



# Impedance Budget from LINAC to SASE2

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Beam Dynamics Group Meeting

3.12.07

overview

wake sources = geometric & resistive (=surface effects)

definitions (average & rms)

collimator: geometric, surface effects, all ~40%

pipe: surface effects ~40%

kicker: geometric, surface effects, all ~20%

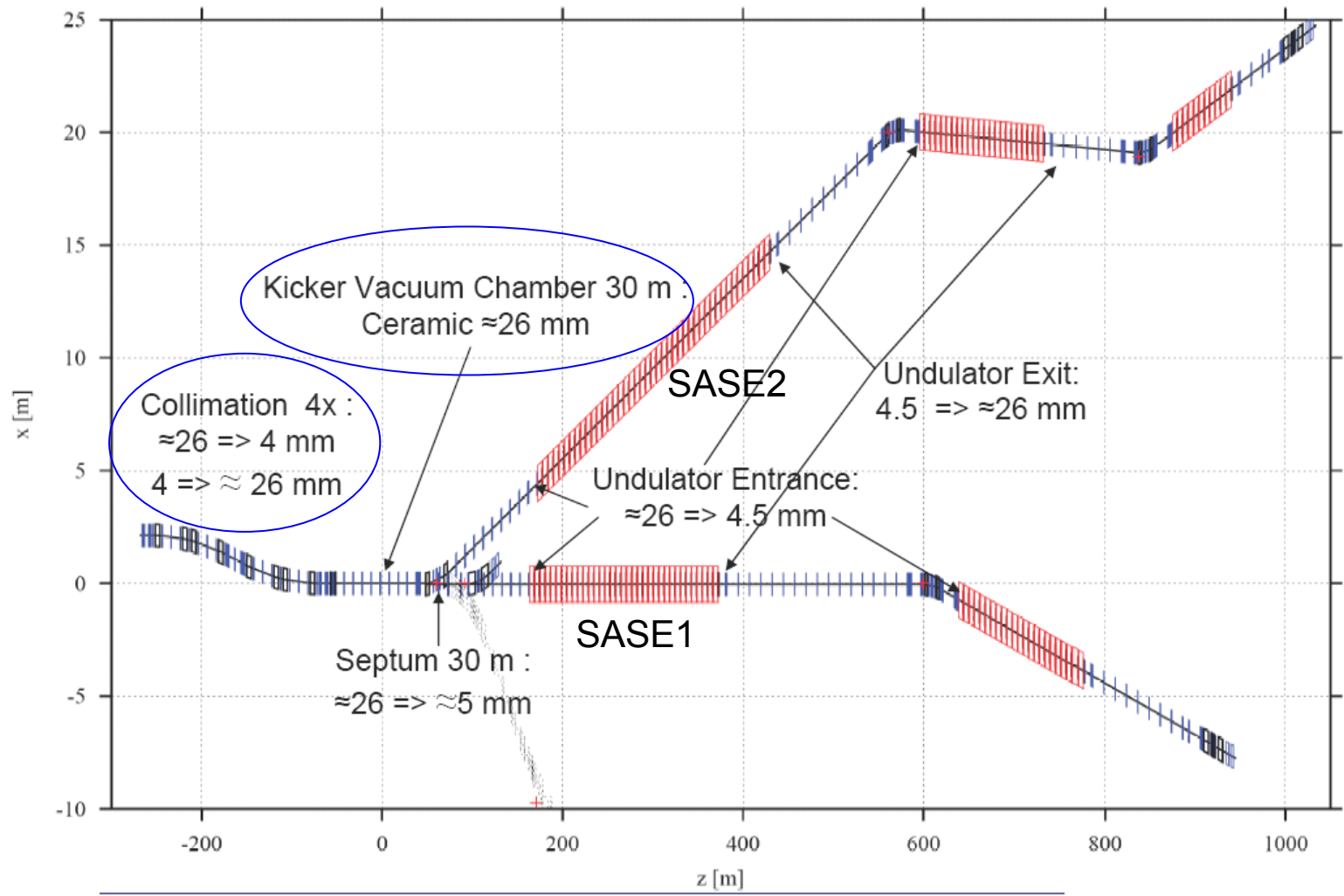
total

total vs. pipe radius

comparison with effects in LINAC

comparison with SASE2 ~SASE2 / 2

total vs. pipe radius normalized to SASE2

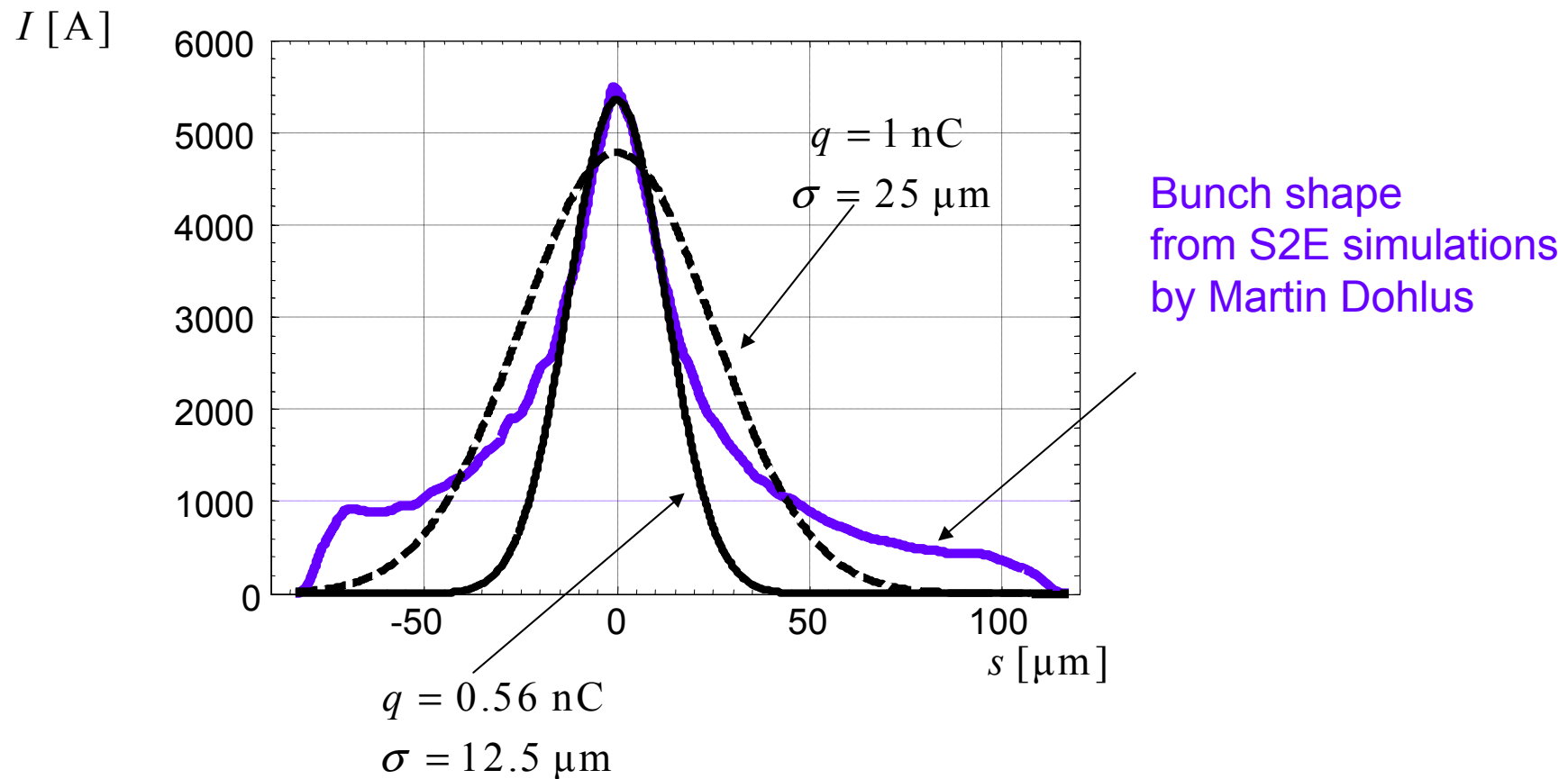


	Length [m]	# of Quads	Aperture Radius [mm]	Other Insertions
Linac to SASE2	486	63	25	4 Collimators (2-4 mm aperture) 30 m Ceramic (10 mm aperture) 2 bifurcation/septum chambers

(W.Decking)

## Wakefield sources

- Resistance of the pipe ( $r \sim 20$  mm,  $L=456$  m, Aluminium)
- Collimators ( $r=2$  mm,  $L=50$  cm, 4 items, TIMETAL 6-4 )
- Kickers ( $r=10$  mm,  $L=10$  m, 3 items,  $R/L=10\Omega/m$  )

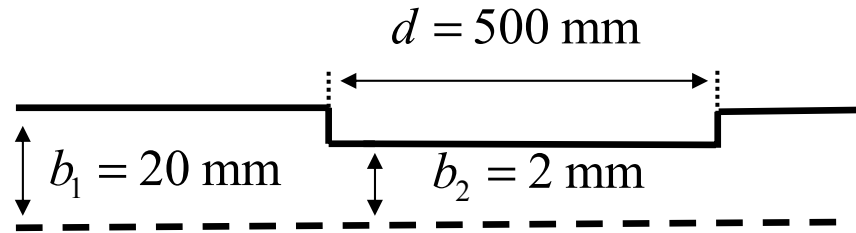


$\lambda(s)$  – bunch shape

$$Q^2 \langle W \rangle = Q^2 \int W(s) \lambda(s) ds \text{ – energy loss}$$

$$Q^2 \langle (W - \langle W \rangle)^2 \rangle^{0.5} = Q^2 \left[ \int (W(s) - \langle W \rangle)^2 \lambda(s) ds \right]^{0.5} \text{ – energy spread}$$

## Collimator (geometrical wake)



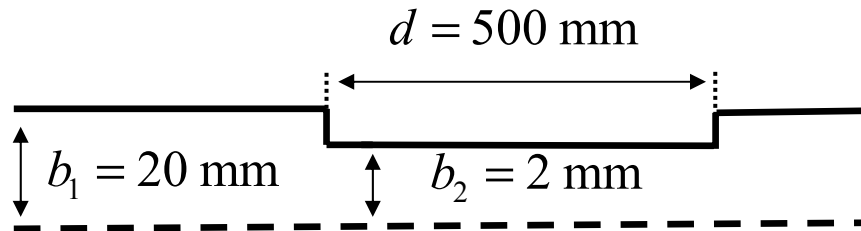
$$QW(s) = Z_{\parallel} I(s) \quad Z_{\parallel} = 276 [\Omega]$$

$$Z^e(0) = \frac{Z_0}{2\pi} \ln \left( \frac{b_1}{b_2} \right) \quad Z_{\parallel} = 2Z^e(0)$$

Optical approximation: the geometrical wake repeats the bunch shape.

## Collimator (resistive wake)

<http://www.timet.com/timetal6-4frame.html>



TIMETAL 6-4 alloy (Titanium)  
(E.Schutz MVA)

$$\sigma = 0.6 \cdot 10^6 \Omega^{-1} m^{-1}$$

$$\tau = 0 [\text{sec}]$$

$$\Delta_{\text{rough}} = 300 [\text{nm}]$$

$$\Delta_{\text{oxid}} = 5 [\text{nm}]$$

$$Z(\omega) = \frac{Z_s(\omega)}{2\pi R} \left[ 1 + i \frac{\omega R}{c} \frac{Z_s(\omega)}{Z_0} \right]^{-1}$$

$$Z_s(\omega) = Z_s^\sigma(\omega) + Z_s^L(\omega)$$

$$Z_s^\sigma(\omega) \approx \sqrt{\frac{i\omega\mu}{\sigma(\omega)}}$$

$$\sigma(\omega) \approx \frac{\sigma_0}{1 + i\omega\tau}$$

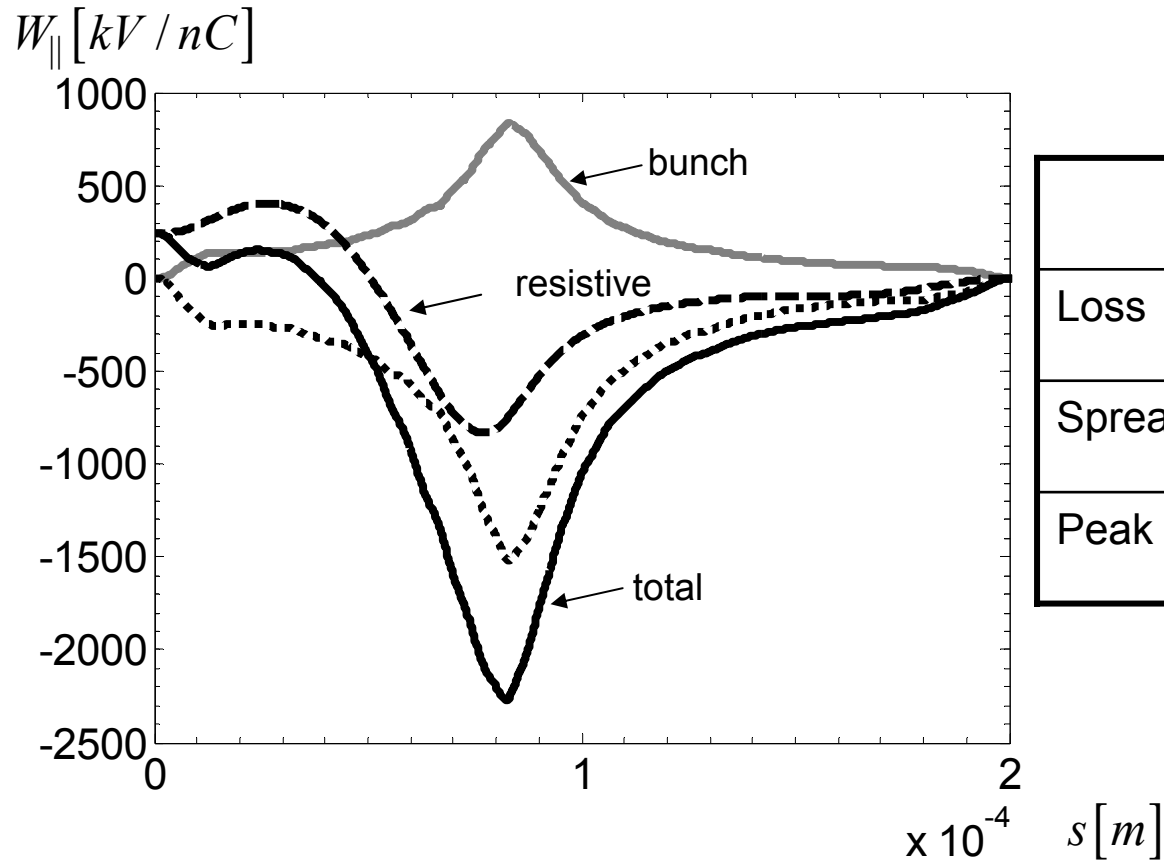
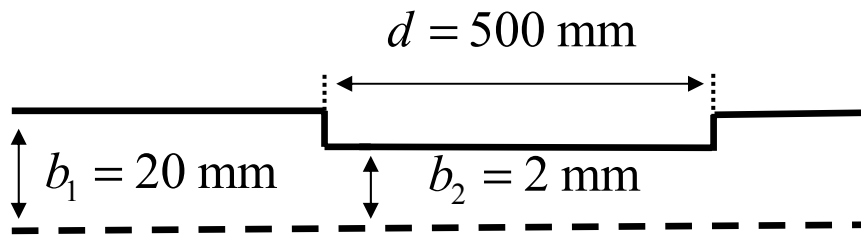
$$Z_s^L(\omega) \approx i\omega L$$

$$L \approx 0.5\mu(\Delta_{\text{oxid}} + 0.02\Delta_{\text{rough}})$$

M.Dohlus. TESLA 2001-26, 2001

K.L.F.Bane, G.V.Stupakov, SLAC-PUB-10707, 2004

# Collimator

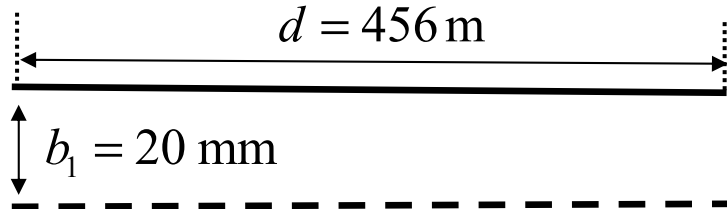


	$kV / nC$		
	Geom.	Res.	Total
Loss	754	332	1086
Spread	457	365	791
Peak	-1518	-833	-2272



(T.Wohlenberg)

### Pipe (resistive+oxid layer+roughness)



**Materialauswahl:** zu erwartende Oxidschicht:  
Aluminium: 5nm  
Kupfer: nach 10min ca. 1nm bis 5nm  
Gold: Annahme 0nm

### Aluminium

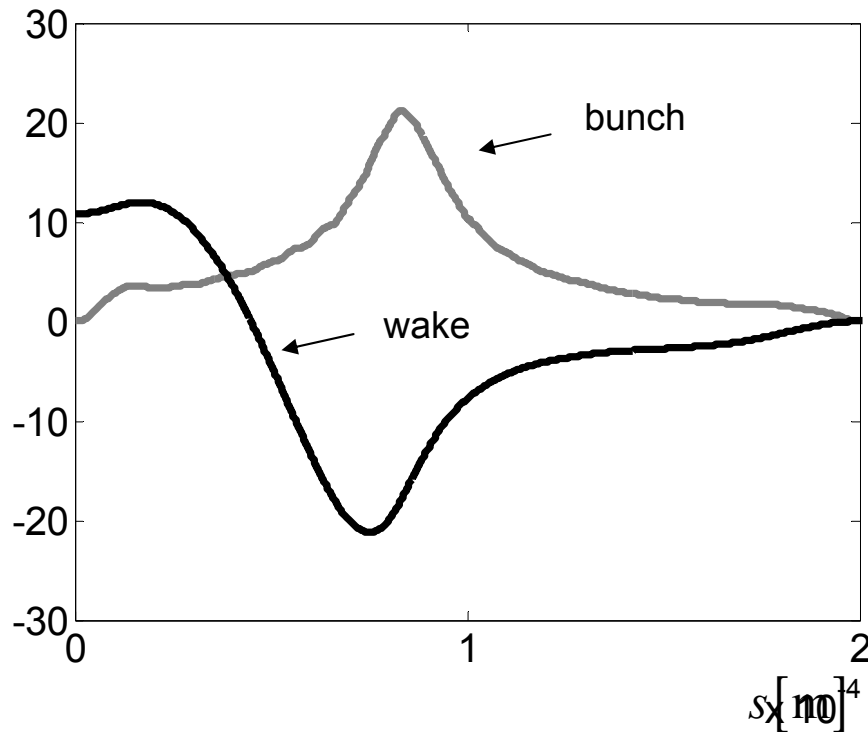
$$\sigma = 3.66 \cdot 10^7 \Omega^{-1} m^{-1}$$

$$\tau = 7.1 \cdot 10^{-15} [\text{sec}]$$

$$\Delta_{rough} = 300 [\text{nm}]$$

$$\Delta_{oxid} = 5 [\text{nm}]$$

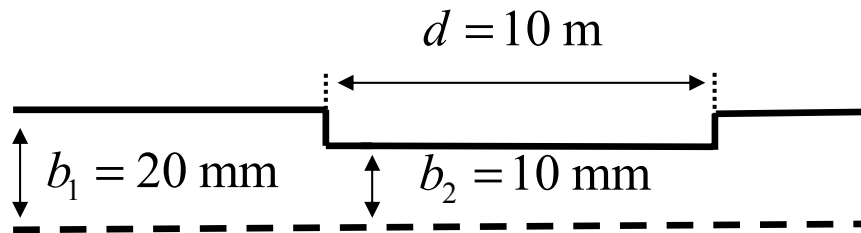
$W_{||} [\text{kV/nC/m}]$



$kV / nC / m$

	resistive	total
Loss	8.4	9.0
Spread	8.5	9.3
Peak	-19.8	-21

## Kicker (geometrical wake)



$$QW(s) = Z_{\parallel} I(s)$$

$$Z_{\parallel} = 110 [\Omega]$$

$$Z_{\parallel} = 2Z^e(0)$$

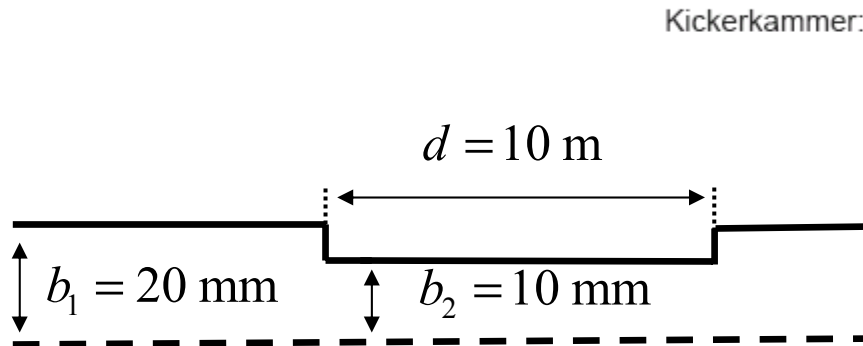
$$Z^e(0) = \frac{Z_0}{2\pi} \ln \left( \frac{b_1}{b_2} \right)$$

Kickerkammer:

**Verzweigungsstrecke:** (T.Wohlenberg)

Keramikrohr mit titanstabilisierten Edelstahl beschichtet, Schichtdicke ca  $0,7 \mu\text{m}$ . Elektrischer Widerstand gemessen über die Rohrlänge beträgt 10-12 Ohm/Meter. Die Kammerlänge beträgt ca. 900mm der Innendurchmesser beträgt ca.20mm.

## Kicker (resistive wake)



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$$\rho = 12 \frac{\Omega}{\text{m}} \cdot 4.4 \cdot 10^{-8} \text{ m}^2 = 0.53 \cdot 10^{-6} \Omega \text{ m}$$

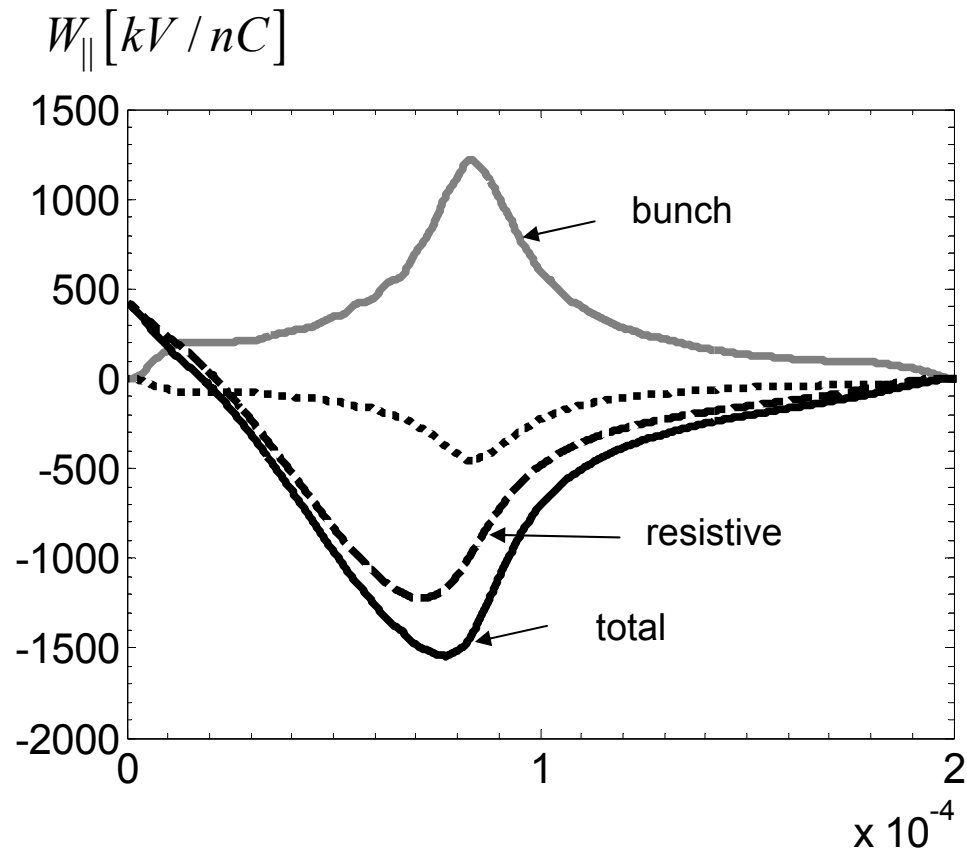
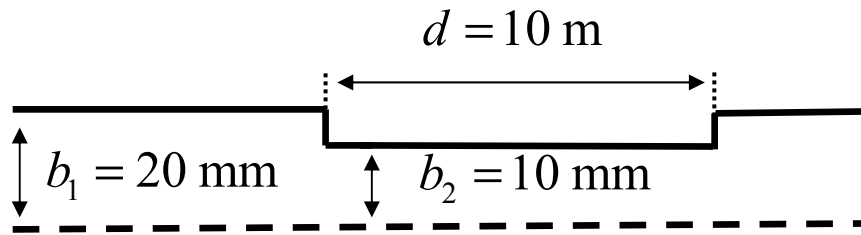
$$\sigma = 1.9 \cdot 10^6 \Omega^{-1} \text{ m}^{-1}$$

$$\tau = 2.4e-15 [\text{sec}]$$

$$\Delta_{\text{rough}} = 300 [\text{nm}]$$

$$\Delta_{\text{oxid}} = 5 [\text{nm}]$$

# Kicker



$kV/nC$

	Geom.	Res.	Total
Loss	227	659	886
Spread	137	412	519
Peak	-457	-1222	-1544

# *A. Tsakanian*

## • Tube with finite thickness

B. Zotter, S. Kheifets, 1997.

Method: matching technique

Problem: fields are diverges in outer space for  $\gamma \rightarrow \infty$

## • Usual Approach

A.W. Chao, SLAC-PUB- 2946, 1982  
A. Piwinski, DESY-94-068, 1994

skin-depth < tube thickness



Tube with infinite thickness

## • Solution in General Case



- Analytical solution for the fields inside tube for finite Lorenz factor*
- Perform the ultrarelativistic limit*

M. Ivanyan, A. Tsakanian, Phys. Rev. ST-AB, 2006

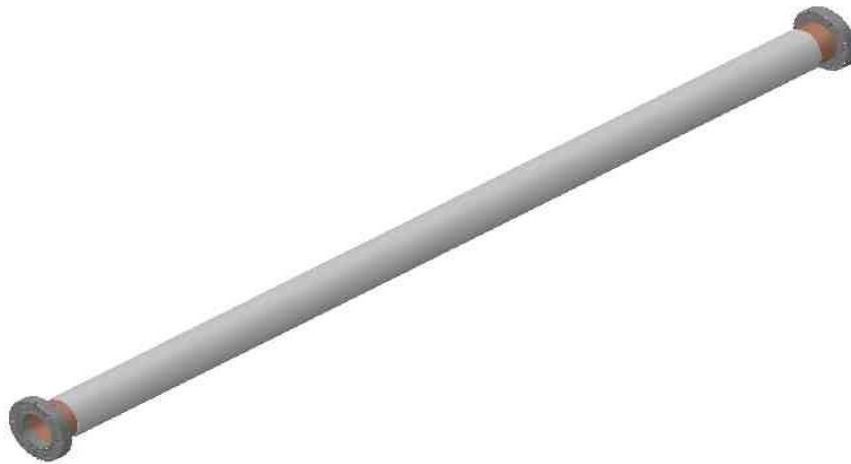
# Impedance of XFEL Ceramic Kicker Vacuum Chamber with Metallic Coats.

***A. Tsakanian***

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Ceramic Kicker Vacuum chamber:

Ceramic with Titanium-Stabilized High Gradient Steel (TSHGS) coats



Vacuum Chamber Parameters

Radius - 0.01 m

Length - 0.9 m

TSHGS Parameters

Thickness -  $0.7 \mu\text{m}$

Resistance -  $R/L = 10 - 12 \Omega\text{m}^{-1}$

$\sigma \approx (2.0841 \pm 0.18946) \times 10^6 \Omega^{-1}\text{m}^{-1}$

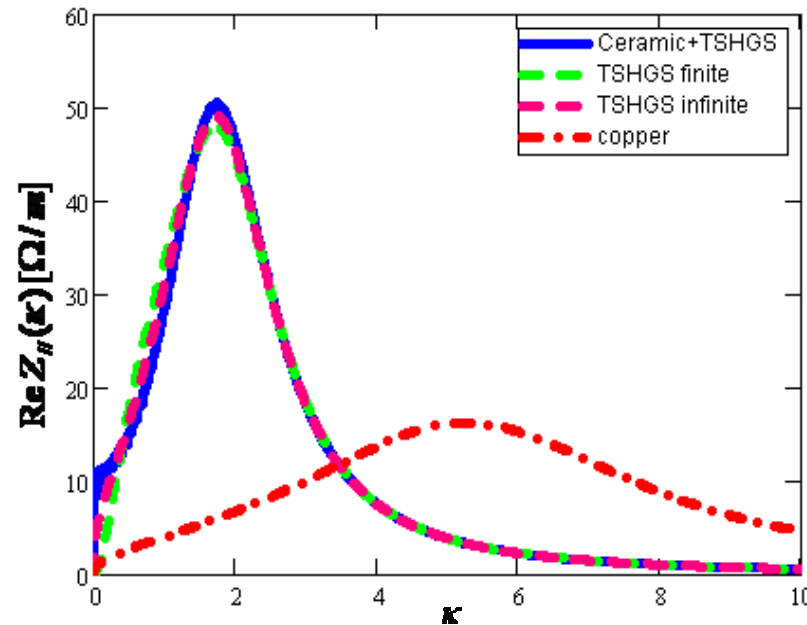
Ceramic Parameters

$\epsilon_r = 9.1$

$\tan \delta \sim 10^{-4}$

*A. Tsakanian*

## Monopole Term Longitudinal Impedance Per Unit Length



$$\kappa = k \cdot s_0$$

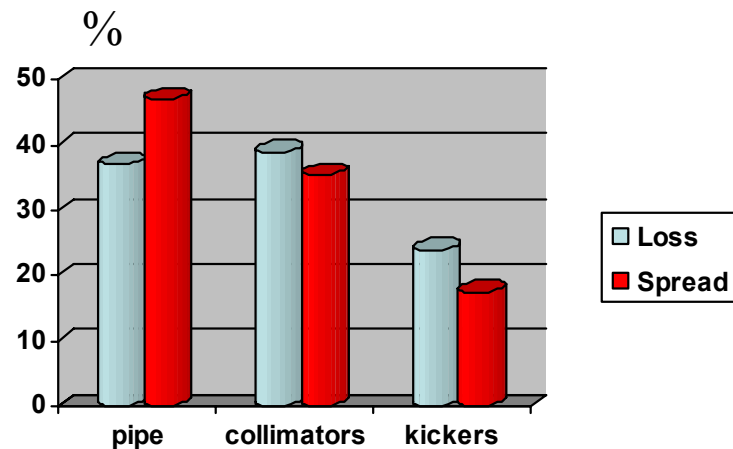
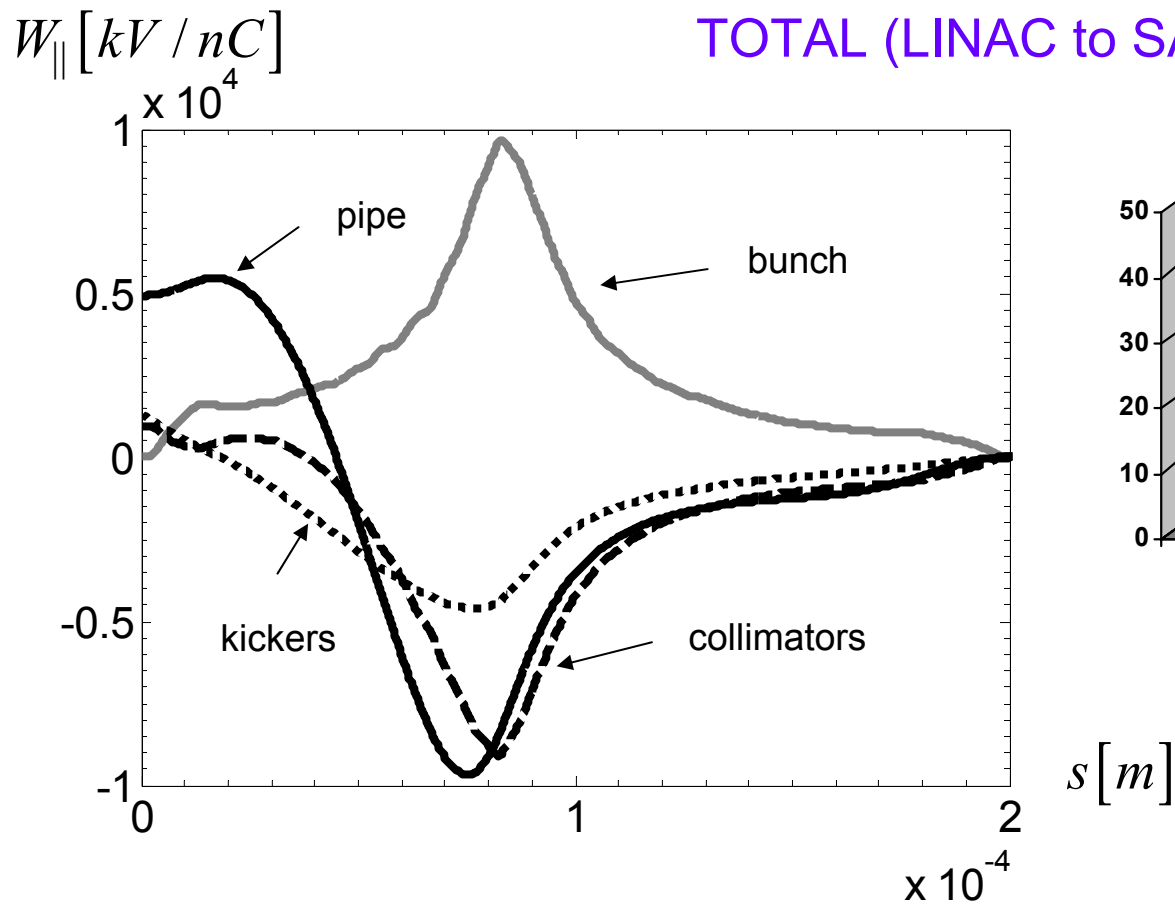
Longitudinal monopole impedance as function of dimensionless wave number for several cases of vacuum chamber material:

1. Ceramic with TSHGS coats.
2. TSHGS single layer tube with finite and infinite thickness.
3. Copper single layer tube.

**$s_0$  characteristic distance:**  $s_0 = \left(2ca^2 \varepsilon_0 / \sigma\right)^{1/3} \approx 63.4 \mu\text{m}$

transverse  $\rightarrow$  A.T.

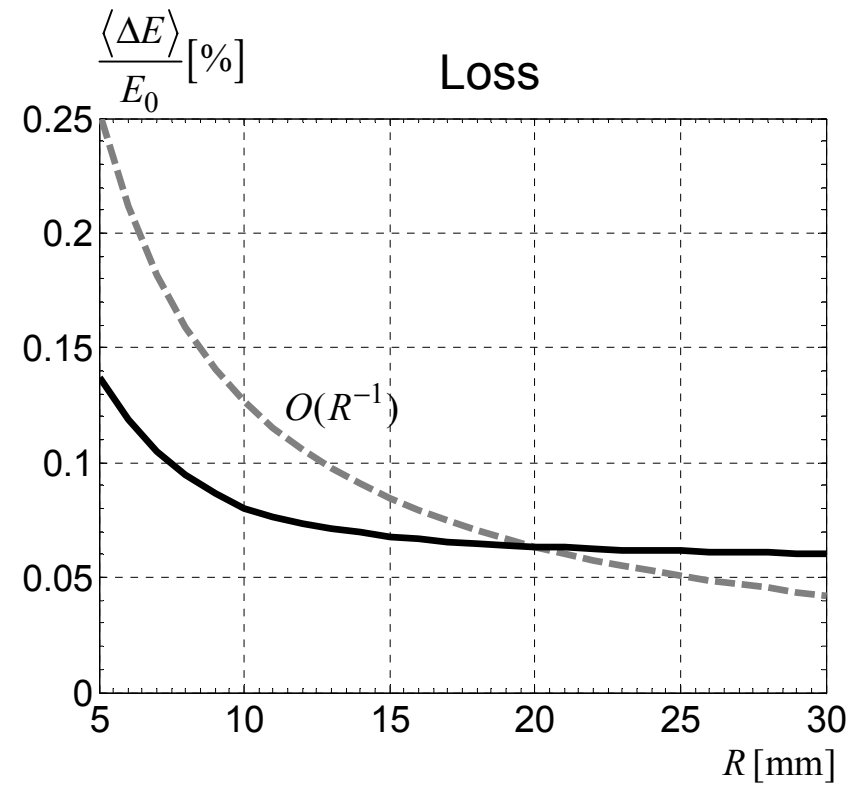
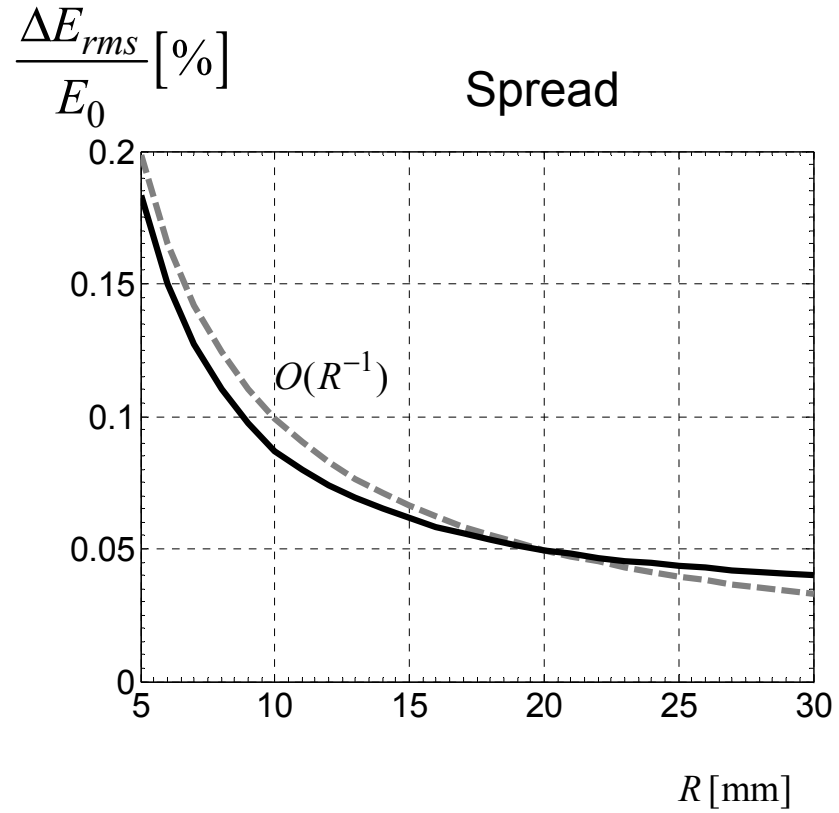
## TOTAL (LINAC to SASE2)



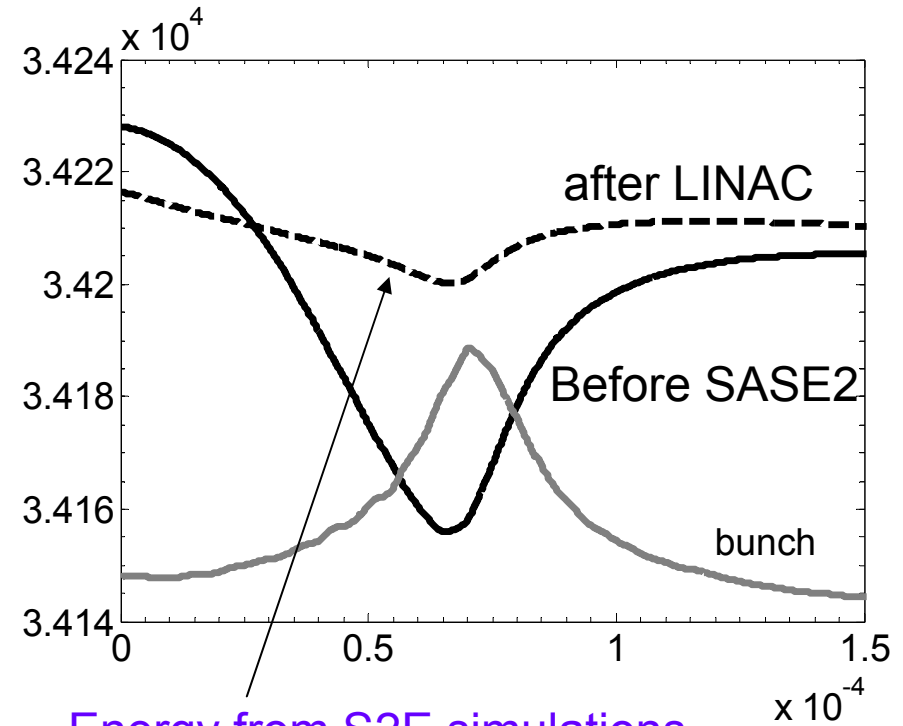
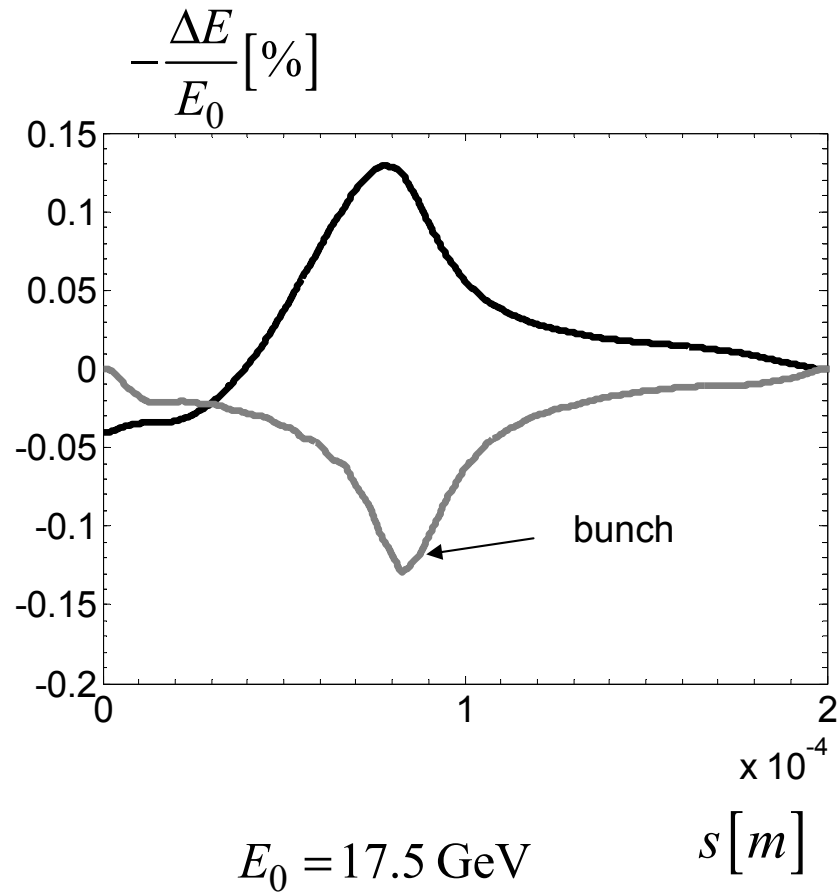
$kV/nC$	Pipe (456m)	Collimators (4 items)	Kickers (3*10m)	Total
Loss	4103	4343	2659	11105
<b>Spread</b>	<b>4222</b>	<b>3164</b>	<b>1557</b>	<b>8682</b>
Peak	-9680	-9088	-4633	-22595



# Energy losses between LINAC and SASE2 vs. pipe radius R

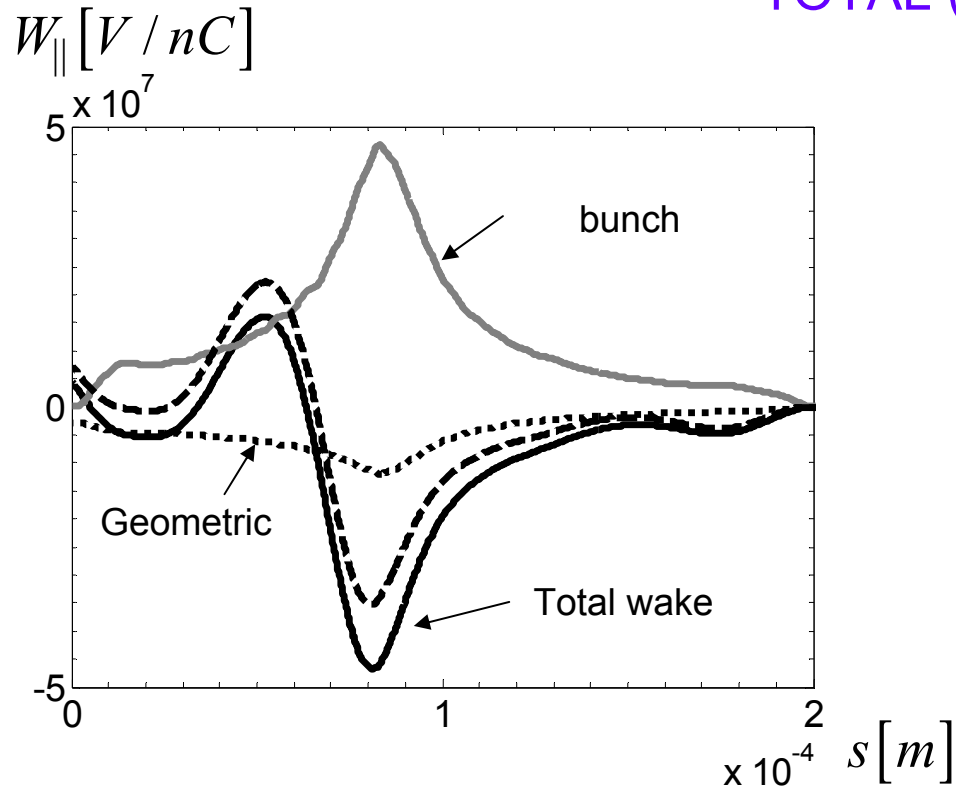


## Energy spread due to wakefields between LINAC and SASE 2

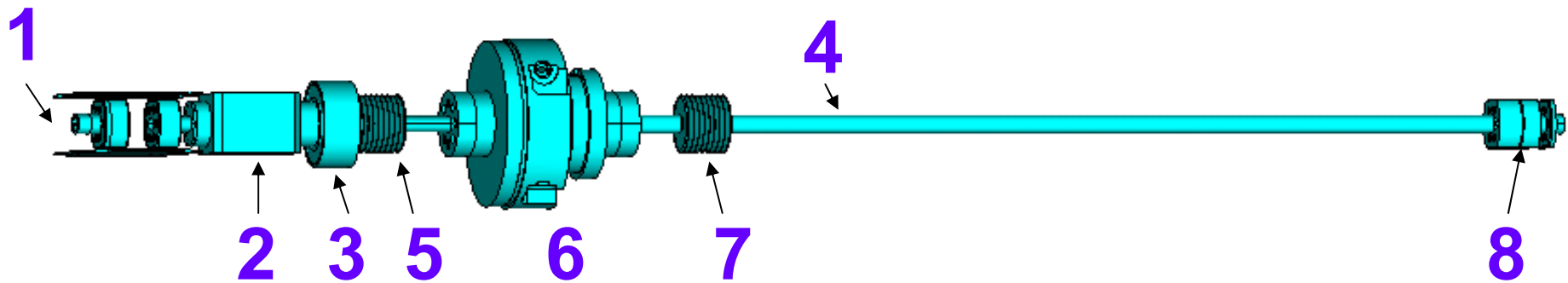


Energy from S2E simulations  
by Martin Dohlus

# TOTAL (SASE2)



$kV / nC$	Geometric	Total
Loss	0.69e4	1.77e4
Spread	0.33e4	1.89e4
Peak	-1.2e3	-4.67e4



(for comparison)

Katrin Schuett, ZM1  
Dirk Lipka, MDI

# Energy spread between LINAC and SASE2 vs. pipe radius R (normalized to the spread in SASE2)

$$\frac{\Delta E_{rms}^{Linac2SASE2}}{\Delta E_{rms}^{SASE2}} [\%]$$

