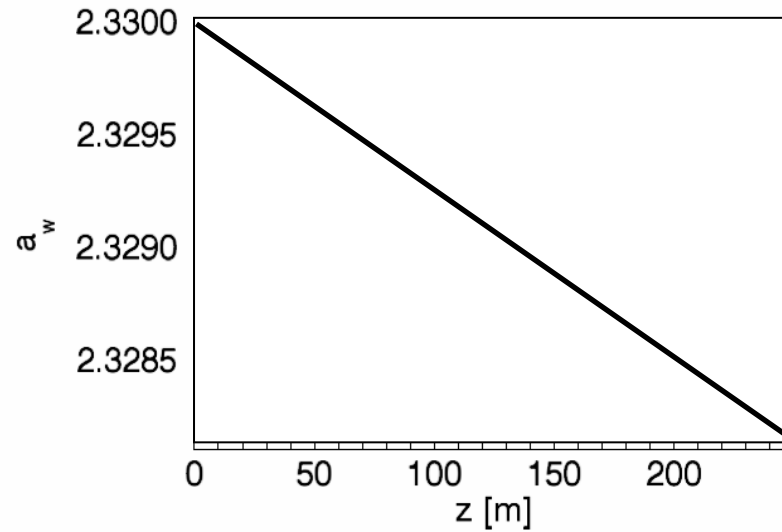
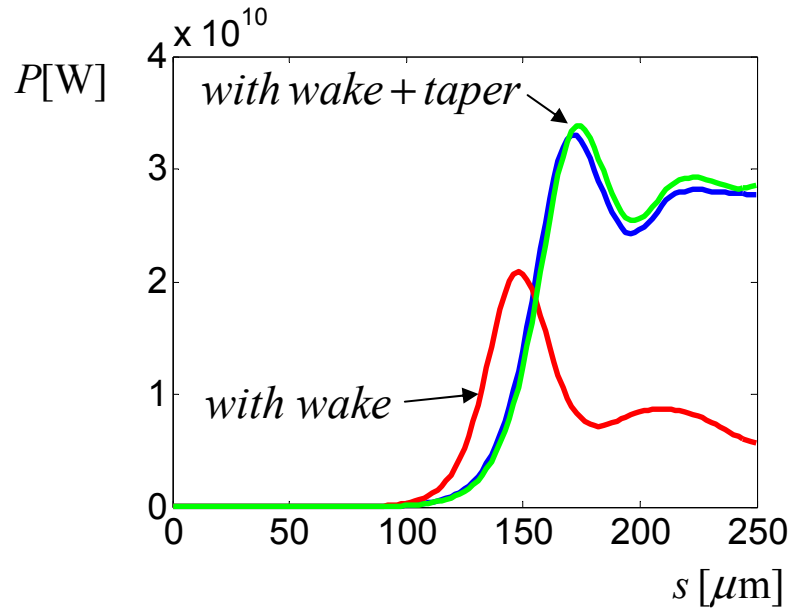


$$\frac{\langle P_{180} \rangle}{\langle P_{180}^{wake} \rangle} = 3.6$$

Power at  $z = 180$  m

## Tapering (steady state)

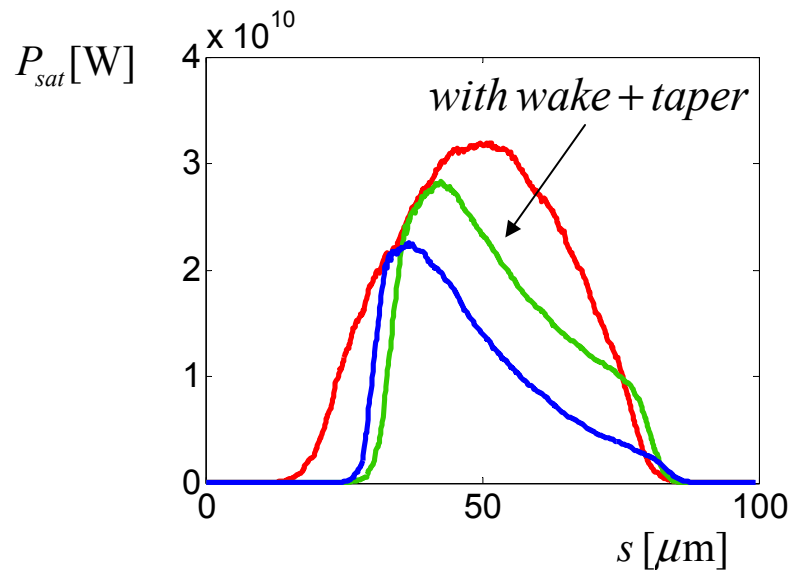
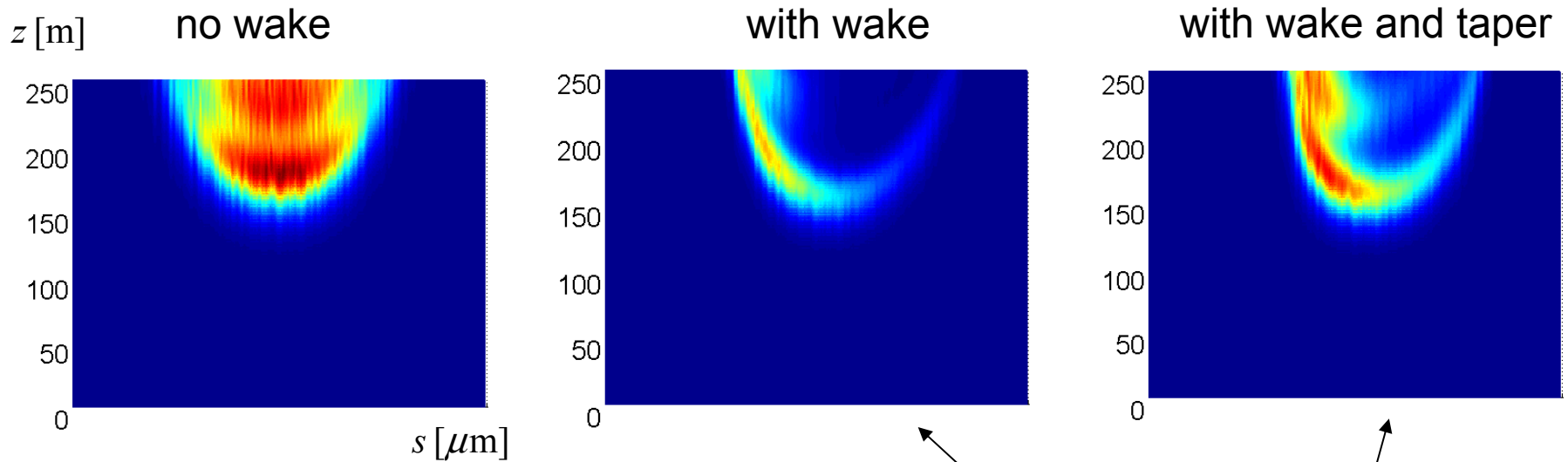
with ELOSS = - 51keV/m



$$\frac{\Delta a_w}{a_w} \approx \frac{\Delta \gamma}{\gamma} = \frac{\Delta E}{E} = \frac{51[\text{keV} / \text{m}] \cdot 250[\text{m}]}{20[\text{GeV}]} = 6.375e-4$$

$$\frac{\Delta a_w}{a_w} = 8.0e-4 = 1.5\rho_1 \quad \rightarrow \quad \text{Taper} \sim 64 \text{ keV/m}$$

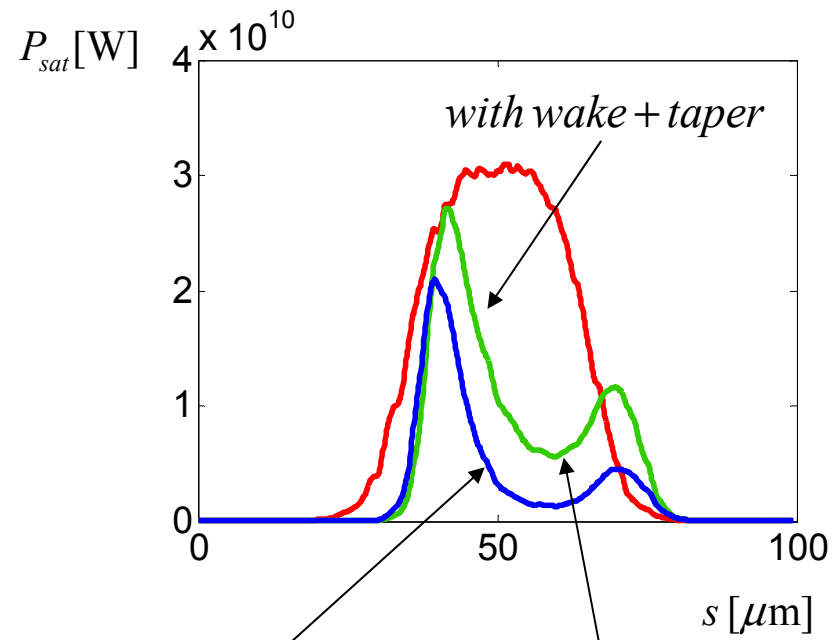
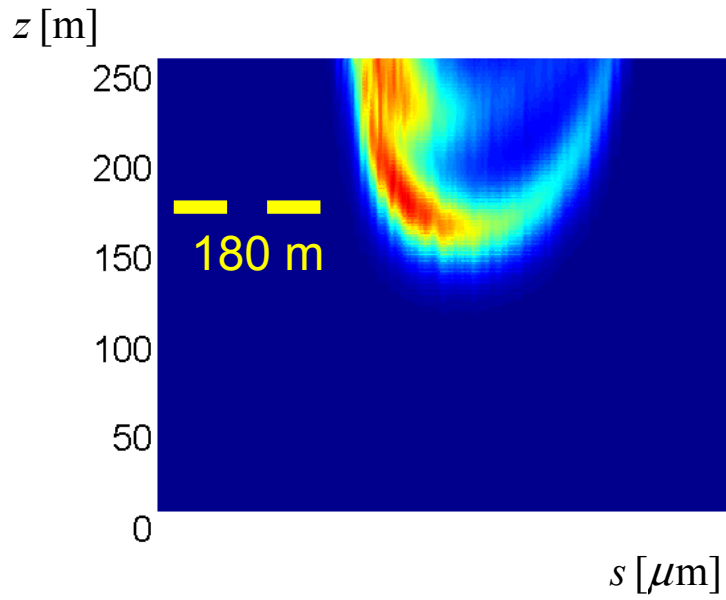
# Power with tapering (time-dependent)



$$\frac{\langle P_{sat} \rangle}{\langle P_{sat}^{wake} \rangle} = 2.1$$

$$\frac{\langle P_{sat} \rangle}{\langle P_{sat}^{wake+taper} \rangle} = 1.5$$

## Tapering



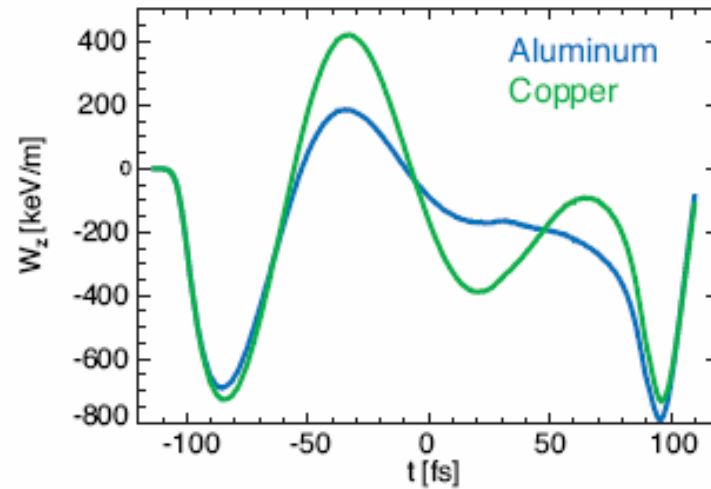
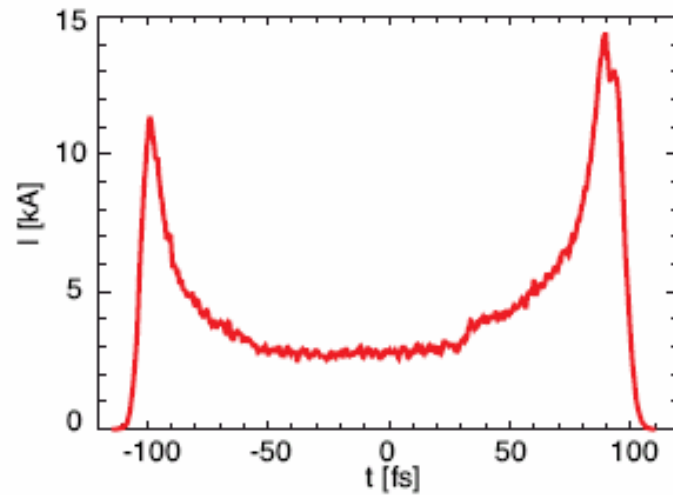
$$\frac{\Delta a_w}{a_w} = 8.0e-4 = 1.5\rho_1$$

$$\frac{\langle P_{180} \rangle}{\langle P_{180}^{wake} \rangle} = 3.6$$

$$\frac{\langle P_{180} \rangle}{\langle P_{180}^{wake+taper} \rangle} = 1.9$$

# Comparison with LCLS

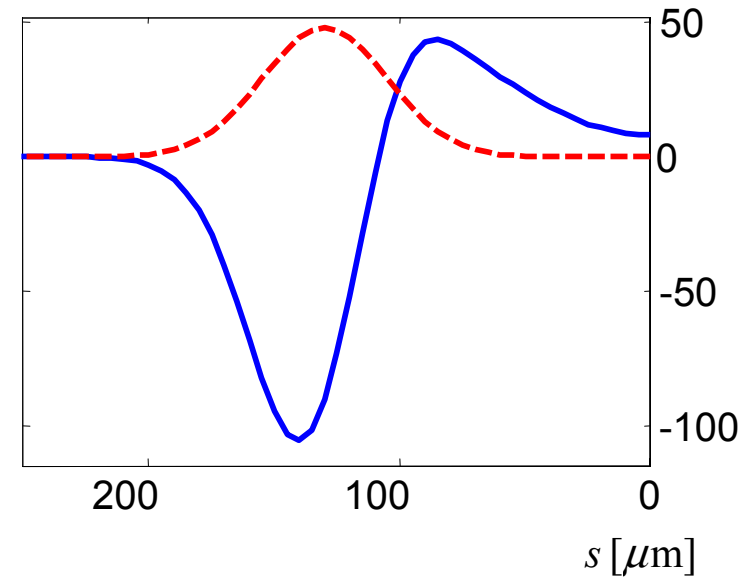
K.Bane  
and  
G.Stupakov



$\delta_A = \frac{W_A L}{E \rho_1}$  - fractional energy oscillation amplitude

	LCLS	XFEL
$W_A$ , kV/m	400	100
L, m	100	200
E, GeV	14	20
$\rho_1$	5e-4	5.5e-4
$\delta_A$	<b>6</b>	<b>2</b>

$W_{\parallel} \left[ \frac{kV}{m} \right]$





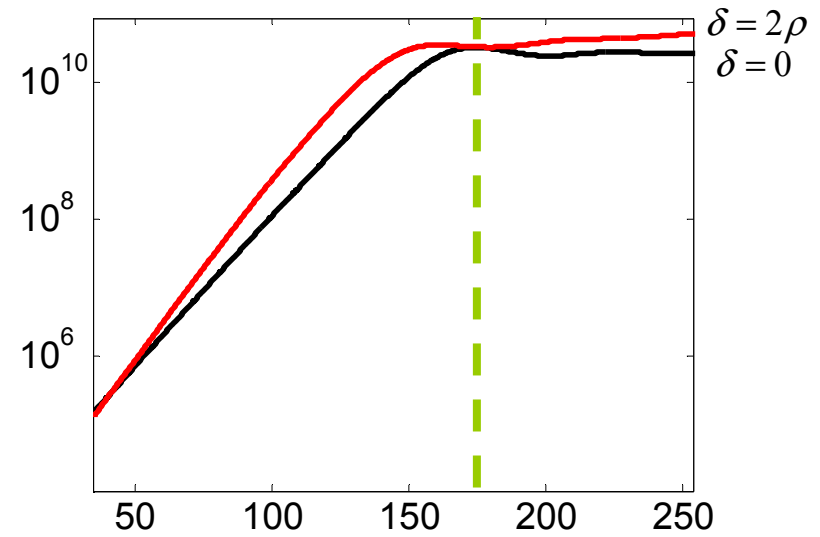
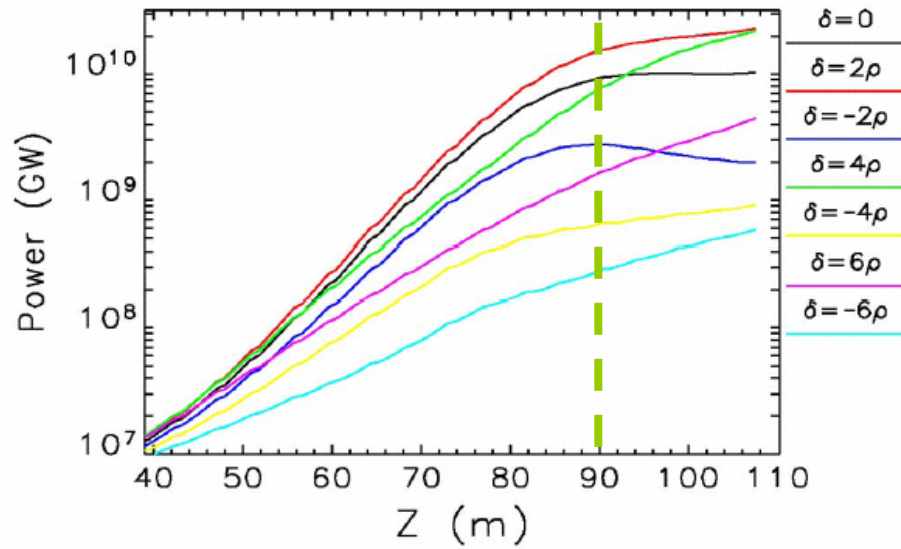


FIG. 9. (Color) LCLS power evolution obtained from GENESIS simulations for different fractional energy change  $\delta(z = 90 \text{ m})$ .

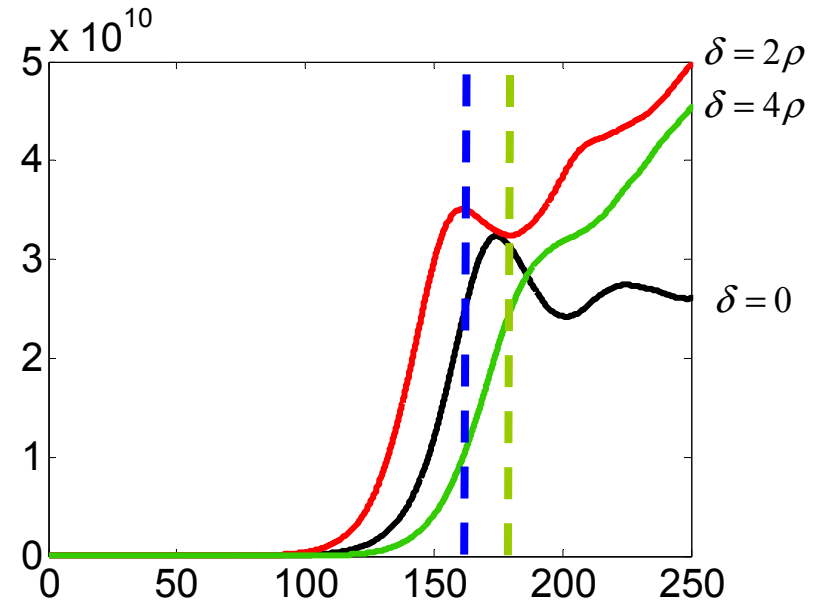
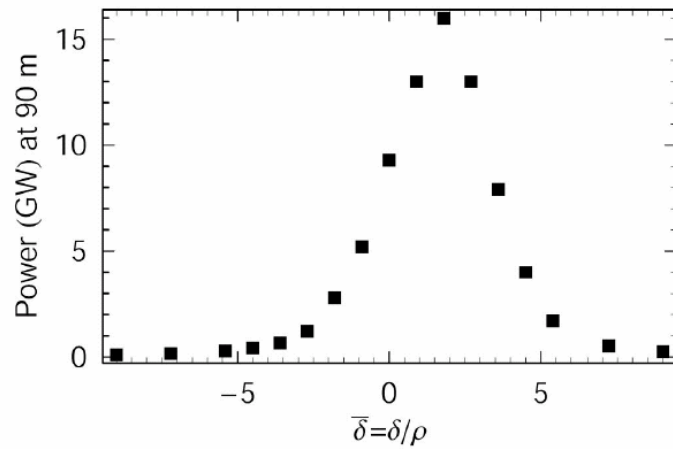


FIG. 10. LCLS power obtained from GENESIS simulations versus fractional energy change  $\bar{\delta} = \delta/\rho$  at  $z = 90 \text{ m}$ . The maximum power is reached when  $\bar{\delta} \approx 2\rho$ , and the FWHM fractional energy change is about  $4\rho$ , in agreement with Eq. (50).

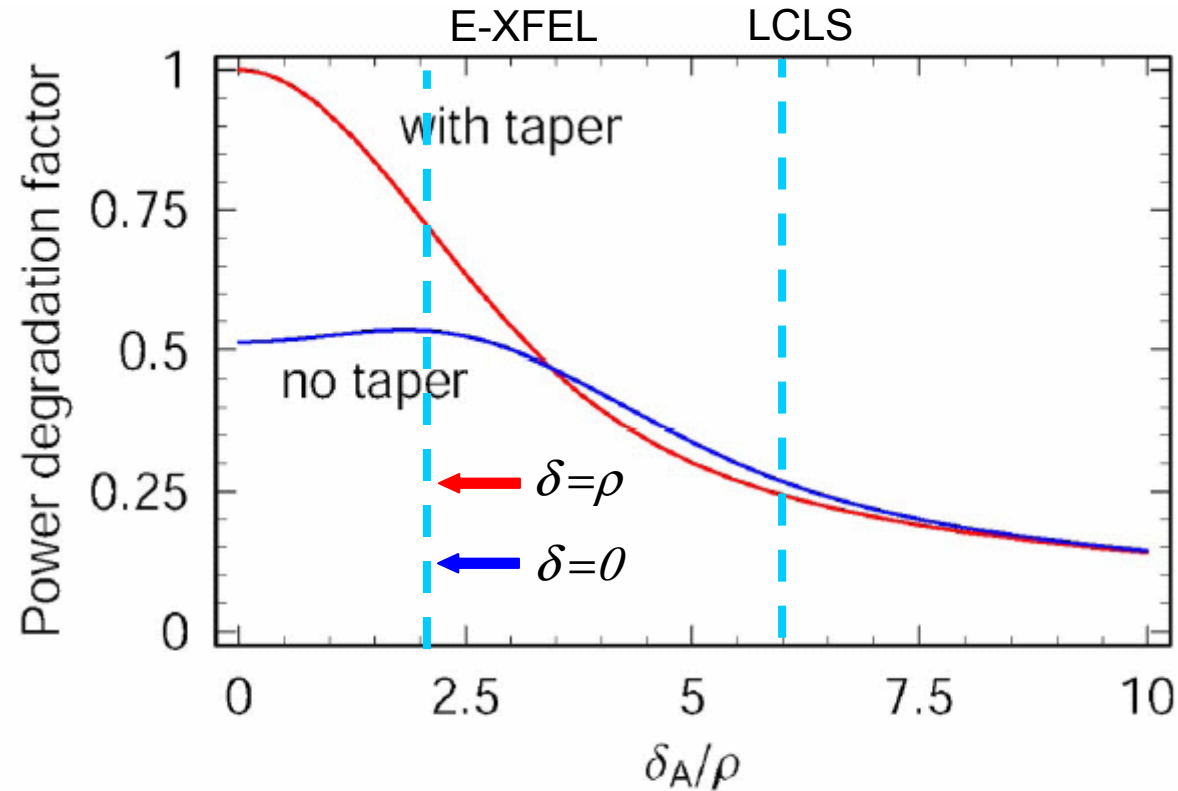


FIG. 11. (Color) Power degradation factor averaged over the core part of the bunch (with about  $30 \mu\text{m}$  in length) versus the sinusoidal wake oscillation amplitude  $\delta_A/\rho$  at the LCLS saturation ( $z = 90 \text{ m}$ ) for a prescribed tapered undulator (red) and without any taper (blue).

## Conclusions

1. For smooth Gaussian bunch the wake field reduces the power at L=180 m by factor 3.6

$$\langle P_{180} \rangle / \langle P_{180}^{wake} \rangle = 3.6$$

2. The tapering allows to reduce the degradation

$$\langle P_{180} \rangle / \langle P_{180}^{wake+taper} \rangle = 1.9$$

3. The numerical simulations are required to find an optimal tapering.
4. The wake effect for the expected bunch shape should be analyzed .