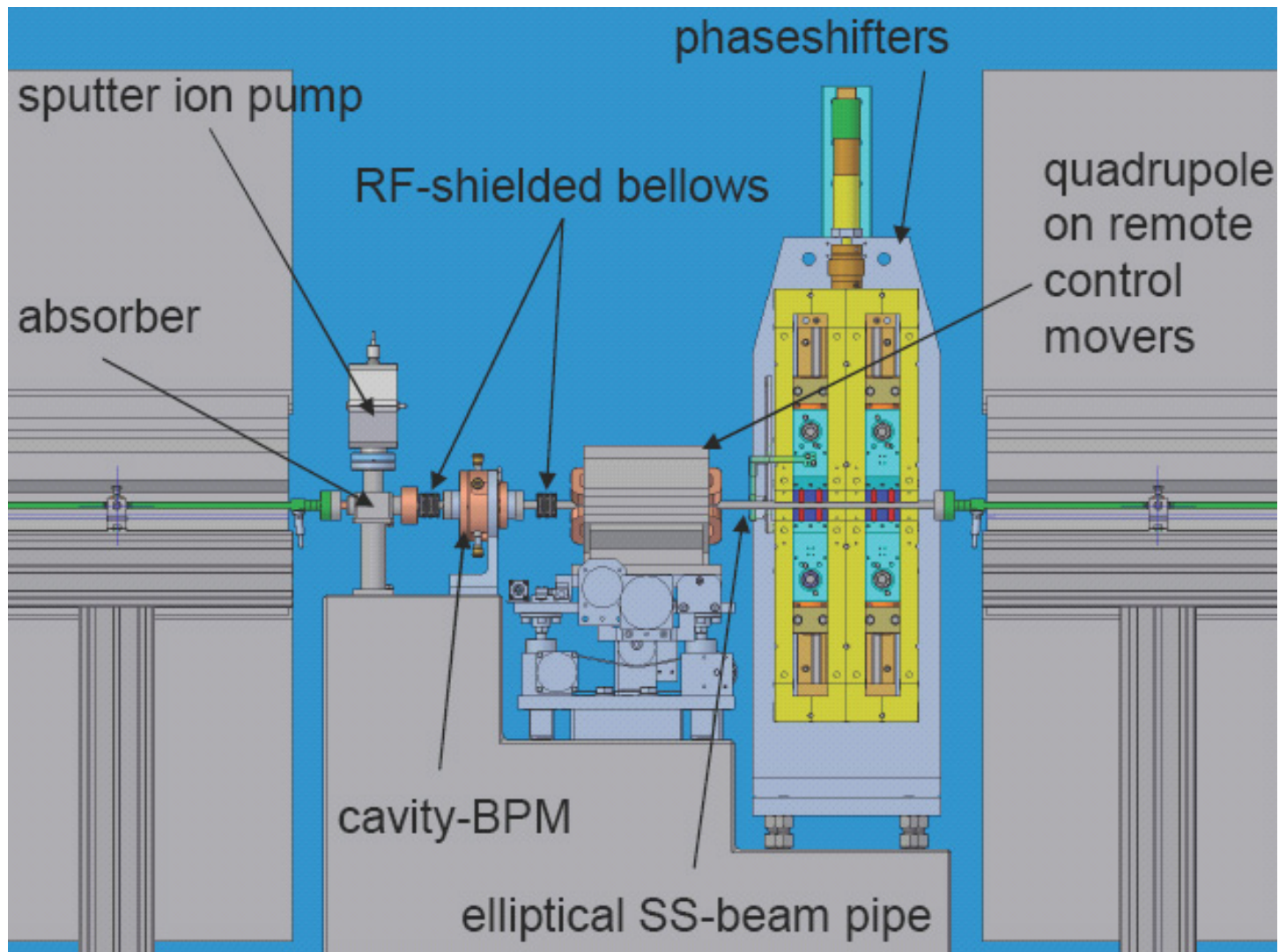




# Longitudinal Impedance Budget in XFEL undulator section

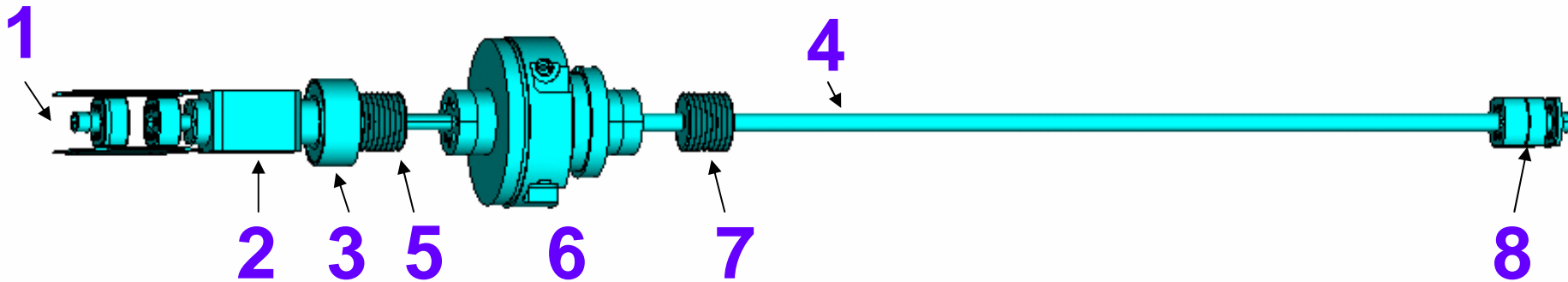
Igor Zagorodnov  
Beam Dynamics Group Meeting  
19.11.07



UNDULATOR- CELL(6.1m) = UNDULATOR (5m) + INTERSECTION (1.1m)

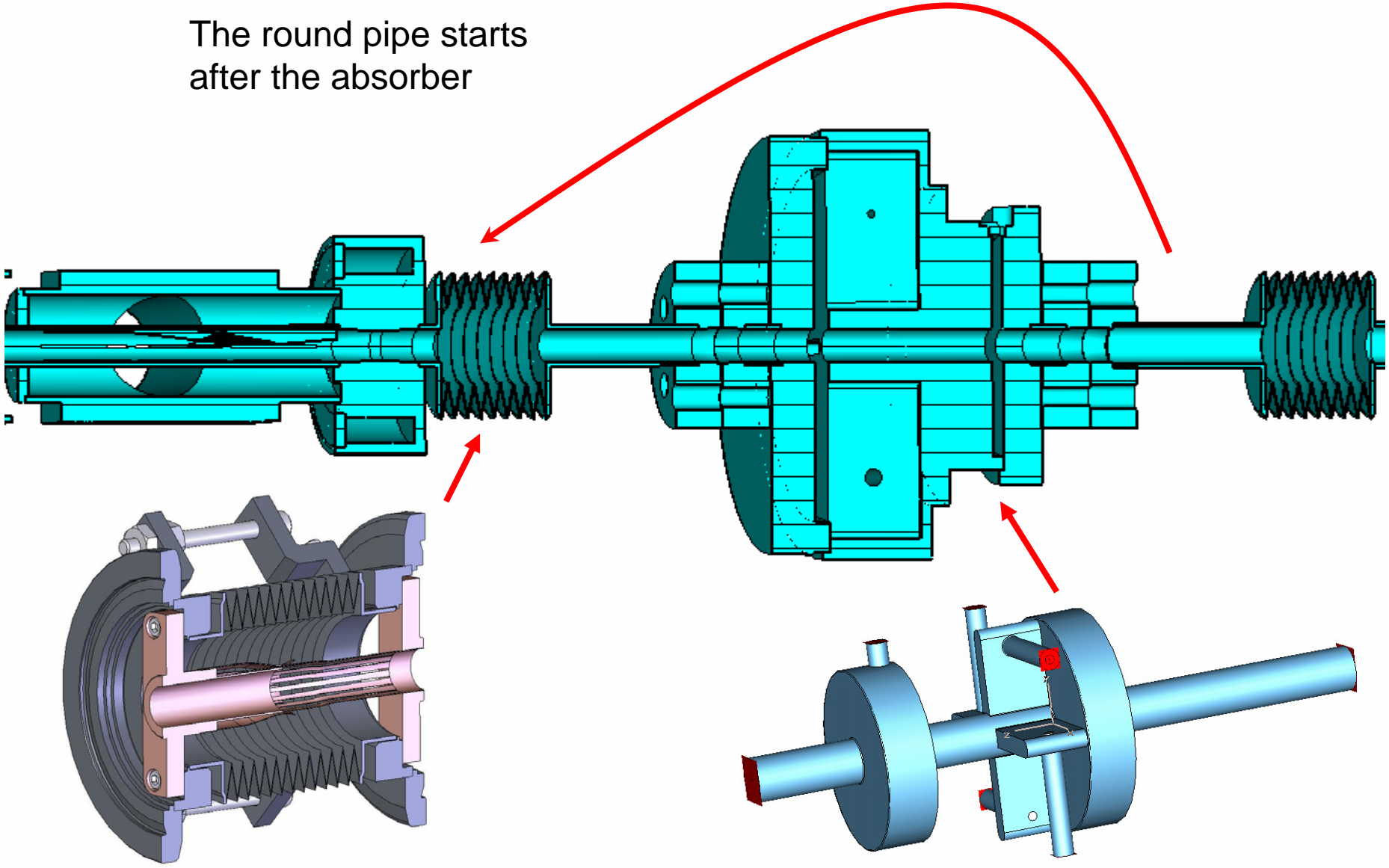
N	Element	from mm	to mm	Effective Length mm	Material	Conduct. 1/Omm/m	Relax. Time sec	Oxid layer nm	Rough ness nm
1	Elliptical pipe	0	5288	5161	Aluminium	3,66E+07	7,10E-15	5	300
2	Pump	5161	5266	105	Aluminium	3,66E+08	7,10E-15	5	300
3	Absorber/Round transition	5266	5288	22	Copper	5,80E+07	2,46E-14	5	300
4	Round pipe	5288	6100	652	Copper	5,80E+07	2,46E-14	5	300
5	Below	5288	5318	30	BeCu 174	2,78E+07	2,46E-14	5	300
6	BPM	5373	5473	100	Stainless Steel 304	1,40E+06	2,40E-15	5	300
7	Below	5513	5543	30	BeCu 174	2,78E+07	2,46E-14	5	300
8	Round/Elliptical transition	6100	6100	0					

6100



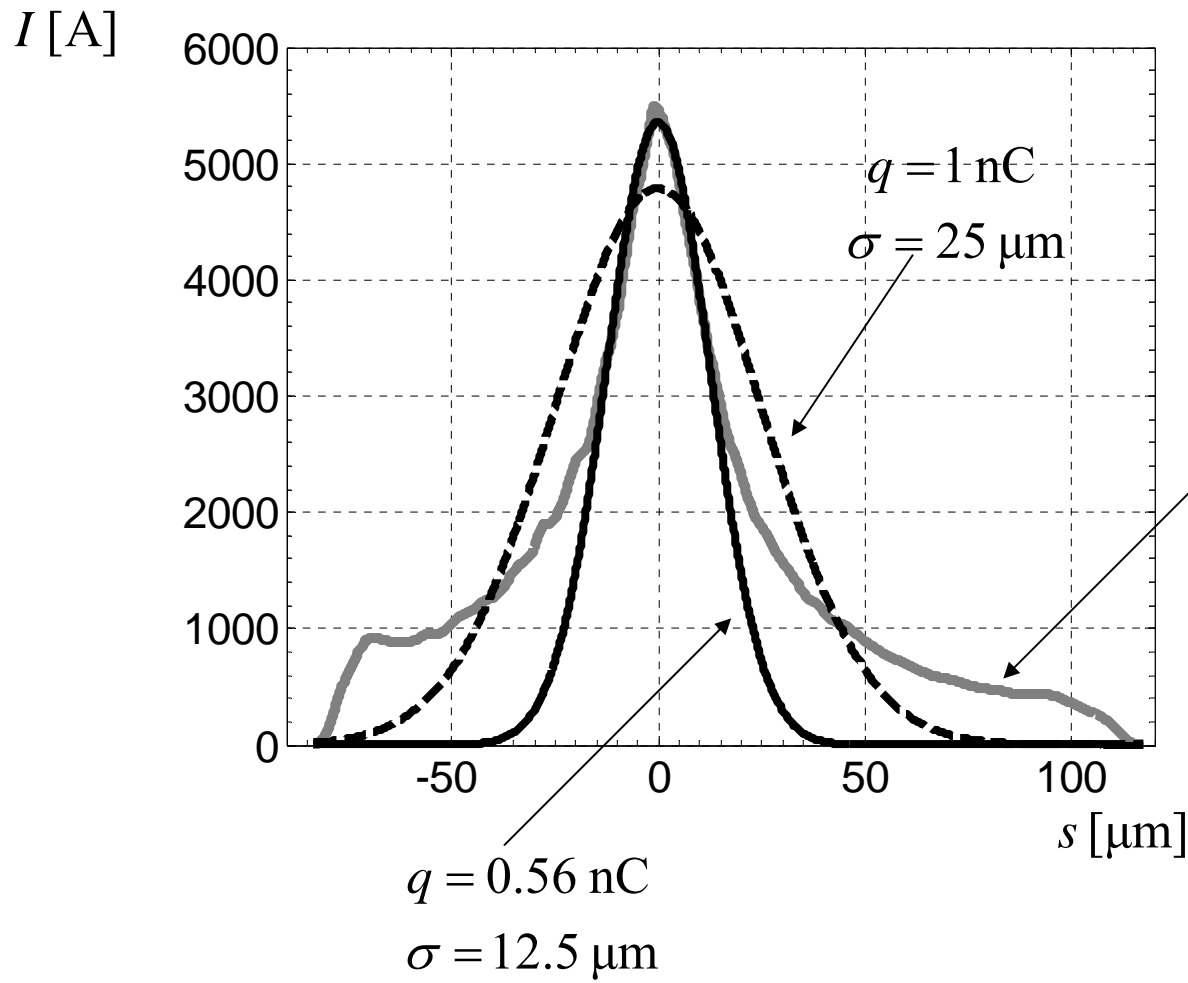
Katrin Schuett, ZM1  
Dirk Lipka, MDI

The round pipe starts  
after the absorber



SLAC design (Soon-Hong Lee talk)  
Torsten Wohlenberg, MVS

Shintake BPM,  
Dirk Lipka, MDI



Bunch shape  
from S2E simulations  
by Martin Dohlus

$$\sigma = 25 \mu\text{m} \quad q = 1 \text{ nC}$$

N	Element	Geom Loss	Geom Spread	Loss	Spread
		kV	kV	kV	kV
1	Elliptical pipe	0	0	239	274
2	Pump	4,4	4,5	9	10
3	Absorber/Round transition	69	27	70	28
4	Round pipe	0	0	22	32
5	Below	24	9	25	10
6	BPM	42	17	70	34
7	Below	24	9	25	10
8	Round/Elliptical transition	36	14	36	14

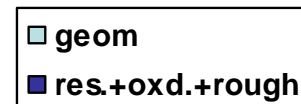
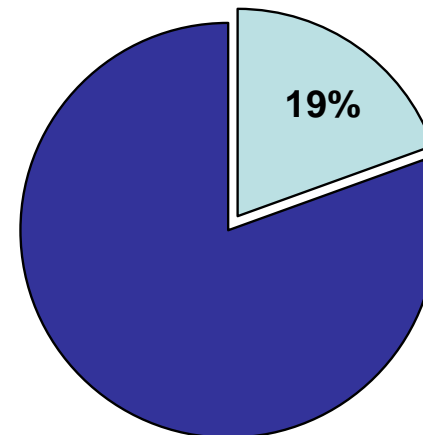
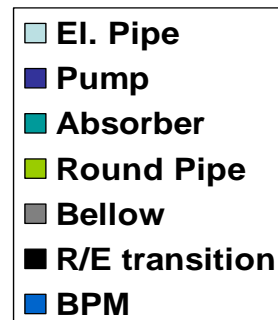
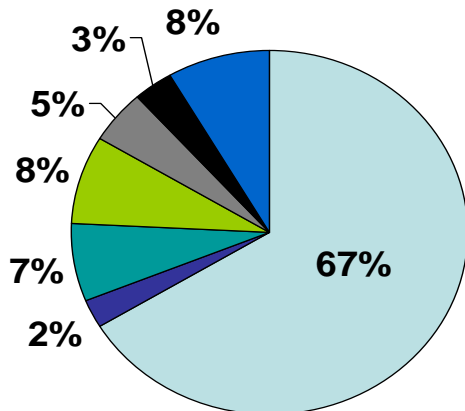
Energy Spread

199,4

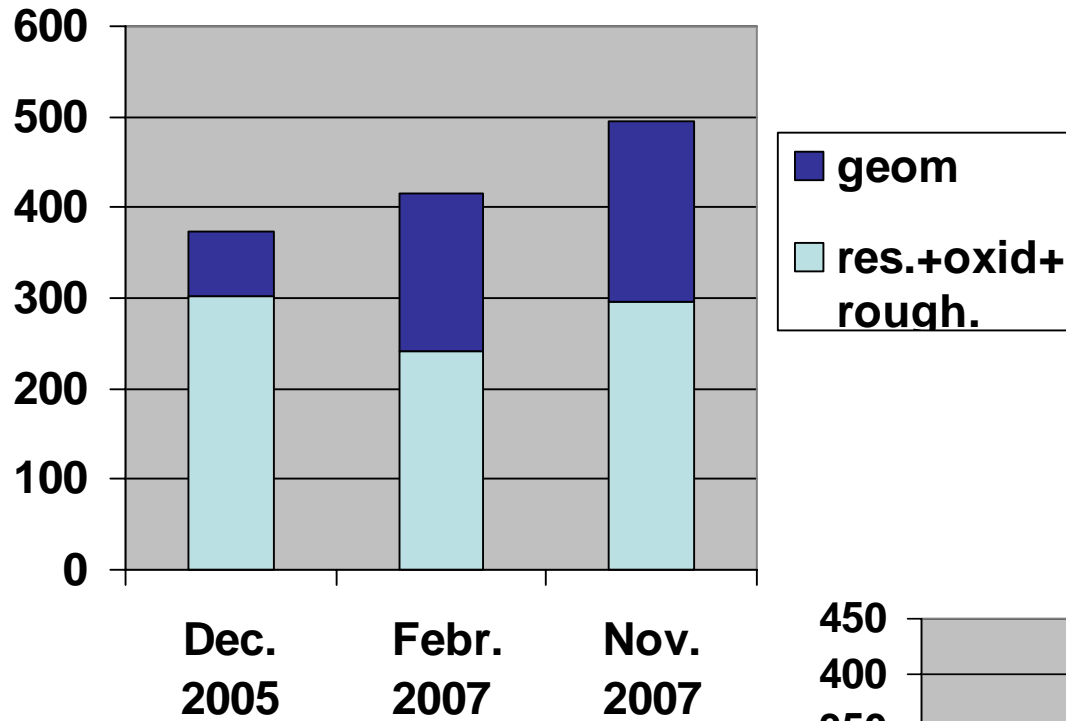
80,5

496

412(365)

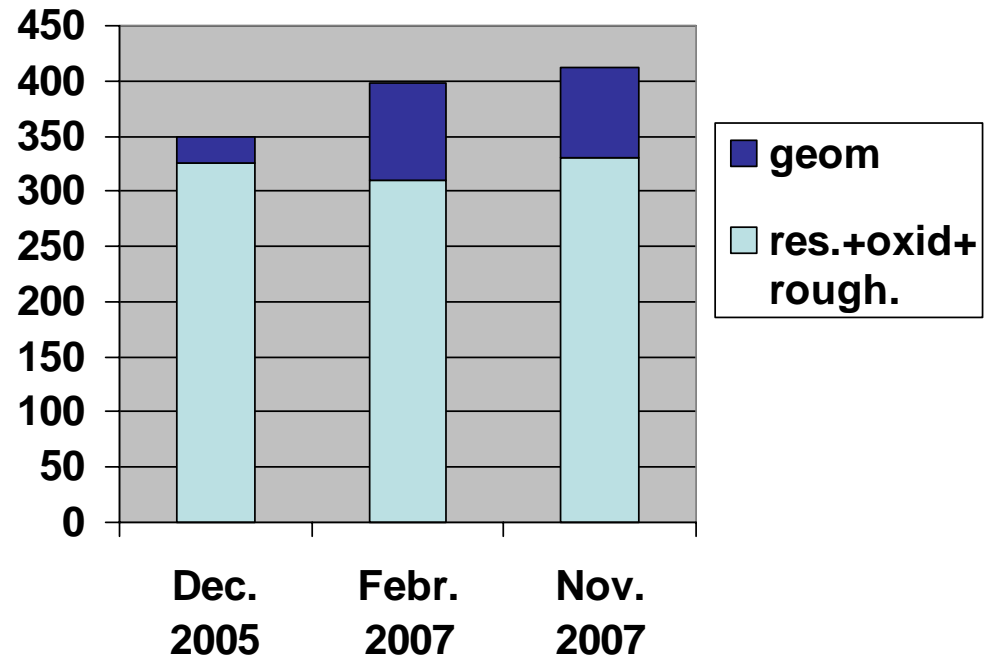


## Energy Loss



$$\sigma = 25 \mu m$$

## Energy Spread



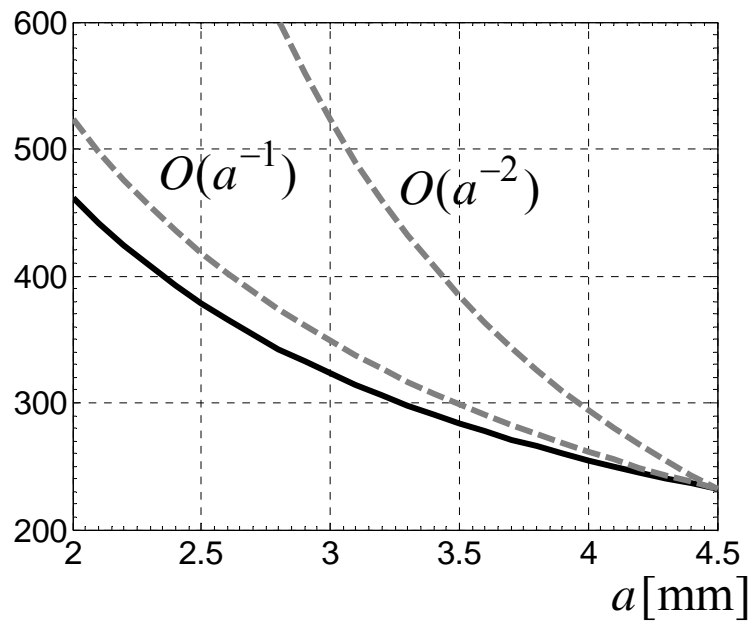
## Scaling laws of longitudinal wakes

Cavity	$\text{Loss} = \frac{Z_0 c}{4a\pi^{2.5}} \Gamma\left(\frac{1}{4}\right) \sqrt{\frac{g}{\sigma}}$	$O(a^{-1})$
Periodic structure		$O(a^{-2})$
Collimator	$\text{Loss} = \frac{Z_0 c}{2\pi^{1.5} \sigma} \ln\left(\frac{b}{a}\right)$	$O(1)$
Short Range Resistive		$O(a^{-2})$
Long Range Resistive	$s \gg s_0 = \left(\frac{2a^2}{k Z_0}\right)^{1/3}$	$O(a^{-1})$

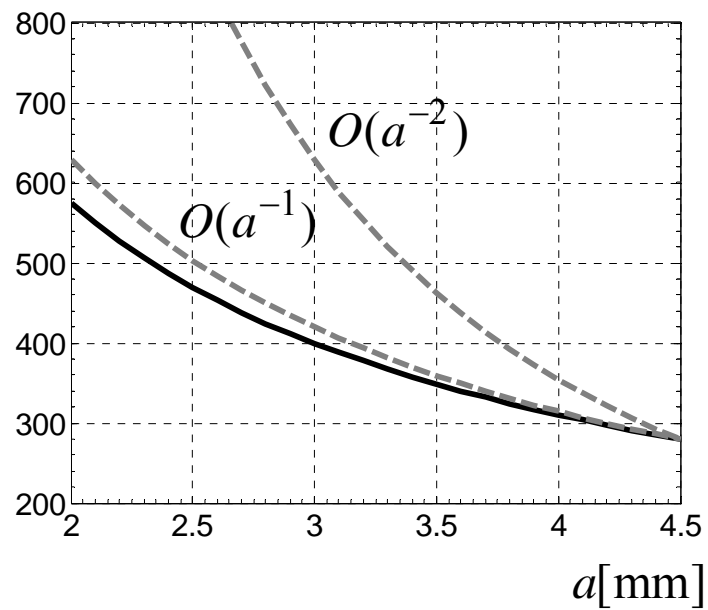
$s_0 = 14 \mu\text{m}$  for  $a=4.4 \text{ mm}$  and  $k=3.66\text{e}7/\text{Omm/m}$



Loss [V/pC]



Spread [V/pC]



N	Element	Scaling
1	Elliptical pipe	$O(a^{-1})$
2	Pump	
3	Absorber/Round transition	$O(1)$
4	Round pipe	$O(a^{-1})$
5	Below	
6	BPM	
7	Below	
8	Round/Elliptical transition	$O(1)$

$\sim O(a^{-1})$

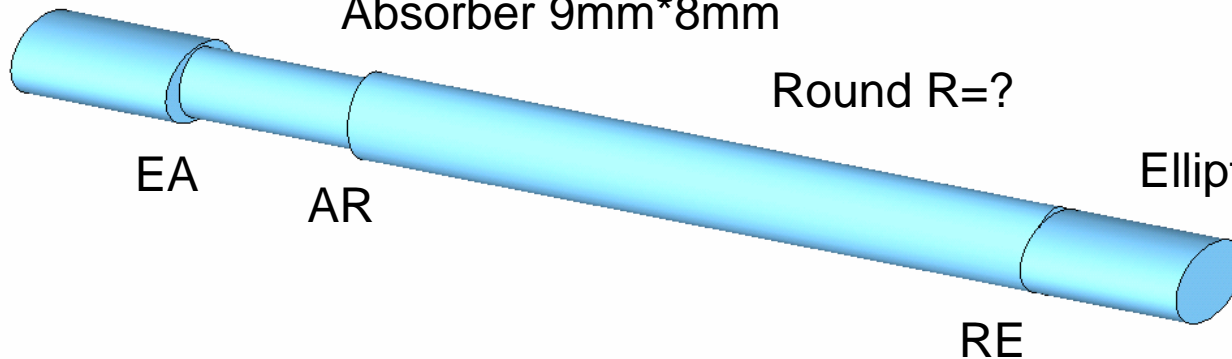
# Absorber+Round Pipe+Elliptical Pipe

Elliptical 15mm\*8.8mm

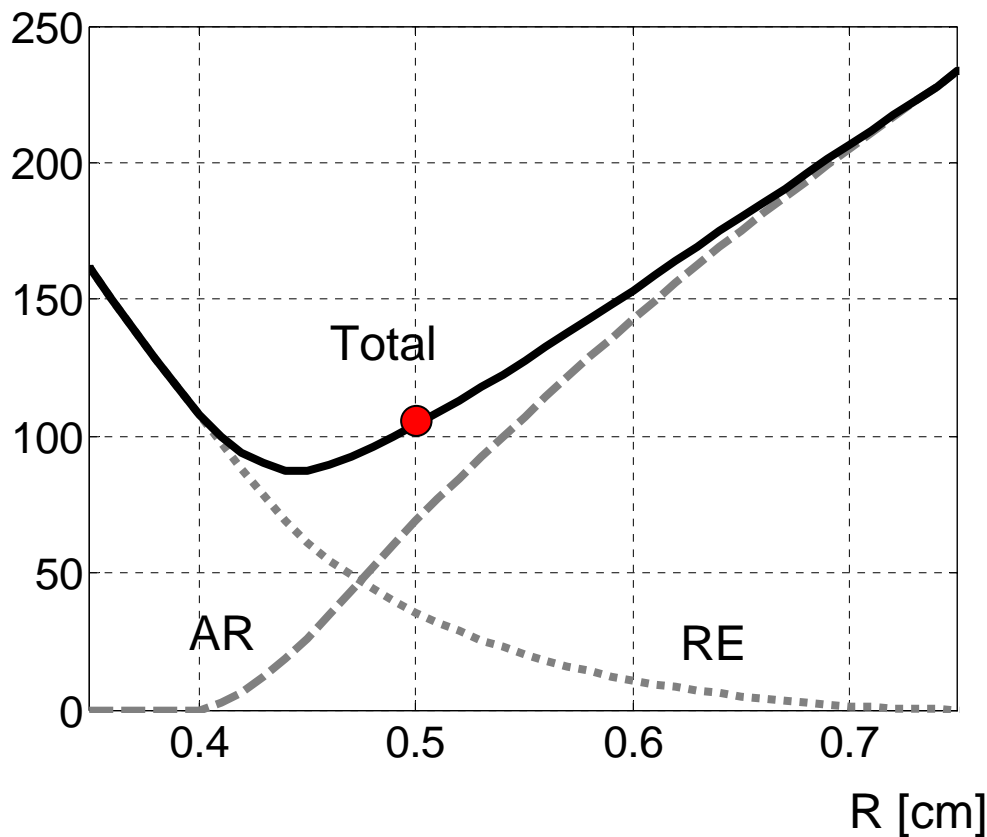
Absorber 9mm\*8mm

Round R=?

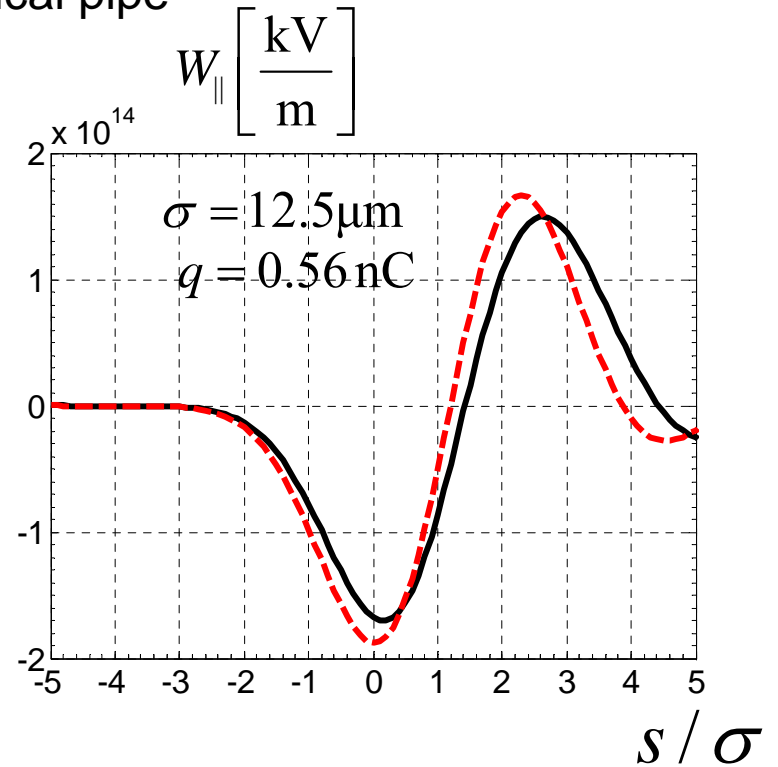
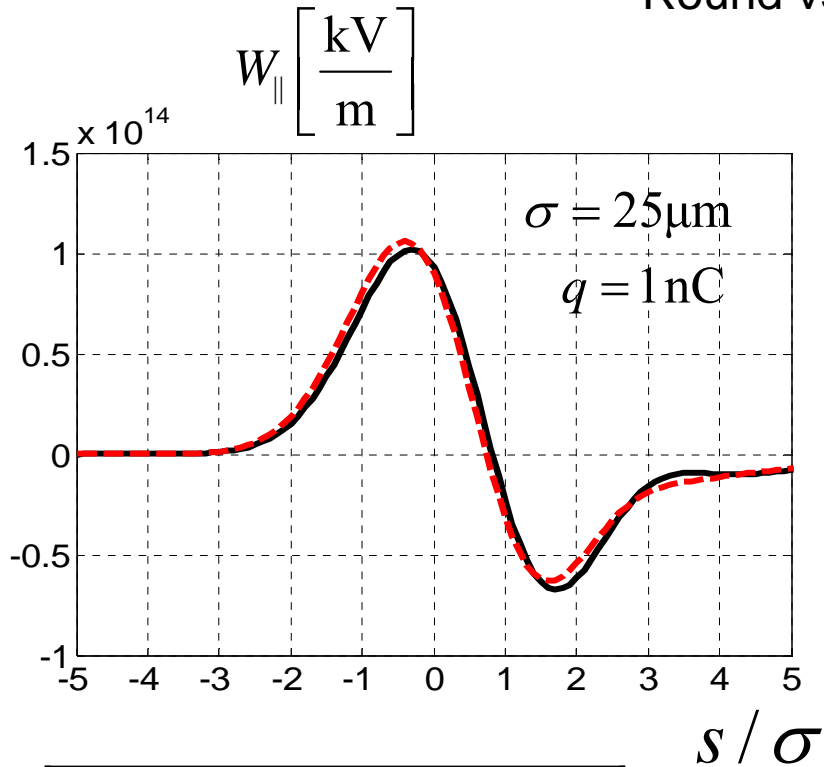
Elliptical 15mm\*8.8mm



Loss [V/pC]



## Round vs. Elliptical pipe

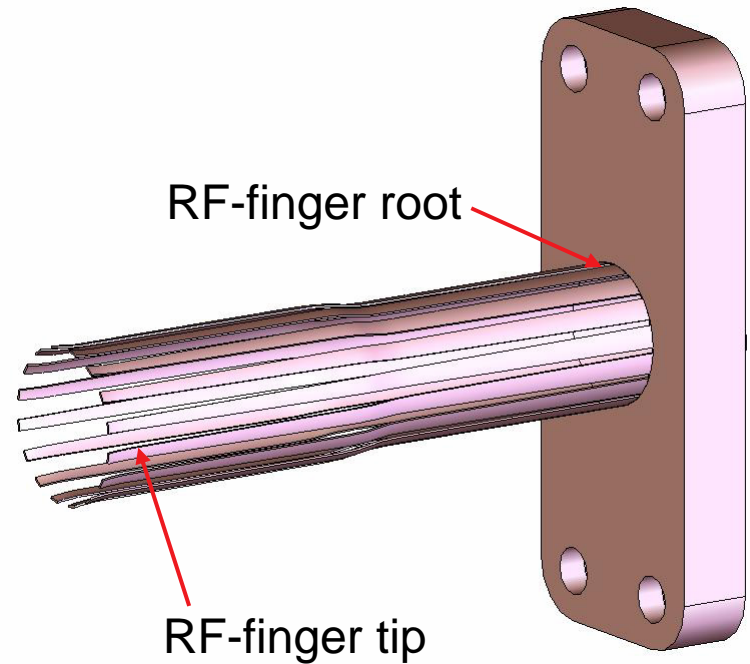
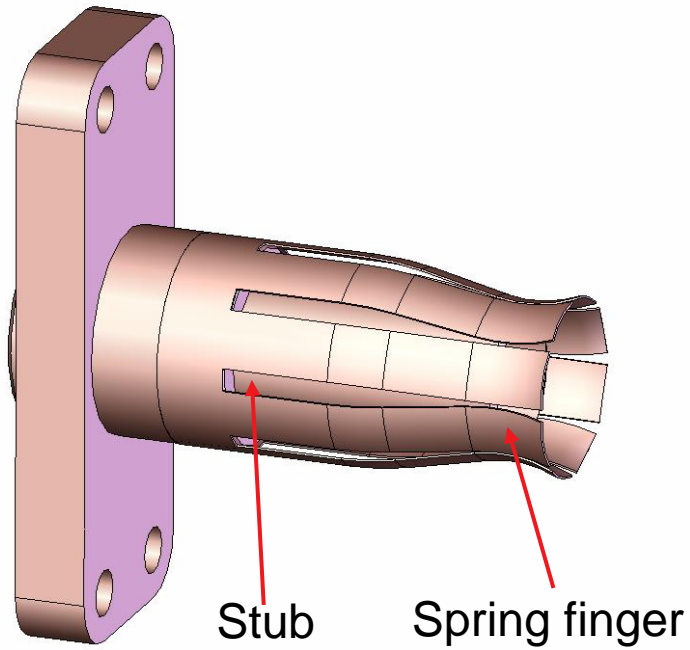
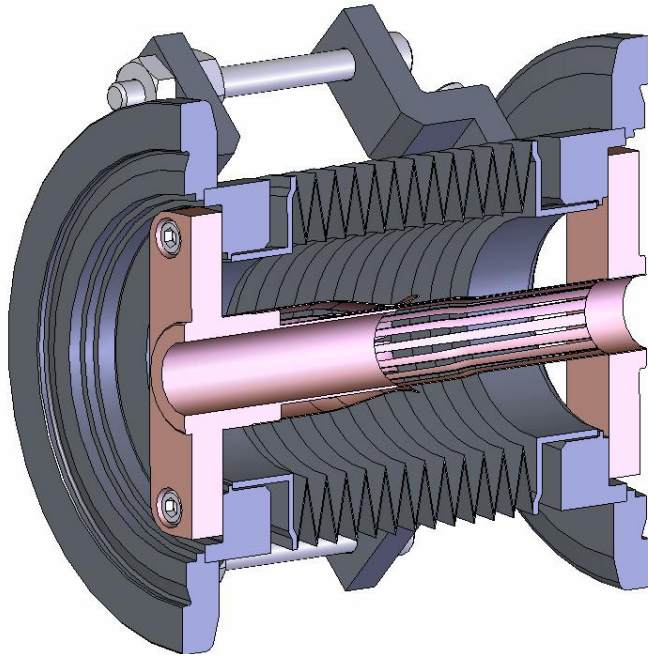


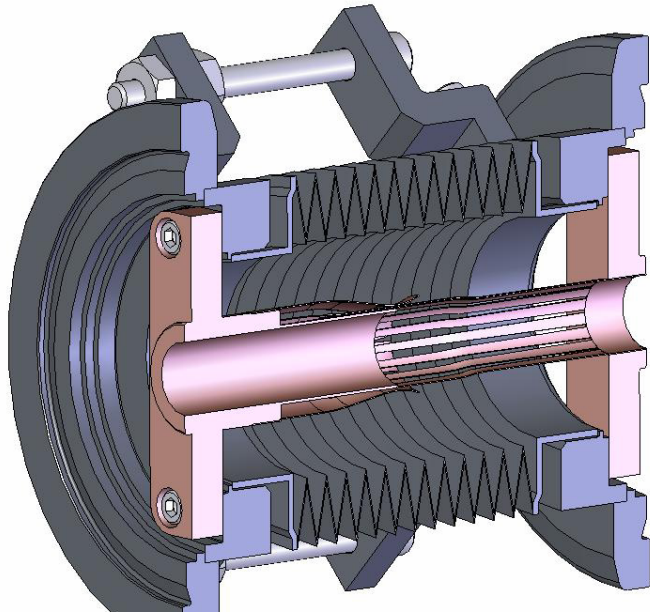
	Loss, V/pC	Spread, V/pC
round	237	285
elliptical	239	274

Mathcad script for arbitrary shape (author M. Dohlus)

**Internal Design Review**

Soon-Hong Lee

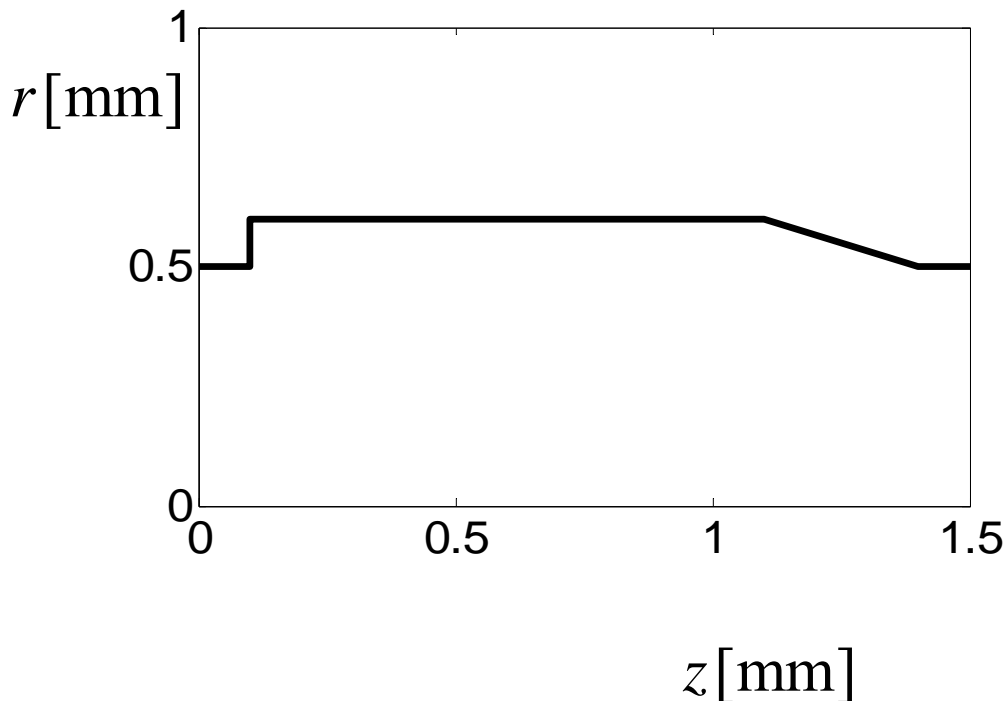




## Shielded bellows

$$\text{Loss} = 23.8 \text{ V} / \text{Pc}$$

$$\text{Spread} = 9.3 \text{ V} / \text{Pc}$$



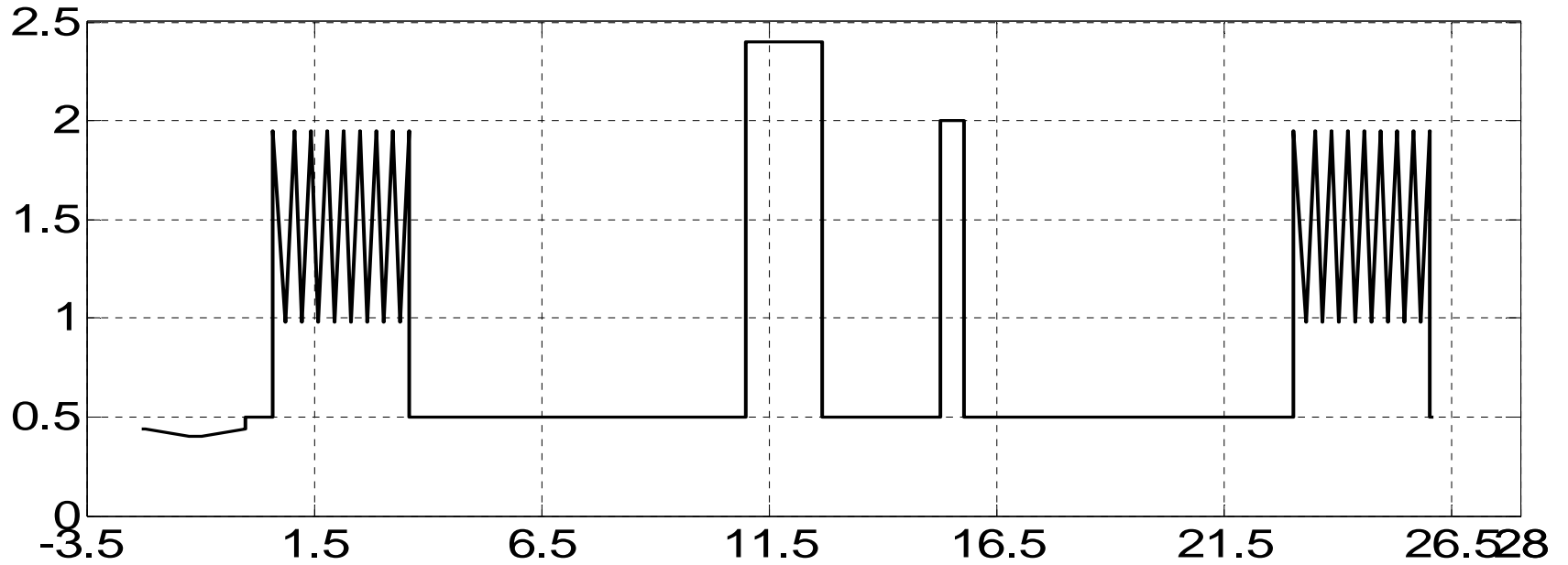
„Now, we extend the vacuum chamber from one side almost all the way through the bellows section leaving a small variable length gap at one end. The maximum length of the variable gap at the end is 7 mm for a fully extended bellows.

... two additional in-line bellows per break section, ... each of these bellows can be modeled as three small gaps. (0.77 mm in length).“

Heinz-Dieter Nuhn, SLAC, 13.11.07

# Unshielded bellow

Absorber, bellow, BPM, bellow



	Loss V/pC	Spread V/pC
Absorber with step	57.2	25.1
Bellow	39.1 (24)	15.8 (9)
BPM	42.2	17.0
Absorber, Bellow	78.6	24.9
Absorber, bellow, BPM	113.0	36.9
Absorber, bellow, BPM, bellow	143.9	49.3

$$\sigma = 12.5 \mu\text{m} \quad q = 0.56 \text{ nC}$$

$$\sigma = 25 \mu\text{m} \quad q = 1 \text{ nC}$$

N	Element	Loss	Spread	Loss	Spread
		kV	kV	kV	kV
1	Elliptical pipe	520	363	239	274
2	Pump	16	14	9	10
3	Absorber/Round transition	79	33	70	28
4	Round pipe	56	64	22	32
5	Below	31	14	25	10
6	BPM	86	37	70	34
7	Below	31	14	25	10
8	Round/Elliptical transition	40	17	36	14

859

556(514)

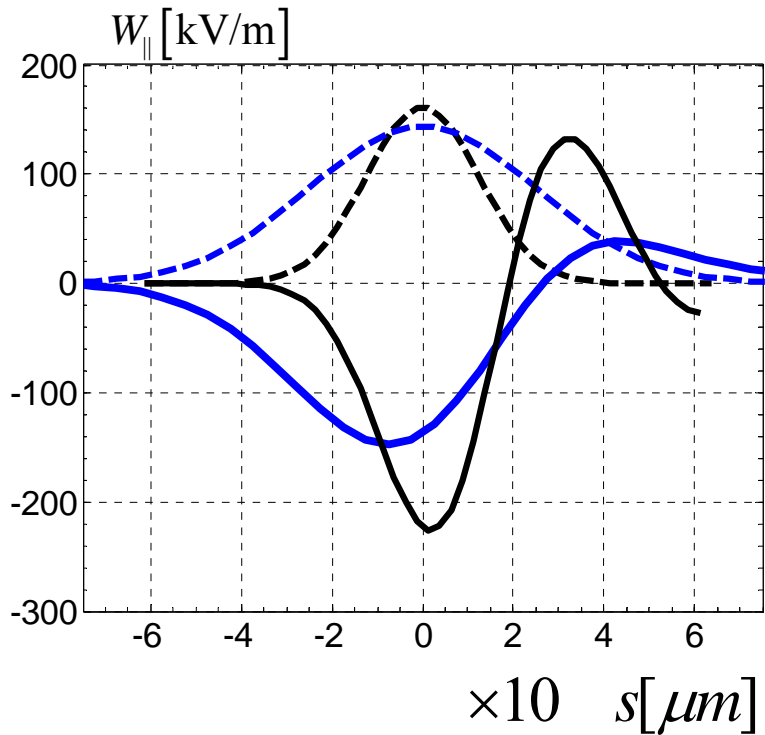
496

412 (365)



**+40%**



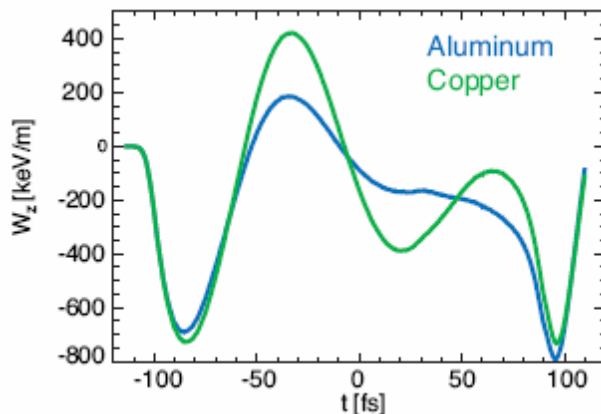
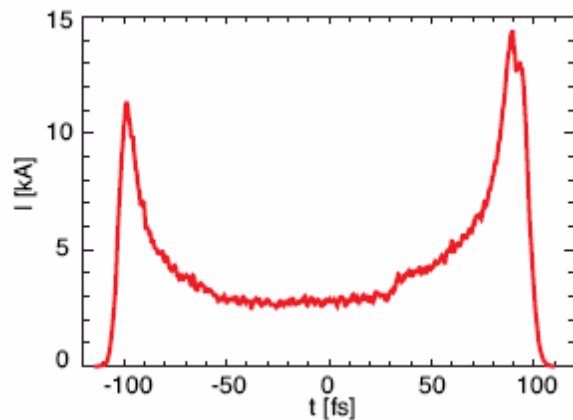


$$\delta_A = \frac{W_A L}{E \rho_1}$$

- fractional energy  
oscillation amplitude

	LCLS	XFEL SASE2 (q=1nC, sig=25mkm)	XFEL SASE2 (q=0.56nC, sig=12.5mkm)
$W_A$ , kV/m	200	140	220
L, m (L_sat)	100 (90)	200 (175)	200 (175)
E, GeV	14	17.5	17.5
$\rho_1$	3.2e-4	4e-4	4e-4
$\delta_A$	<b>4.5</b>	<b>4</b>	<b>6.3</b>

*K. Bane and G. Stupakov*



# TESLA-FEL Report 2005-10

$$\delta_A = 2.4, \rho = 7e-4 \quad \varepsilon = 0.7 \text{ mm*mrad!}$$

