

compensation of rf coupler kicks

1st attempt

previous investigations

calculation of coupler kicks

local compensation

not quite local compensation

global compensation

beam dynamics

summary and remarks



previous investigations

s2e-meeting 21.May 2007: Emittance Growth by RF Coupler Kicks

2005

Proceedings of 2005 Particle Accelerator Conference, Knoxville, Tennessee

STEERING AND FOCUSING EFFECTS IN TESLA CAVITY DUE TO HIGH ORDER MODE AND INPUT COUPLERS

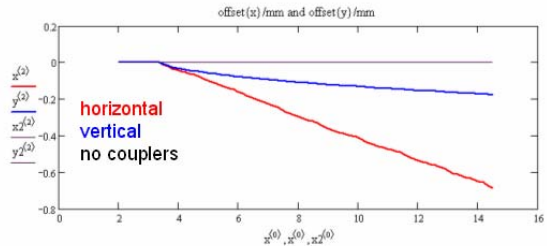
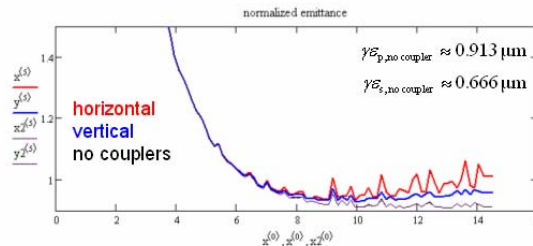
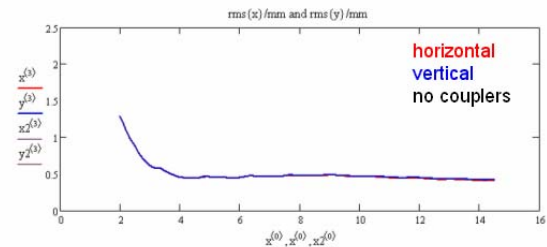
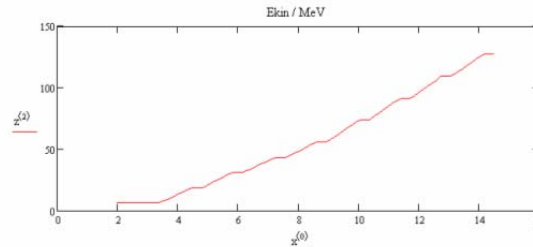
P. Piot, Fermi National Accelerator Laboratory, Batavia, IL 60510, USA,
 M. Dohlus, K. Flöttmann, M. Marx, S.G. Wurfel
 Deutsches Elektronen Synchrotron DESY, Hamburg, D-22603

IMPACT ON THE XFEL PHOTOINJECTOR

We present a practical example of the coupler-effect on the beam dynamics by considering the x-ray FEL photoinjector [5]. In the injector, the electron beam is pre-accelerated in an L-band ($f = 1.3$ GHz) rf-gun and directly injected into a standard TESLA-type accelerating module composed of eight cavities and accelerated to ~ 190 MeV. The first two cavities of the accelerating module are operated with $\hat{E}_z = 23$ MV/m and the remaining six cavities with $\hat{E}_z = 50$ MV/m. Figure 7 compares the beam parameter evolutions along the injector beamline from photocathode surface ($z = 0$) up to the end of the accelerating module. The field disturbances caused by the coupler result in a 16% and 1% relative emittance growth respectively in the horizontal and vertical plane. The induced steering results in beam displacements at the accelerating module exit of $|\delta x| = 680 \mu\text{m}$ and $|\delta y| = 170 \mu\text{m}$ and no significant $x - y$ coupling is observed.

$h=17\%$
 $v=1\%$

ASTRA calculation for ACC1



projected emittance

$$\frac{\mathcal{E}_{p,x}}{\mathcal{E}_{p, \text{no coupler}}} \approx 1.11 \quad \frac{\mathcal{E}_{p,y}}{\mathcal{E}_{p, \text{no coupler}}} \approx 1.051$$

slice emittance (center 10% charge)

$$\frac{\mathcal{E}_{s,x}}{\mathcal{E}_{s, \text{no coupler}}} \approx 1.028 \quad \frac{\mathcal{E}_{s,y}}{\mathcal{E}_{s, \text{no coupler}}} \approx 1.021$$



conclusions, questions

similar results as Philippe

growth of horizontal emittance in ACC1: projected 11%, slice 3%

1st order effect = offset independent field (centroid shift) 5.5%

2nd order effect = offset dependent field 5.7%, 2.8%

horiz. emittance growth to end of ACC2: projected 16%, slice 3%

s2e-meeting 21.May 2007: Beam Dynamics in Low Energy Part of XFEL Acc.
V. Tsakanov

Summary

- Coupler RF Field effects

ACCEL1 – 5-100 MeV

Emittance growth - 14 %

Linac 1 – 100-500 MeV

Emittance growth – 5%

- Other effects - below 1%



calculation of coupler kicks

the old MAFIA method

see: http://adweb.desy.de/~mpymax/mafia/HOM_Coupler/index.html

a lengthy procedure:
 about 10 MAFIA runs
 intermediate processing with fortran program
 final post processing with mathcad

TTF HOM Coupler

Documentation including a calculation procedure (pdf file, 5 pages) has been written by M. Dohlus.

Calculation downstream without coupler (reference file)

Commandfiles: Geometry [m.com](#)
 Running T3 [t3.com](#)
 Running P [psign.com](#) [pfnorm.com](#)

Output files [ezref.prn](#)

Note: T3 calculations have been done with magnetic boundary conditions in beam- (z-) direction.

Calculation downstream with coupler

The following tables give the results for different penetration depths of 6 and mm (zpen).

	downstream with coupler (old geometry)	downstream with coupler (new geometry)
zpen=6mm	Commandfiles:	Commandfiles:
	Running M m.com	Running M m.com
	Running E e.com	Running E e.com
	Running T3 t3.com	Running T3 t3.com
	Running P psign.com	Running P psign.com
	pfnorm.com	pfnorm.com
	pfield.com	pfield.com
	MAFIA output files prn.zip	MAFIA output files prn.zip
	Pictures not available	Pictures 2d y-cut 2d z-cut
		3d-plot

calculation downstream with coupler

```

m.com (icoup=1, idown=1)
e.com
t3.com
psign.com
fortran.exe
reader.mcd check power and envelope
pnorm.com
def fref=... (from fresult.dat)
--> enre.enim (normalized to enor=50MV/m)
bre=0.5*(brea+breb), bim=...
--> bnre.bnim
load reference solution (erefr.erefim.brefre.brefim)
subtract reference field, invert time
esre:=(enre-erefr)
esim:=- (enim-erefim)
bsre:=- (bnre-brefre)
bsim:=- (bnim-brefim)
pfield.com
fortran_fields.exe
reader_fields.mcd calculate kick ...
                    
```

calculation downstream without coupler

```

m.com (icoup=0, idown=1)
t3.com ($ material=3, $ #waveguide section)
psign.com
fortran.exe
reader.mcd check power and envelope
pfnorm.com
def fref=... (from fresult.dat)
--> enre.enim (normalized to enor=50MV/m)
bre=0.5*(brea+breb), bim=...
--> bnre.bnim
                    
```

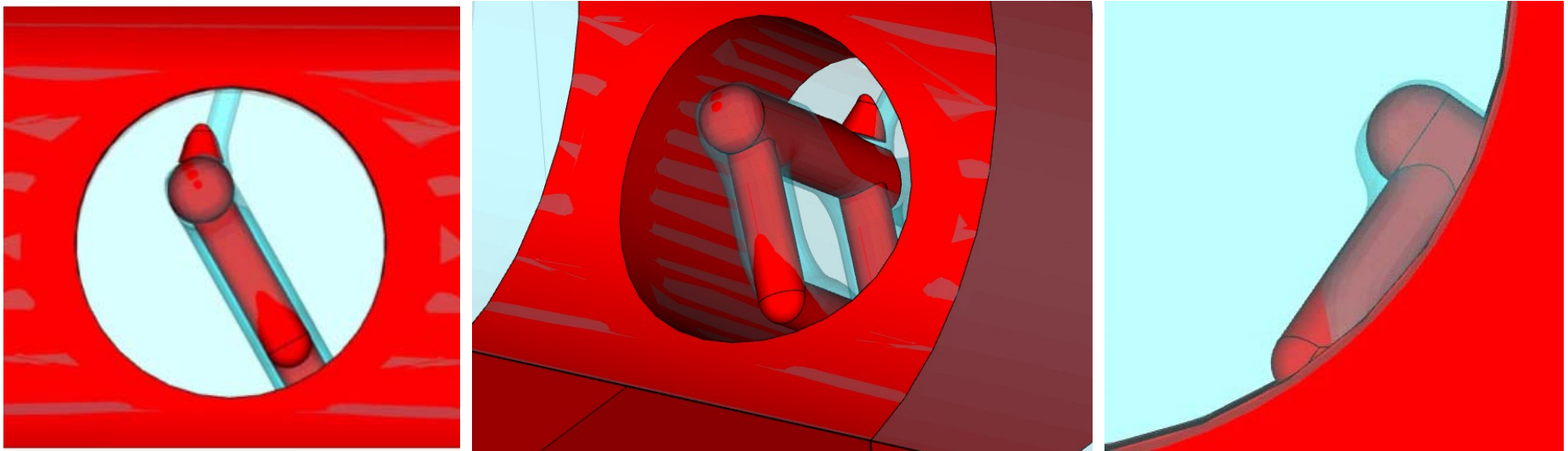
Note: A pink box highlights 'enre.enim' and 'bnre.bnim' in the code blocks, with an arrow pointing from the 'load reference solution' line in the left block to the 'bnre.bnim' line in the right block.



calculation of coupler kicks

mode of operation: steady state, pure forward wave, $z_{\text{pen}}=6\text{mm} \rightarrow Q_e \approx 3.5\text{E}6$
kick from input coupler depends
on forward and backward waves!

the old main and HOM coupler geometry



comparison with FNAL geometry (report Lunin, Solyak, Yakolev)
the actual DESY geometry is probably similar

old / FNAL

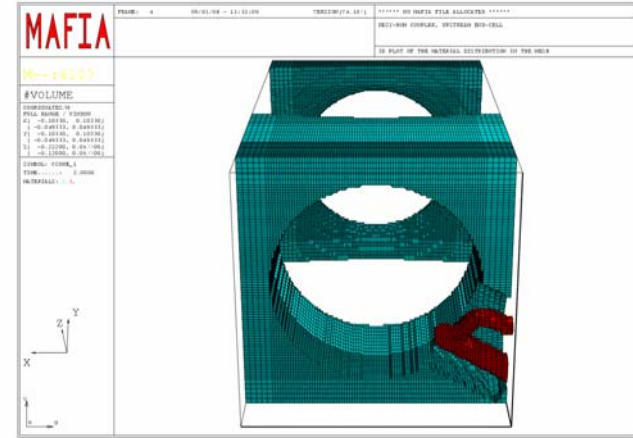
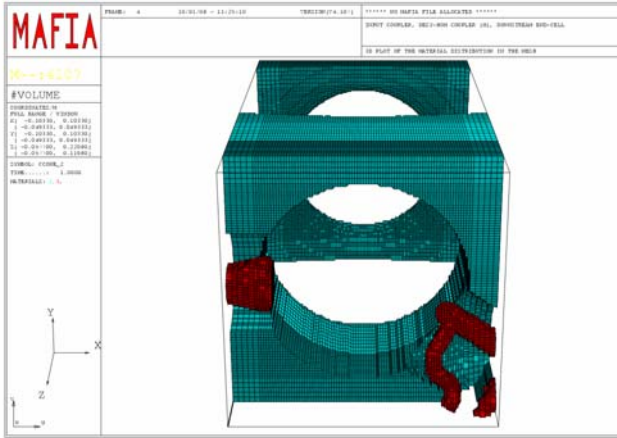
everything could be done better

discretization
field calculation but more time consuming!



calculation of coupler kicks

existing version



TTF coupler, downstream, new geometry, zpen=6mm

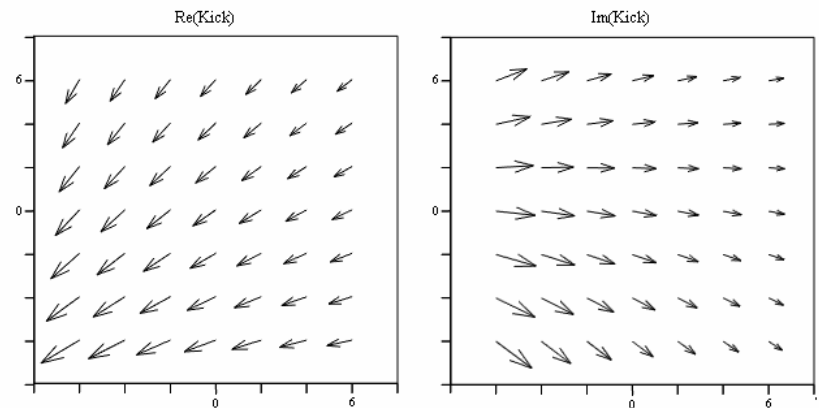
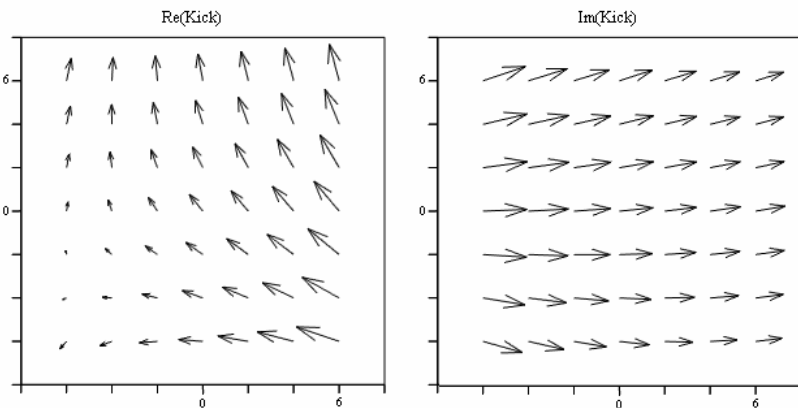
center: $\frac{V_{x,ij}}{V_z} \cdot 10^6 = -24.238 + 53.968i$

$\frac{V_{y,ij}}{V_z} \cdot 10^6 = 31.301 + 5.483i$

TTF coupler, upstream

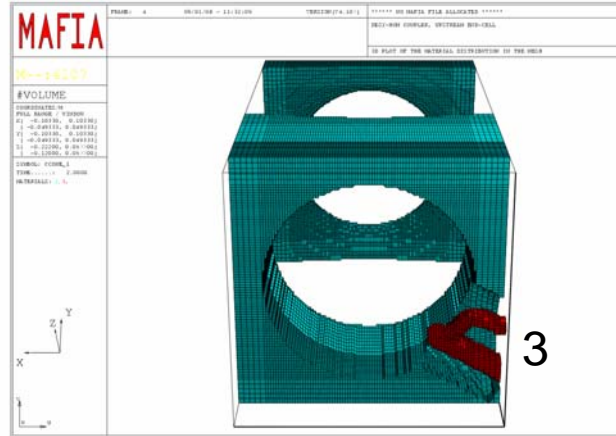
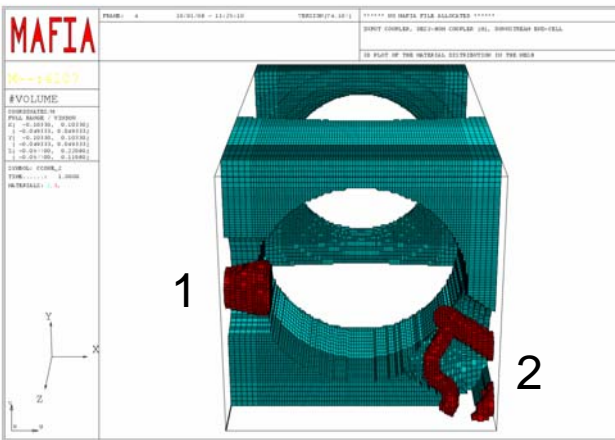
center: $\frac{V_{x,ij}}{V_z} \cdot 10^6 = -59.399 + 9.412i$

$\frac{V_{y,ij}}{V_z} \cdot 10^6 = -43.459 - 1.833i$

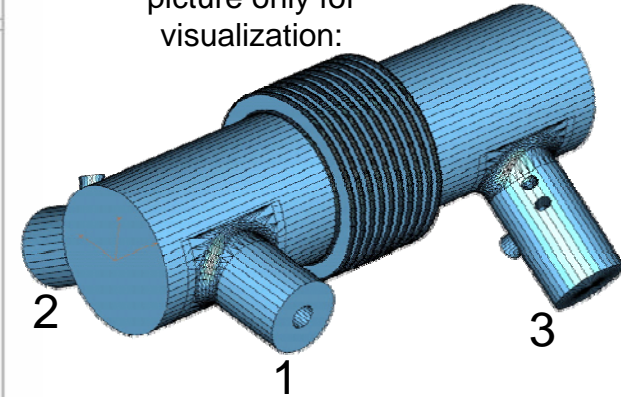


calculation of coupler kicks

existing version (all couplers together)



picture only for visualization:



new geometry, zpen=6mm

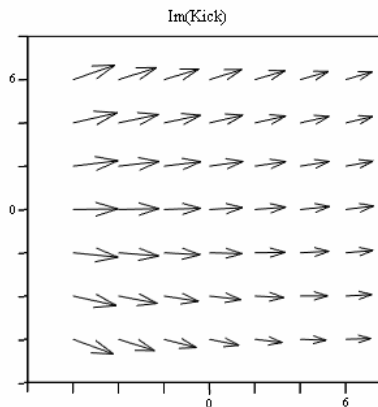
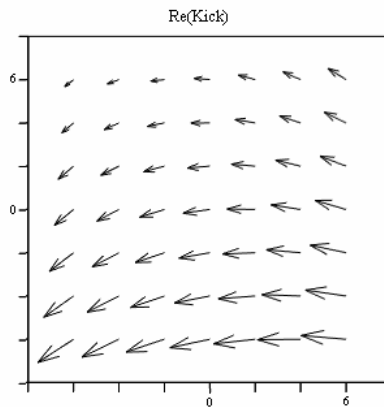
center:
(both)

$$v_{x_{i,j}} \cdot 10^6 = -83.657 + 63.38i$$

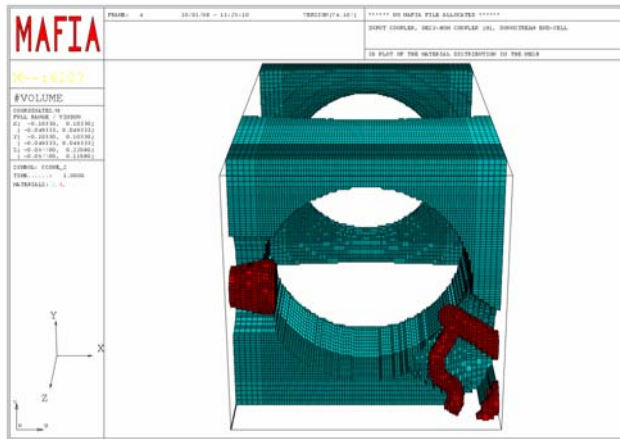
$$v_{y_{i,j}} \cdot 10^6 = -12.158 + 3.65i$$

name1 = "kick_upstream_kick.dat"

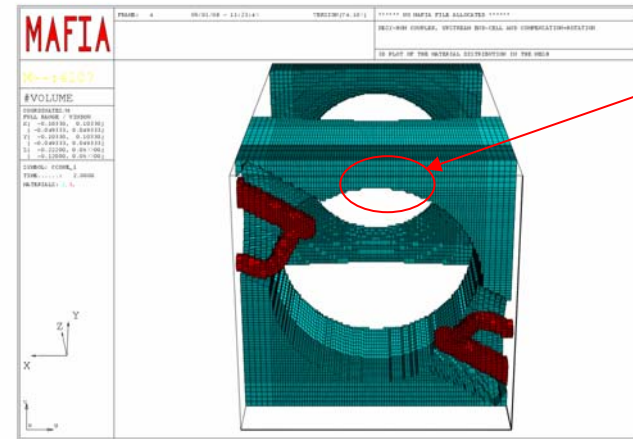
name2 = "kick_downstream_kick.dat"



(downstream = unchanged)



(upstream with compensation)



E sensor

real or virtual
2nd HOM coupler

TTF coupler, downstream, new geometry, zpen=6mm

center: $\frac{V_{x,ij}}{V_z} \cdot 10^6 = -24.238 + 53.968i$

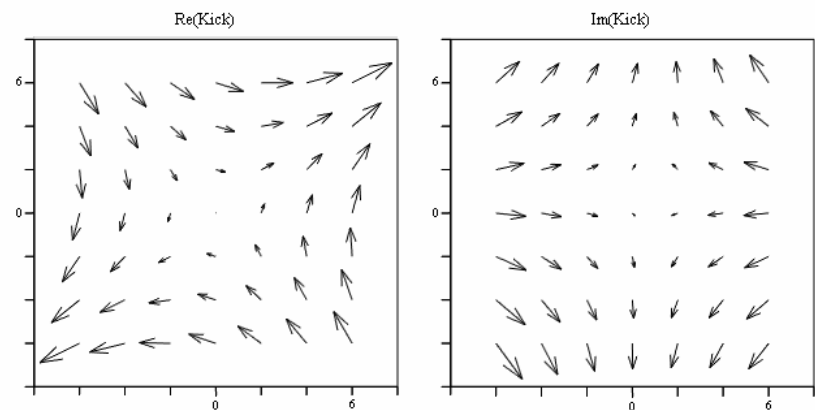
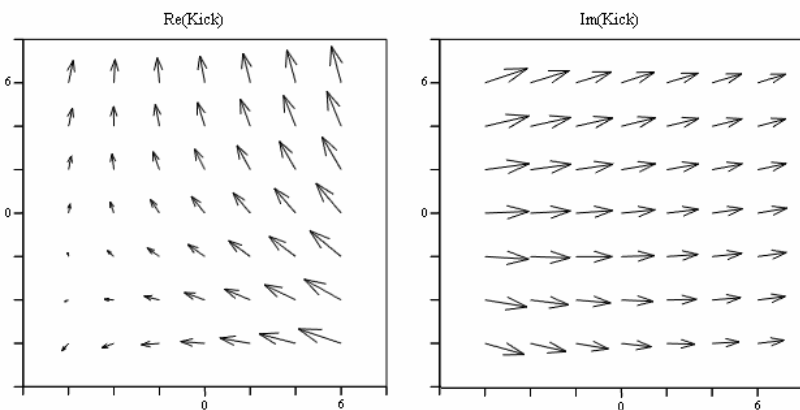
$\frac{V_{y,ij}}{V_z} \cdot 10^6 = 31.301 + 5.483i$

TTF coupler, upstream

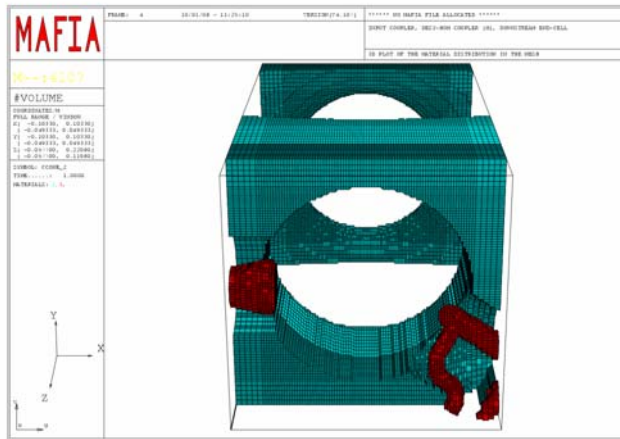
center: $\frac{V_{x,ij}}{V_z} \cdot 10^6 = 0.482 + 0.852i$

$\frac{V_{y,ij}}{V_z} \cdot 10^6 = 0.569 - 0.997i$

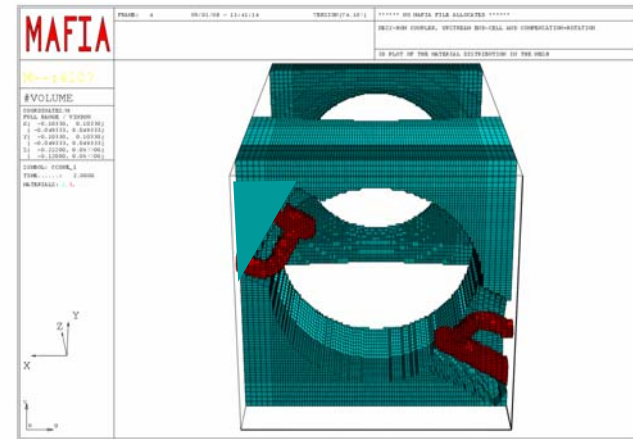
not perfect due to
numerical errors!



(downstream = unchanged)



(upstream with compensation)



virtual 2nd HOM coupler
reduced length

TTF coupler, downstream, new geometry, zpen=6mm

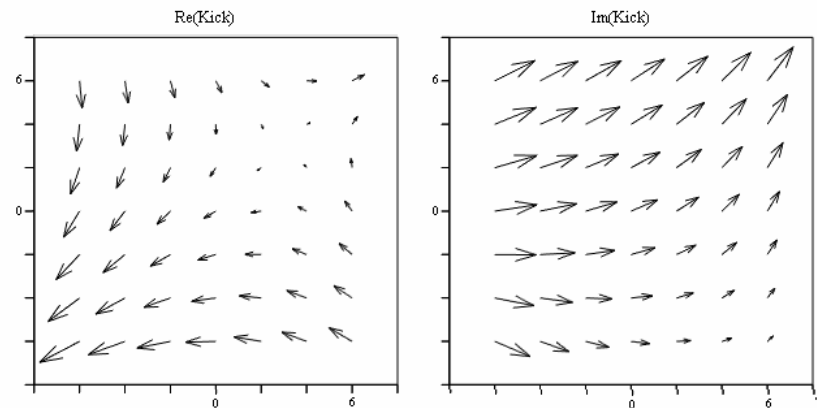
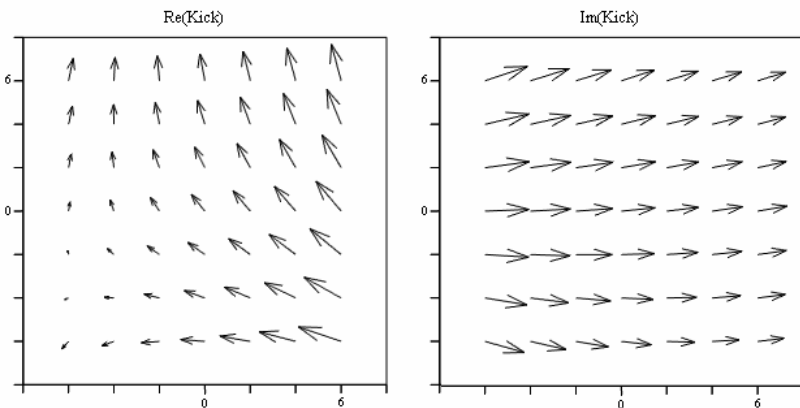
center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = -24.238 + 53.968i$

$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = 31.301 + 5.483i$

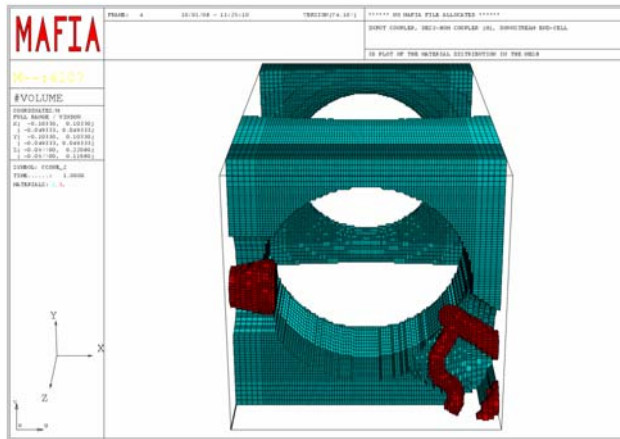
TTF coupler, upstream

center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = -22.521 + 11.54i$

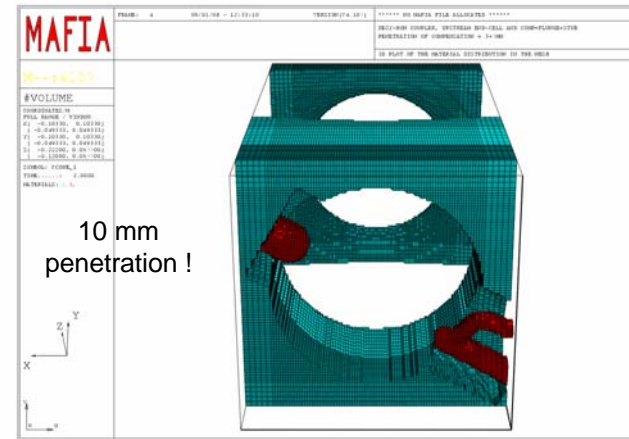
$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = -14.089 + 5.138i$



(downstream = unchanged)



(upstream with compensation)



TTF coupler, downstream, new geometry, zpen=6mm

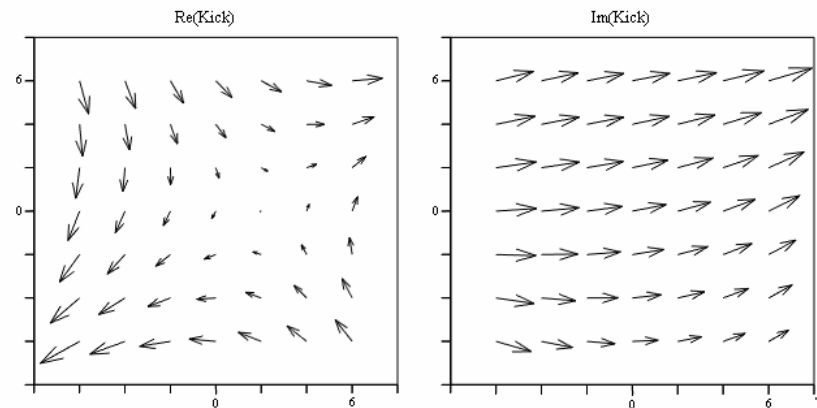
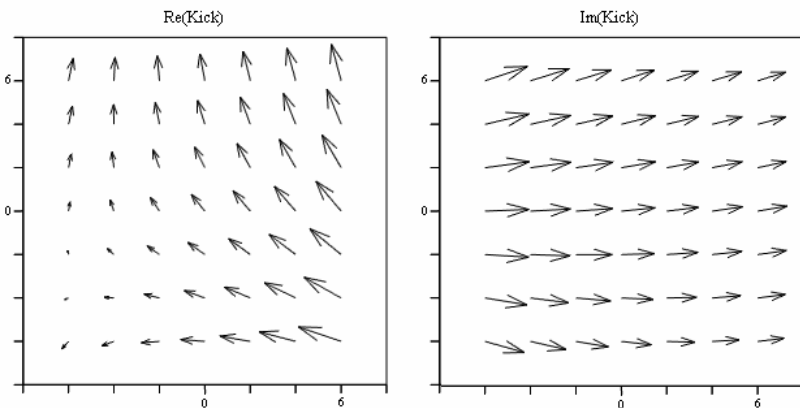
center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = -24.238 + 53.968i$

$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = 31.301 + 5.483i$

TTF coupler, upstream

center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = -6.925 + 19.794i$

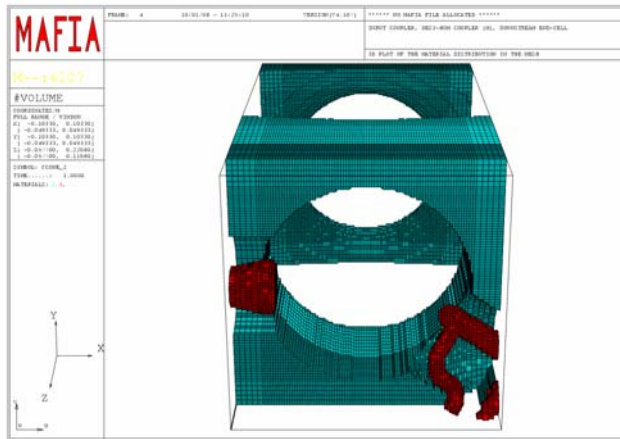
$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = -13.043 + 3.994i$



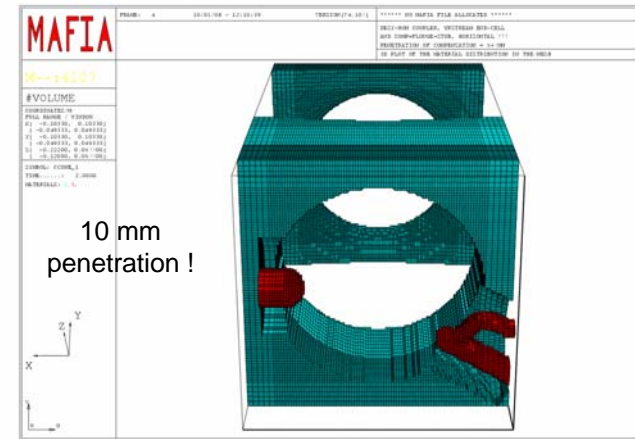
not quite local compensation

version 1
reduce real part of sum

(downstream = unchanged)



(upstream with compensation)



TTF coupler, downstream, new geometry, zpen=6mm

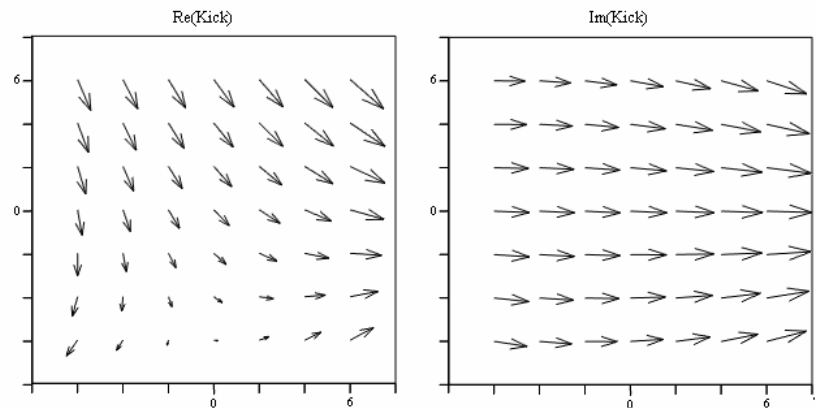
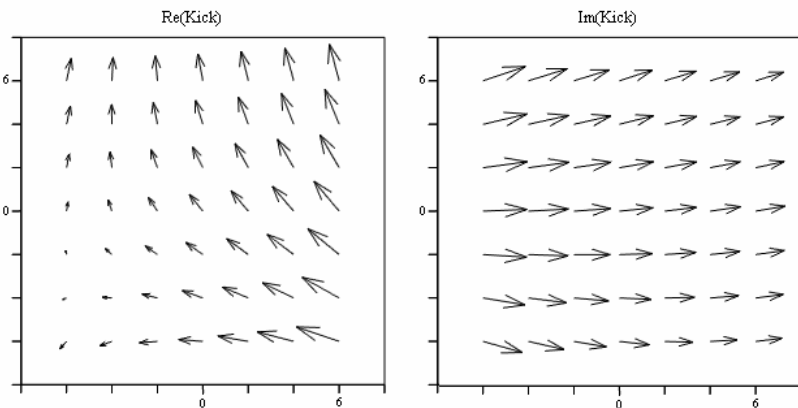
center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = -24.238 + 53.968i$

$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = 31.301 + 5.483i$

TTF coupler, upstream

center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = 39.961 + 37.917i$

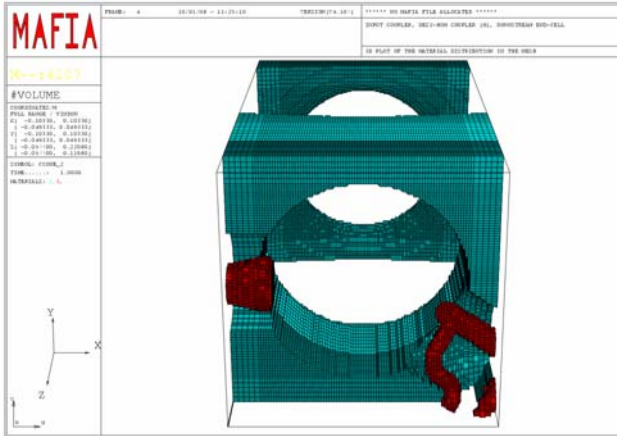
$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = -42.745 - 1.84i$



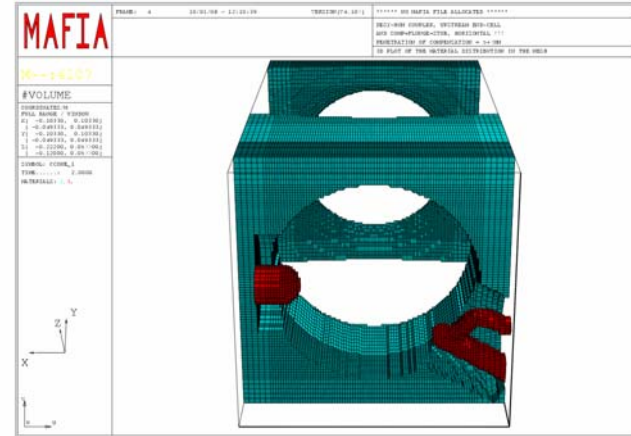
not quite local compensation

version 1
reduce real part of sum

(downstream = unchanged)



(upstream with compensation)



new geometry, zpen=6mm

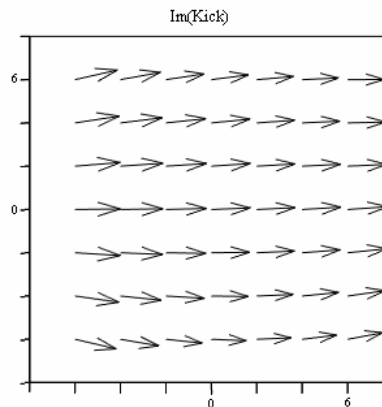
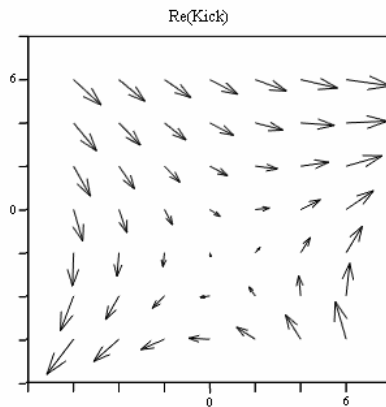
center:
(both)

$$vx_{i,j} \cdot 10^6 = 15.703 + 91.885i$$

$$vy_{i,j} \cdot 10^6 = -11.444 + 3.644i$$

name1 = "kick_upstream_comp8.dat"

name2 = "kick_downstream_kick.dat"

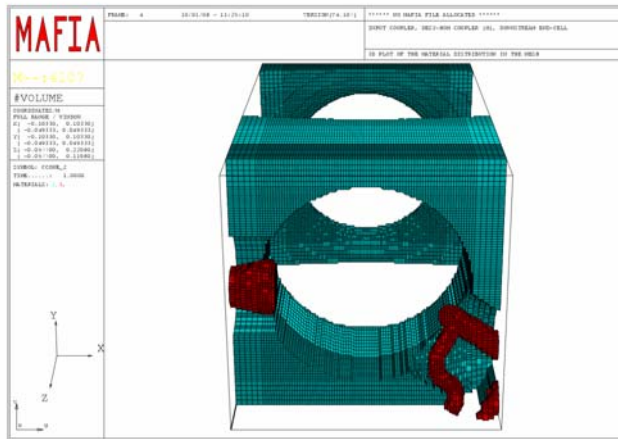


not quite local compensation

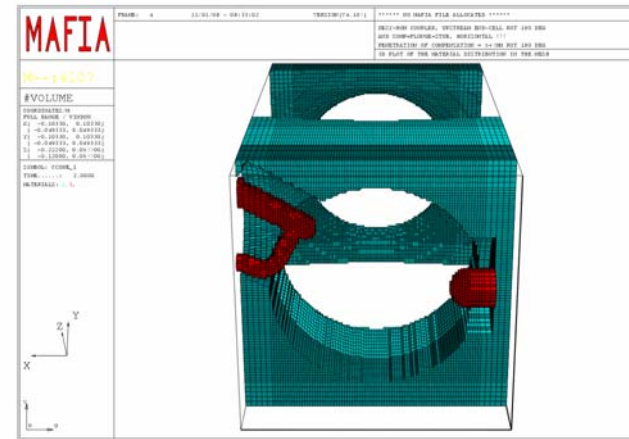
version 2

reduce imaginary part of sum

(downstream = unchanged)



(upstream with compensation)



TTF coupler, downstream, new geometry, zpen=6mm

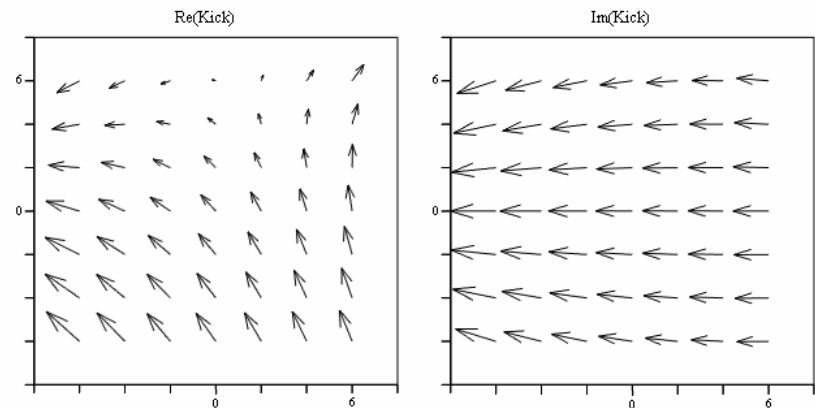
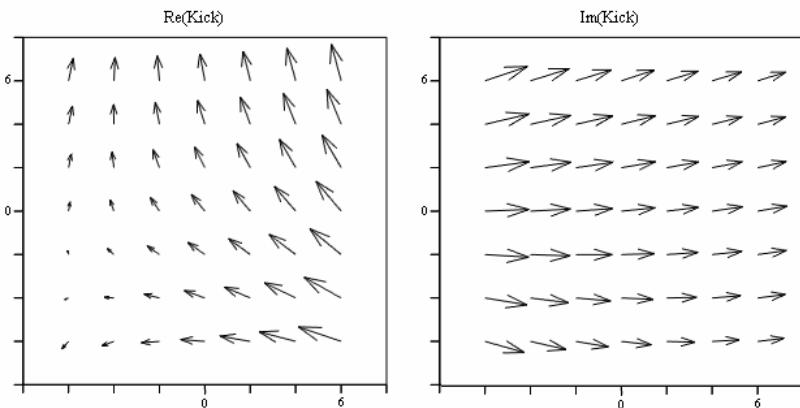
center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = -24.238 + 53.968i$

$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = 31.301 + 5.483i$

TTF coupler, upstream

center: $\frac{V_{x_{i,j}}}{V_z} \cdot 10^6 = -38.587 - 36.233i$

$\frac{V_{y_{i,j}}}{V_z} \cdot 10^6 = 43.788 + 0.351i$



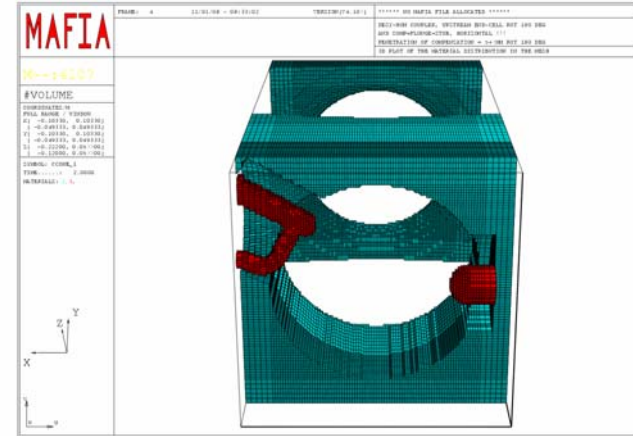
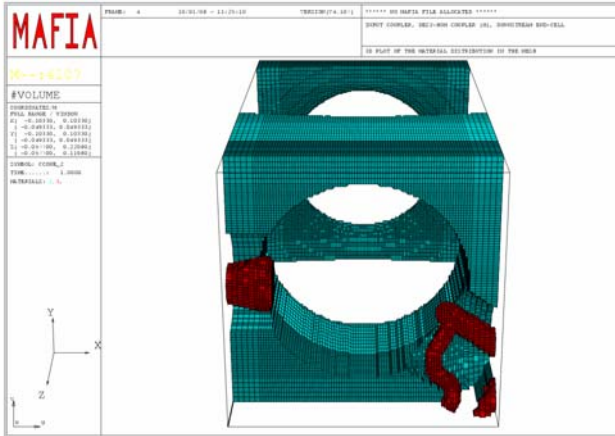
not quite local compensation

version 2

reduce imaginary part of sum

(downstream = unchanged)

(upstream with compensation)



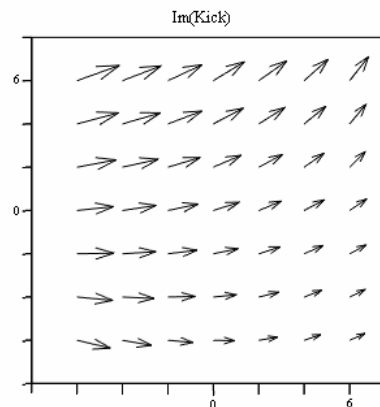
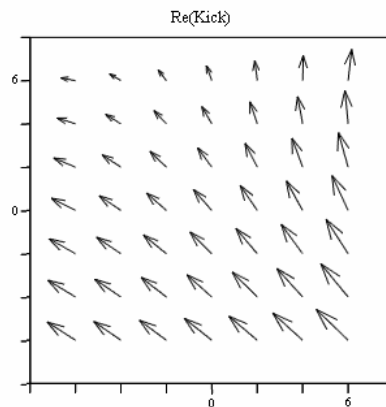
new geometry, zpen=6mm

center:
(both) $vx_{i,j} \cdot 10^6 = -62.845 + 17.735i$

$vy_{i,j} \cdot 10^6 = 75.089 + 5.835i$

name1 = "kick_upstream_comp9.dat"






name2 = "kick_downstream_kick.dat"



global compensation

simple geometry transformations: rotation- or mirror-transformation

general discussion in: <http://www.desy.de/~dohlus/2007/2007.07.ckick/>

summary – complex coupler kick:		
cav		a, b arbitrary: $d_0 = d_0(a, b), \dots$ $V_x^{(0)}(x, y) \approx d_0 + d_x x + d_y y$ $V_y^{(0)}(x, y) \approx f_0 + f_x x + f_y y$
cav+mirror-z		SW: a=b, (equal for sub-structures) $V_x^{(z,0)}(x, y) \approx 2i \operatorname{Im}\{d_0 + d_x x + d_y y\}$ $V_y^{(z,0)}(x, y) \approx 2i \operatorname{Im}\{f_0 + f_x x + f_y y\}$
cav+rot y-axis		SW: a=b, (equal for sub-structures) $V_x^{(z,0)}(x, y) \approx 2\operatorname{Re}\{d_0\} + 2i \operatorname{Im}\{d_x\}x + 2\operatorname{Re}\{d_y\}y$ $V_y^{(z,0)}(x, y) \approx 2i \operatorname{Im}\{f_0\} + 2\operatorname{Re}\{f_x\}x + 2i \operatorname{Im}\{f_y\}y$
cav+mirror-y		a, b arbitrary (but equal for sub-str.) $V_x^{(z,0)}(x, y) \approx 2d_x x$ $V_y^{(z,0)}(x, y) \approx 2f_0 + 2f_y y$
cav+rot z-axis		a, b arbitrary (but equal for sub-str.) $V_x^{(z,0)}(x, y) \approx 2d_x x + 2d_y y$ $V_y^{(z,0)}(x, y) \approx 2f_x x + 2f_y y$

redesign of distribution network and cryostat

one side distribution network

two side distribution network

same or similar arguments for rf-fields and wake-fields

different energy at kick and compensating kick

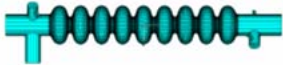

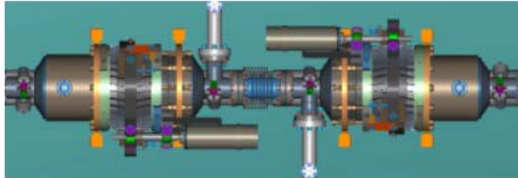
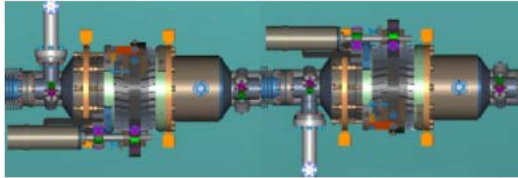

→ is global compensation possible at the very low energy of ACC1?



global compensation

general discussion (standard modules / 3rd harm. modules)

see: <http://www.desy.de/~dohlus/2007/2007.07.ckick/>

summary – complex coupler kick:	
<p>cav</p> 	<p>a, b arbitrary: $d_0 = d_0(a, b), \dots$</p> $V_x^{(\Sigma, n)}(x, y) \approx d_0 + d_x x + d_y y$ $V_y^{(\Sigma, n)}(x, y) \approx f_0 + f_x x + f_y y$
<p>cav+mirror-z</p> 	<p>SW: a=b, (equal for sub-structures)</p> $V_x^{(\Sigma, n)}(x, y) \approx 2i \operatorname{Im}\{d_0 + d_x x + d_y y\}$ $V_y^{(\Sigma, n)}(x, y) \approx 2i \operatorname{Im}\{f_0 + f_x x + f_y y\}$
<p>cav+rot y-axis</p> 	<p>SW: a=b, (equal for sub-structures)</p> $V_x^{(\Sigma, n)}(x, y) \approx 2\operatorname{Re}\{d_0\} + 2i \operatorname{Im}\{d_x\}x + 2\operatorname{Re}\{d_y\}y$ $V_y^{(\Sigma, n)}(x, y) \approx 2i \operatorname{Im}\{f_0\} + 2\operatorname{Re}\{f_x\}x + 2i \operatorname{Im}\{f_y\}y$
<p>cav+mirror-y</p> 	<p>a, b arbitrary (but equal for sub-str.)</p> $V_x^{(\Sigma, n)}(x, y) \approx 2d_x x$ $V_y^{(\Sigma, n)}(x, y) \approx 2f_0 + 2f_y y$
<p>cav+rot z-axis</p> 	<p>a, b arbitrary (but equal for sub-str.)</p> $V_x^{(\Sigma, n)}(x, y) \approx 2d_x x + 2d_y y$ $V_y^{(\Sigma, n)}(x, y) \approx 2f_x x + 2f_y y$

} no on crest kick
 phase dep. kick,
 position dep.

} systematic kick
 no phase dep. kick
 position dep.

} no kick on axis
 position dep.



beam dynamics

complicated mechanism of emittance growth

emittance compensation schema

strong variation of energy and transverse beam size

spatial and temporal dependency of coupler fields

$$V_x^{(n)}(x, y) \approx d_0 + d_x x + d_y y \rightarrow \Delta p_{x,v} \approx \text{Re}\{V_x^{(n)}(x_v, y_v) \cdot \exp(i\omega t_v)\}$$

$$V_y^{(n)}(x, y) \approx f_0 + f_x x + f_y y \rightarrow \Delta p_{y,v} \approx \text{Re}\{V_y^{(n)}(x_v, y_v) \cdot \exp(i\omega t_v)\}$$

steering effects of coupler fields

it is not clear what type of compensation is needed

is the emittance growth driven by spatial or temporal dependency? ...

further ASTRA calculations are required

procedure is lengthy, the risk of mistakes is considerable

simplified and/or standardized procedure desirable

1st order Taylor expansion of kick parameter → analytic theory

1st order Taylor expansion of kick parameter → generic coupler field → efficient BD simulation

use of glue-track?



summary and remarks

local- or quasi-local compensation: fixed (not tunable) reactive element
partial compensation of some effects

clarify operational conditions, limitation of tuning ranges bunch currents
and bunch charges

optimal geometry for rf induced kicks is not necessarily identical
with geometry for minimal wake field effects → simultaneous investigation

global compensation: does it work in principle?

strong geometrical constraints: tuner (local)
cryostat (in general)
E sensor

further BD simulations required: lengthy
improved or simplified method
driving terms of emittance growth

